UPDATED MINERAL RESOURCE ESTIMATE, NORTH TIMMINS PROJECT, TIMMINS, ON

GOWEST GOLD LTD.

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DATE: NOVEMBER 15, 2012

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1. SUMMARY

Messrs. Neil N. Gow, P.Geo., Mr. Kevin Montgomery, P.Geo. and Ms. Peimeng Ling, P.Eng. were retained by Mr. Greg Romain, President of Gowest Gold Ltd. (Gowest) to prepare an updated mineral resource estimate and updated independent technical report on a group of claims located north of Timmins, ON. This report is required to update the status of the most recent drilling campaign. This technical report conforms to National Instrument 43-101 (NI 43-101) Standards of Disclosure for Mineral Projects. The effective date of this report is November 15, 2012.

Gowest holds a central block of claims, the Frankfield Block that has been the site of almost all of the work to date. The Frankfield Block is located in Tully and Prosser Townships. More recently, various contiguous claim blocks have been added to the Frankfield Block in Tully, Little and Evelyn townships. Other claims in Tully, Prosser, Wark and Gowan Townships are included in the overall property and are discussed in this report.

The objectives of this report are to update the mineral resource estimate for the Frankfield East deposit. Since the previous report with an effective date of November 2011, Gowest has completed 46 diamond drill holes with an aggregate depth of 14,835 m. The database and the geological and structural models have all been updated. Whereas, the previous NI 43-101 report relied on a polygonal estimate, a block model has been developed. Gowest considers that the block model will be more useful for ongoing mine planning and other work that the company wishes to undertake.

TABLE 1-1 MINERAL RESOURCE ESTIMATE				
Frankfield East deposit –Gowest Gold Ltd.				
Indicated Resources				
Lens ID	**Volume**	**Tonnes**	**Oz Au**	**Grade g/t Au**
MZ1	521,908	1,487,438	241,497	**5.05**
MZ2	469,064	1,336,832	200,283	**4.66**
HWZ1	484,036	1,379,503	214,659	**4.84**
HWZ2	451,000	1,285,350	207,033	**5.01**
HWZ3	185,060	527,421	82,070	**4.84**
Totals	**2,111,068**	**6,016,544**	**945,542**	**4.88**
Inferred Resources				
Lens ID	**Volume**	**Tonnes**	**Oz Au**	**Grade g/t Au**
MZ1	995,816	2,838,076	425,198	4.66
MZ2	33,232	94,711	9,987	3.28
HWZ1	189,852	541,078	69,409	3.99
HWZ2 (50m)	41,856	119,290	16,951	4.42
HWZ3 (50m)	34,988	99,716	15,228	4.75
Totals	**1,295,744**	**3,692,871**	**536,773**	**4.22**

Notes:
1. (CIMM) Canadian Institute of Mining, Metallurgy and Petroleum) definitions were followed for Mineral resources.
2. Mineral Resources are estimated at a cut-off grade of 3 g/t Au.
3. Mineral Resources are estimated at a long-term gold price of US$1,200/oz, and a US$/C$ exchange rate of 1:1.
4. A minimum width of 2 m was used.

The mineral Resource estimate is based on drilling up to April 2012

The major part of the recommendations in this report is taken from Ling and Trinder (2012). The recommendations deal with the preparation of a final feasibility study and initial detailed mine planning. Further drilling in the upper part of the deposit is considered necessary. All of this work will be carried out to, or for the advancement of the Frankfield Block.

Some drilling is required as part of the agreement with Transition Metals. This work will be carried out outside the Frankfield Block.

TABLE 1-2 RECOMMENDED PROGRAM COSTS
Frankfield Project – Gowest Gold Ltd.

Item	**C$**
Milling	
Final Engineering Agreement and Feasibility Study	800,000
Mining	
Block model development	150,000
Mine development plans	300,000
Further diamond drilling (20,000 m @$125/m)	2,500,000
Mining permits	350,000
General and Administration	
G&A	2,200,000
Subtotal	6,300,000
10% contingency	630,000
Outside Exploration	
Transition Metals Option	500,000
Grand Total	**7,430,000**

Any further work will follow the completion of the Feasibility Study.

1.1. TECHNICAL SUMMARY

1.1.1. PROPERTY DESCRIPTION AND LOCATION

The North Timmins Project of Gowest includes patented claims, mineral claims and claims held under joint venture with Transition Metals Corp. (Transition). The entire property covers an area of 9,449 ha. The claims lie with Tully, Prosser, Wark, Gowan, Little and Evelyn Townships. Access to the main area of interest at the present time, the Frankfield Block, is gained along Highway 655 and then 13.5 km along an all-weather dirt road east off the highway. Gowest owns a 100% interest in all of the claims that are not part of the Transition joint venture.

1.1.2. HISTORY

As with much of the Timmins camp, the area controlled by Gowest has had a long, involved exploration history. The area was especially active during the Texasgulf/Kidd Creek discovery period. The mineralization of interest for which mineral resources are estimated, lies within the Frankfield Block. The initial discovery of mineralization occurred before Gowest obtained title to the property.

1.1.3. GEOLOGY

The Gowest claims lie within different parts of the Abitibi Greenstone Belt. Various terranes are recognized within the claims area. These are the Porcupine Assemblage and the Kidd-Munro Assemblage. These assemblages have been divided in some detail.

The North Timmins Project is underlain by tholeiitic basalt flows and komatiitic basalt to peridotite flows of the Kidd-Munro assemblage. Thin (<10 m) units of pyritic graphitic argillite interflow sediments are commonly at or close to the contacts of the komatiitic peridotite flows in the tholeiitic volcanic sequence. Depositional indicators demonstrate a steeply north dipping and north younging direction for the volcanic sequence. The stratigraphy has been deformed by at least two periods of deformation, as is common in the Abitibi Greenstone Belt.

Mineralization is present in a number of sub-parallel lenses that broadly follow the strike. At present, five lenses are recognized; the Main Zone One (MZ1), the Main Zone Two (MZ2) and four hanging wall lenses (HWZ1, HWZ2, and HWZ3). The bulk of the mineralization lies within the two Main Zones. Gold is associated with arsenopyrite and pyrite and the lenses generally show a characteristic alteration package with silicification, minor quartz-ankerite veining, hematite staining and the presence of tourmaline. Gold is almost inevitably fine-grained and there is no coarse-gold problem associated with the deposit.

1.1.4. MINERAL RESERVES / RESOURCES

The mineral resource estimate that is updated in this report is based on the results of 292 holes with an aggregate length of 86,408 m. A database was prepared and validated. A block model was constructed with blocks 2 m X 2 m X 1 m. The size of the blocks allowed the shapes of the lenses to be better mimicked. Suitable variograms could not be developed and the grades were interpolated using inverse distance squared (ID2).

1.1.5. METALLURGY

Metallurgical studies were conducted by Gowest primarily at SGS Canada Inc. (Lakefield Research) in 2008 and 2010/11 and are ongoing at the time of this report. Preliminary metallurgical tests undertaken include:

- Mineralogy and gold deportment studies.
- Direct cyanidation.
- Flotation.
- Pressure oxidation.
- Bacterial oxidation (completed by Goldfields Limited).

Prior to the initiation of the 2010/11 metallurgical test work program a series of rock samples from different zones within the deposit were subjected to a program of QEMSCAN™ and XRD analysis by

SGS Canada (Lakefield Research) to identify the type and nature of the mineral species present in the deposit. The results of this program provided insights into the physical characteristics of the deposit, which included:

- Arsenopyrite and pyrite were the primary carriers of gold with the fine gold grains (submicron to 10 microns in size) being largely attached to or locked within the sulphides.
- Sulphide minerals were comprised almost exclusively of pyrite and arsenopyrite with variations in the ratio of these species in the different mineral zones.
- Sulphide grain sizes were very similar in the different ore zones (main vs. hanging wall) with >80% liberation at a particle size of 20-30 microns.
- The non-sulphide minerals in the different ore zones were relatively similar with the exception of a quantity of micas/clays in the hanging wall areas that was largely absent in the main zone.

Overall, the QEMSCAN™ and XRD data confirmed that differences between the mineralization present in the historically identified main and hanging wall zones were in fact minimal and both areas should respond similarly to metallurgical treatments

Following the completion of the mineralogy work a comprehensive metallurgical test work program was completed primarily at SGS. The main conclusions developed by the SGS work include:

- The gold present in the Frankfield East deposit is “refractory” in nature producing low recoveries via direct cyanidation (<10%). Fine grinding offers small improvements in recovery.
- Through the use of selective flotation a high-grade arsenopyrite concentrate representing 6-7% of the original ore mass can be produced (+90 g/t Au) with gold recoveries of approaching 93%.
- Alternately, a bulk flotation concentrate containing both pyrite and arsenopyrite can be produced representing 12% of the original ore mass with gold recoveries approaching 97%.
- Pressure oxidation of the flotation concentrates can oxidize up to 99% of the sulphide minerals at 200^{o}C with a retention time of 60 minutes.
- Gold extraction from the neutralized pressure oxidation residues approaches 97-98% after 24 hours of conventional cyanidation.
- Bacterial oxidation of the flotation concentrates can produce 96% sulphide mineral oxidation after 5 days. Gold dissolution from the neutralized residues approaches 95-96%.
- Additional metallurgical test work continues at SGS. The ongoing work is directed at further optimising the conditions for recovery of gold from the Frankfield East deposit. Specifically this involves:
- Optimisation of pressure oxidation conditions, including temperature, oxygen partial pressure, and reaction time.
- Additional flotation studies including a continuous min-pilot campaign.
- Studies to optimize the stability of the arsenic-bearing residues and solutions from the pressure oxidation process.

1.1.6. ENVIRONMENTAL AND PERMITTING

Gowest retained Golder Associates in 2010 to conduct environmental baseline studies on the Frankfield Gold Project. Data acquisition is completed and Golder is interpreting the results which will be presented in a final report at the end of 2012. Completed environmental baseline studies include:

- Geochemistry
- Water Quality

- Hydrology
- Hydrogeology
- Terrestrial Ecology
- Aquatic Ecology

1.1.7. MINING

A conceptual plan was prepared for the underground mining operations at the Frankfield Project. Sections through the deposit were prepared on 25 m spacing showing the mineralized intervals on each hole. Intervals were then connected vertically based on geological interpretations to estimate the extents of the parallel zones present throughout the deposit. A total of six (6) zones within the “main zone” and first two “hanging wall zones” were identified and enveloped in 3D wireframes.

The Frankfield East deposit consists of bulk mining areas as well as narrow vein sections. The two main mining methods selected for this phase of mine evaluation are open stopping and shrinkage/cut and fill. Open stopping was selected where the geometry of the deposit appeared regular between sublevels. Shrinkage was suitable where a more selective technique was required in areas that are thinner and more irregular.

The overall mine plan envisions a predevelopment period where ramp access will be completed from surface down to the 200 m mine level. Following the initiation of commercial mining operations, production will be supported exclusively via ramp access down to approximately the 400-500 m level. Following this an auxiliary shaft would be constructed to maintain mine production rates as the mining operations progress to greater depths.

It is expected that the mine plan as currently conceived would allow for production rates of approximately 1500 tpd. Based on the current models, approximately 2/3 of this extraction rate would come from open stops and the remainder from shrinkage operations. As much as possible waste rock generated by underground mine development will be placed in mined out stops to avoid hoisting/trucking it to surface.

It is estimated that the quantity of backfill required for the operation will be approximately 35-40% of the mined ore production rate. Existing sand and gravel pits in close proximity to the mine site will be utilized for the preparation of mixed fill. Studies are currently underway to determine optimal backfill mix ratios and the quantity of deslimed flotation tailings from the Frankfield processing site that can be backhauled to the mine for use in the backfill mix.

1.1.8. PROCESSING

A complete Metsim computer simulation was prepared for the Frankfield processing operations. It is assumed that a portable crushing and screening plant with a daily production rate of 1500 tonnes will be operated at the mine site by an independent contractor. Crushed material will then be transported by truck to the processing facility for gold recovery operations. The current plant design incorporates the following unit processes:

- Comminution -- grinding (d_{80} of 75 microns) and regrinding (d_{80} of 25 microns)
- Flotation for gold concentrate production
- Pressure oxidation (POX) of sulphide concentrate
- Cyanidation of POX's discharge for gold recovery
- Gold refinery

- Tailings and cyanide destruction

It is important to note that the later stages of the process (pressure oxidation, cyanidation, etc.) will be performed only on the flotation concentrate which represents approximately 180 tpd of the original 1500 tpd plant feed rate. Overall gold recoveries through the entire processing plant are estimated at 95% resulting in an annual production rate of approximately 95,000 ounces of gold.

1.1.9. CAPITAL AND OPERATING COSTS

Life-of-mine capital costs of $253 million are summarized in Table 1-3. Of this total, $167 million represents the initial capital outlay followed by $86 million of sustaining capital. The largest single component of the sustaining capital requirement (approximately $50 million) is the result of the construction of an auxiliary ore haulage shaft. Included in the totals are approximately $33 million in mine pre-development activities (mine site and ramp development to 200 m level). Subsequent to the initial pre-development costs all additional mine development is treated as operational development and included in the contractor mining rates.

TABLE 1-3 BASE CASE CAPITAL COSTS (GREENFIELDS PLANT) - $M

Area	Pre-Production Capital Costs	Sustaining Capital Costs	Total Capital Costs
Mine			
Mine predevelopment	21		21
Mine site	12[*1]		12
Mine expansion (shaft)		50 (year 4-5)	50
Process Plant/ Infrastructure			
Processing Plant	96		96
NSR Purchase	3.5[*2]		3.5
Infrastructure	12		12
Tailings	10	5 (year 4)	15
Mine Closure (less $4 million salvage value)		11	11
Owner cost	12		12
Sustaining Capital (LOM)		20	20
Total Capital	167	86	253

Notes:
Cost includes predevelopment mine costs plus installation of mine site permanent substation and truck shop.
Buyout of NSR royalty related to Texmont land acquisition.

The total unit operating costs for the project are estimated at $119 /tonne of ore resulting in a net cash production cost of $660 /oz of gold (including corporate G&A). It should be noted that the decision to utilize contractors for mining and crushing has added somewhat to this cost. Should the deposit resource continue to grow it may make sense in future evaluations to perform these activities in-house. Of the total $39 /tonne in processing costs, approximately $17 /tonne are related to the additional sulphide oxidation stage, which is required to effectively process the Frankfield East mineralization. This equals to a processing cost of $90-100 /oz of recovered gold beyond that which would be expected from more "conventional" non-refractory gold deposits.

TABLE 1-4 OPERATING COST SUMMARY

Description	$/tonne ore
Total Underground Mining Costs Crushing and Haulage Processing/Refining G&A	68.80 7.00 38.82 4.28
Total	**118.90**

The life-of-mine operating costs are summarized in Table 1-4. It is assumed that mining and crushing/haulage operations will be performed by qualified independent contractors.

1.1.10. ECONOMIC ANALYSES

The base case economic analysis for the Frankfield East gold deposit envisions the construction of a new mine and processing facility with an average annual production of 95,000 ounces of gold at a cash cost of $660 per ounce over a 10-year mine life. Under this scenario and at a gold price of $1,200 /oz, the Frankfield East gold deposit is expected to generate $265 million in pre-tax net cash flow, a pre-tax NPV (5% discount) of $159 million and a pre-tax IRR of 23% (USD/CAD = 1). The payback period is 3.3 years.

Table 1-5 summarizes the parameters utilized in this economic analysis.

TABLE 1-5 BASE CASE ECONOMIC MODEL PARAMETERS

Item	Value
Mining / Processing Throughput	1,500 tpd
Mineable Resource (based on total indicated+inferred resources)	85%
Mine Life	10 years
Total Mining Costs	$69 per tonne
Crushing /Truck Haulage	$7 per tonne
Total Processing Costs	$39 per tonne
G & A Costs	$4.30 per tonne
Gold Price (USD)	$1,200 per oz.
Exchange rate	1 USD/CAD
Overall Gold Recovery	95%
Initial Capital Costs ($167 million)	
Process Plant / Infrastructure / Owner's Costs	$130 million
Mine Development	$21 million
Mine Site	$12 million

Item	Value
Sustaining Capital Costs (LOM - $86 million)	
Phase 2 Tailings Expansion	$5 million
Mine Shaft Construction	$50 million
Sustaining Capital (LOM)	$20 million
Mine Closure Costs (less $4 million salvage value)	$11 million

The economic model used in the current PEA study is simplified as follows:

- Average diluted LOM mined material grades are used for all production years;
- All preproduction capital costs are assumed to take place in Year 0
- Mining unit costs, processing unit costs and gold recoveries are assumed to be equal to their LOM averages for all production years
- Gold prices are constant at $1,200 /oz
- No inflation is incorporated into the model parameters
- No allowances are made for depreciation or taxes.

A sensitivity analysis performed on the Frankfield East Project economic model demonstrates that the project economics are most impacted by variations in gold prices and mined gold grades and least impacted by capital requirements and operating costs. A summary of the analyses is included in Table 1-6.

TABLE 1-6 PEA BASE CASE SENSITIVITY ANALYSIS

			Cash Cost	Project NPV: ($millions)		
Sensitivity	**Variances**	**Value**	**USD/ oz**	**0%**	**5%**	**IRR**
Gold Price	-15%	$1,020	$660	$92	$32	10%
($ / oz gold)	Base Case	$1,200	$660	$265	$159	23%
	+15%	$1,380	$660	$437	$285	36%
Mined Gold Grade	-15%	5.0 g/t	$779	$92	$32	10%
(g/t gold)	Base Case	5.9 g/t	$660	$265	$159	23%
	+15%	6.8 g/t	$577	$437	$285	36%
Total LOM Capital	-15%	$215	$660	$301	$191	30%
($ millions)	Base Case	$252	$660	$265	$159	23%
	+15%	$290	$660	$229	$127	18%
Mining Cost	-15%	$58/ tonne	$603	$320	$200	27%
(per tonne of ore)	Base Case	$69/ tonne	$660	$265	$159	23%
	+15%	$79/ tonne	$718	$210	$120	19%
Process Cost	-15%	$33/ tonne	$628	$296	$182	26%
(per tonne of ore)	Base Case	$39/ tonne	$660	$265	$159	23%
	+15%	$45/ tonne	$693	$243	$136	21%

Gowest is continuing to drill at the Frankfield East deposit with an intention of expanding the resource base. A sensitivity analysis was completed in Table 1-7 to demonstrate the impact of potential increases in gold resources on the base case PEA results. Parameters used to calculate the NPV and IRR remain the same with the following exceptions for the +50% resource case:

- Mine production and processing rate increased by 50% to 2,250 tpd
- Capital costs are factored from the base case values based on the increased throughput (initial capital requirement of $258 million)
- Unit operating costs unchanged with the exception of the labour, which was assumed to be reduced based on the change in throughput (total labour costs unchanged but unit costs reduced).

TABLE 1-7 INCREASE IN GOLD RESOURCE RESULTS (@ $1,200 PER OZ GOLD PRICE.)

			Cash Cost	Project NPV ($millions)		
Sensitivity	**Total LOM Capital**	**Mine Life**	**USD/ oz**	**0%**	**5%**	**IRR**
Gold Resources +20% 1500 tpd	$257	12	$660	$367	$214	25%
Gold Resources +50% 2250 tpd	$307	10	$626	$518	$327	28%

2. INTRODUCTION

Messrs. Neil N. Gow, P.Geo., Mr. Kevin Montgomery, P.Geo. and Ms Peimeng Ling, P.Eng. were retained by Mr. Greg Romain, President of Gowest Gold Ltd. (Gowest) to prepare an updated mineral resource estimate and updated independent technical report on a group of claims located north of Timmins, ON. This report is required to update the status of the most recent drilling campaign. This technical report conforms to National Instrument 43-101 (NI 43-101) Standards of Disclosure for Mineral Projects. The effective date of this report is November 15, 2012.

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Gowest has been exploring the Frankfield Block since 1983. A number of diamond drilling campaigns have been carried out on the property and semi-continuous diamond drilling has been carried out since 2004. The property remains an exploration target and there has been no development on the Frankfield Block to date.

This report was completed by Mr. Neil N. Gow and Mr. Kevin Montgomery, and these writers are responsible for Chapters 1 to 12, Chapters 14 and 15, and Chapters 23 to 27. Ms Peimeng Ling has previously completed a NI 43-101 report and is responsible for Chapters 13, and 16 to 22. Each of the authors have visited the property at different times in the past.

Sources of Information

Gow visited the property twice, during an earlier drilling campaign and on March 16, 2011. Mr. Kevin Montgomery is responsible for exploration on the various Gowest properties and has visited the properties numerous times.

Discussions were held with Messrs. Darren Koningen, Technical Advisor - Project Development for Gowest, and Ms. Angela Falcon, Resource Geologist for Gowest. Mr. Kevin Montgomery is familiar with the property and with the work that has been taking place during the program discussed here.

This report was prepared by Neil Gow. P.Geo., an independent consulting geologist. Gow is an independent Qualified Person (QP) and is responsible for Sections 1 to 12, Chapter 14 and Chapters 2 to 27. Gow was aided by Mr. Kevin Montgomery, a geological consultant of Gowest. Ms Peimeng Ling is an independent consultant and prepared a NI 43-101 report on behalf of Gowest earlier in 2012. Some of the material in that report is again reported in this report, specifically in Chapters 13, and 15 to 22

The documentation reviewed, and other sources of information, are listed at the end of this report in Section 27, References.

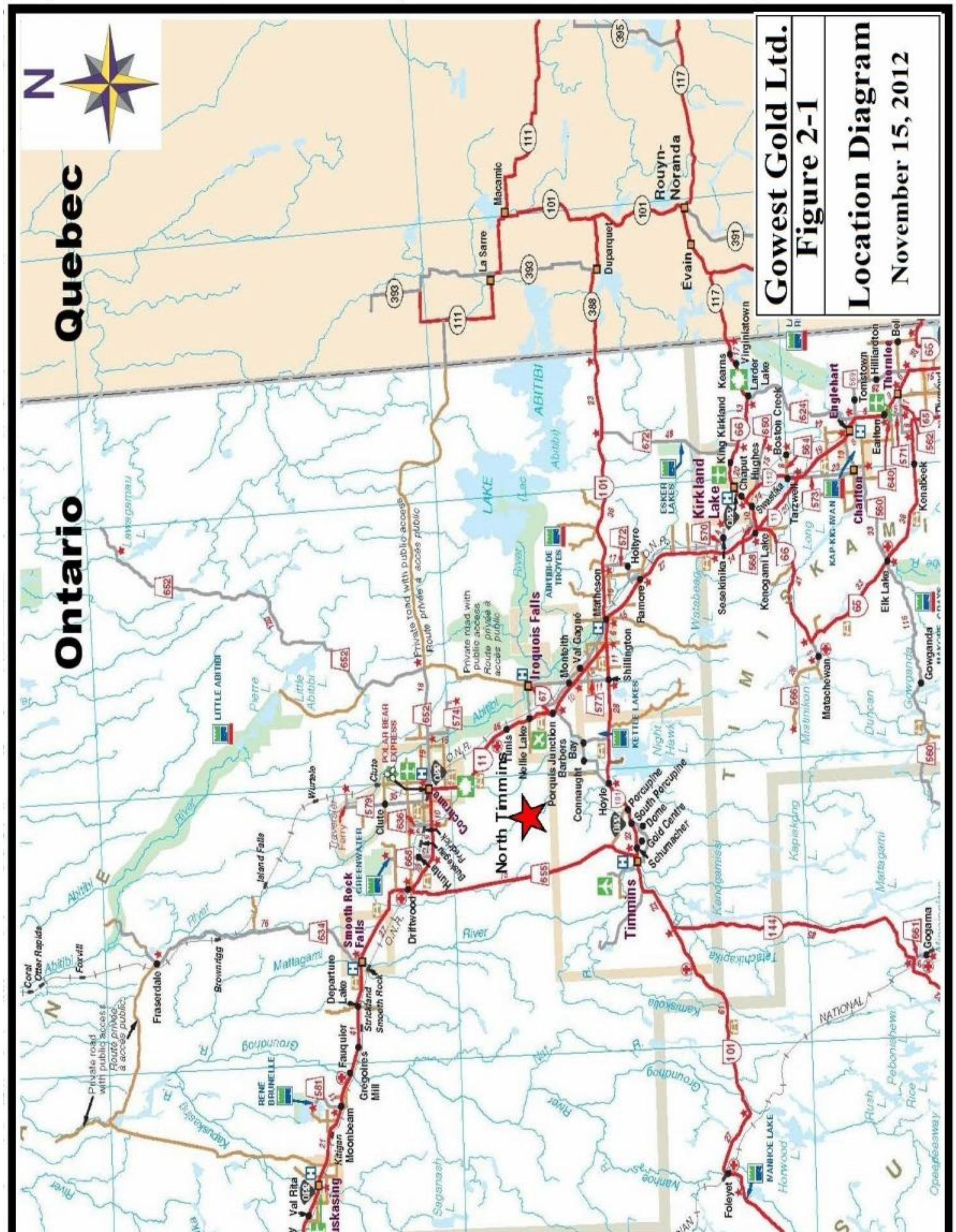

FIGURE 2-1 LOCATION DIAGRAM

2. 1 LIST OF ABBREVIATIONS

Units of measurements used in this report conform to the Metric System. All currency in this report is Canadian dollars (C$) unless otherwise noted.

µ	micron
°C	degree Celsius
°F	degree Fahrenheit
µg	microgram
A	ampere
a	annum
Au	gold
bbl	barrels
Btu	British thermal units
C$	Canadian dollars
cal	calorie
cfm	cubic feet per minute
cm	centimetre
cm^2	square centimetre
d	day
dia.	diameter
dmt	dry metric tonne
dwt	dead-weight ton
ft	foot
ft/s	foot per second
ft^2	square foot
ft^3	cubic foot
g	gram
G	giga (billion)
Gal	Imperial gallon
g/L	gram per litre
g/t	gram per tonne
gpm	Imperial gallons per minute
gr/ft^3	grain per cubic foot
gr/m^3	grain per cubic metre
hr	hour
ha	hectare
hp	horsepower
in	inch
in^2	square inch
J	joule
k	kilo (thousand)
kcal	kilocalorie
kg	kilogram
km	kilometre
km/h	kilometre per hour
km^2	square kilometre
kPa	kilopascal
kVA	kilovolt-amperes
kW	kilowatt
kWh	kilowatt-hour
L	litre
L/s	litres per second
m	metre
M	mega (million)
m^2	square metre
m^3	cubic metre
min	minute
MASL	metres above sea level
mm	millimetre
mph	miles per hour
MVA	megavolt-amperes
MW	megawatt
MWh	megawatt-hour
m^3/h	cubic metres per hour
opt, oz/st	ounce per short ton
oz	Troy ounce (31.1035g)
ppm	part per million
psia	pound per square inch absolute
psig	pound per square inch gauge
RL	relative elevation
s	second
st	short ton
stpa	short ton per year
stpd	short ton per day
t	metric tonne
tpa	metric tonne per year
tpd	metric tonne per day
US$	United States dollar
USg	United States gallon
USgpm	US gallon per minute
V	volt
W	watt
wmt	wet metric tonne
yd^3	cubic yard
yr	year

3. RELIANCE ON OTHER EXPERTS

This report has been prepared by Messrs. Gow and Montgomery for Gowest Gold Ltd. The information, conclusions, opinions, and estimates contained herein are based on:

- Information available to writers at the time of preparation of this report,
- Assumptions, conditions, and qualifications as set forth in this report, and
- Data, reports, and other information supplied by Gowest and other third party sources.

For the purpose of this report, the writers have relied on ownership information provided by both Gowest and a title opinion dated December 22, 2011 and prepared by Mr. Brian L. Montgomery of Weaver-Simmons, located in Brady Square, 233 Brady Street, Sudbury, ON, P3B 4H5 indicates that the Gowest title is in good standing.

Except for the purposes legislated under provincial securities laws, any use of this report by any third party are at that party's sole risk.

4. PROPERTY DESCRIPTION AND LOCATION

The North Timmins Project of Gowest is comprised of one patented mineral claim, eight leased mineral claims and 47 unpatented mineral claims variously located in Prosser, Wark, Tully, Gowan, Little and Evelyn Townships (Figure 4-1). Previous NI 43-101 reports have concentrated on the Frankfield Claim Block that is mainly located on the western side of Tully Township but extending into Prosser Township. The central part of the property located in Tully Township lies at about 490000 East and 5397500 North. The total area of the Gowest holdings is 9,449 ha. Within that area, the area of the Transition Metals Corp. (Transition) joint venture is 3,302 ha.

Details of the claims are set out in Table 4-1.

TABLE 4-1 CLAIM DETAILS
North Timmins Project – Gowest Gold Ltd.

Division	Project/Property	Twp	Claim Number	Recording Date	Claim Due Date	
Porcupine - 60	GW Orphan Tully (G-3985)	Tully	4240049	2010-Mar-03	2015-Mar-03	
Porcupine - 60	GW Orphan Tully (G-3985)	Tully	4254623	2010-Mar-03	2015-Mar-03	
Porcupine - 60	GW Pipestone East	Evelyn	4262511	2011-Jun-15	2015-Jun-15	
Porcupine - 60	GW Pipestone East	Evelyn	4262512	2011-Jun-15	2015-Jun-15	
Porcupine - 60	GW Pipestone East	Little	4262513	2011-Jun-15	2015-Jun-15	
Porcupine - 60	GC Tully East Block-1	Tully	1160197	1995-Jan-27	2013-Jun-26	
Porcupine - 60	GC Tully East Block-1	Tully	1207001	1996-Mar-19	2013-Mar-19	
Porcupine - 60	GC Tully East Block-1	Tully	1207003	1996-Mar-19	2013-Mar-19	
Porcupine - 60	GC Tully East Block-1	Tully	1207004	1996-Mar-19	2013-Mar-19	
Porcupine - 60	GC Tully East Block-1	Tully	1207005	1996-Mar-19	2013-Mar-19	
Porcupine - 60	GC Tully East Block-1	Tully	1207007	1996-Mar-19	2013-Mar-19	
Porcupine - 60	GC Tully East Block-1	Tully	1207009	1996-Mar-19	2013-Mar-19	
Porcupine - 60	GC Tully East Block-1	Tully	1207010	1996-Mar-19	2013-Mar-19	
Porcupine - 60	GC Tully East Block-1	Tully	1207701	1996-Mar-27	2013-Mar-27	
Porcupine - 60	GC Tully East Block-1	Tully	1207702	1996-Mar-27	2013-Mar-27	
Porcupine - 60	GC Tully East Block-1	Tully	1207703	1996-Mar-27	2013-Mar-27	
Porcupine - 60	GC Tully East Block-1	Tully	1212880	1997-Mar-10	2013-Mar-10	
Porcupine - 60	GC Tully East Block-1	Tully	1244809	2001-Mar-30	2013-Mar-30	
Porcupine - 60	GC Tully East Block-1	Tully	1244810	2001-Mar-30	2013-Mar-30	
Porcupine - 60	GC Tully East Block-1	Tully	1245331	2001-Mar-30	2015-Mar-30	
Porcupine - 60	Transition Pipestone East	Evelyn	4253001	2010-Feb-02	2014-Feb-02	
Porcupine - 60	Transition Pipestone East	Evelyn	4253002	2010-Feb-02	2014-Feb-02	
Porcupine - 60	Transition Pipestone East	Evelyn	4253003	2010-Feb-02	2014-Feb-02	
Porcupine - 60	Transition Pipestone East	Evelyn	4253004	2010-Feb-02	2014-Feb-02	

Porcupine - 60	Transition Pipestone East	Evelyn	4253005	2010-Feb-02	2014-Feb-02		
Porcupine - 60	Transition Pipestone East	Evelyn	4253006	2010-Feb-02	2014-Feb-02		
Porcupine - 60	Transition Pipestone East	Evelyn	4257022	2010-Jul-12	2014-Jul-12		
Porcupine - 60	Transition Pipestone East	Evelyn	4257023	2010-Jul-12	2014-Jul-12		
Porcupine - 60	Transition Pipestone East	Evelyn	4257024	2010-Jul-12	2014-Jul-12		
Porcupine - 60	Transition Pipestone East	Evelyn	4257025	2010-Jul-12	2014-Jul-12		
Porcupine - 60	Transition Pipestone East	Evelyn	4257027	2010-Jul-12	2014-Jul-12		
Porcupine - 60	Transition Pipestone West	Gowan	4253015	2010-Feb-02	2013-Feb-02		
Porcupine - 60	Transition Pipestone East	Little	4257021	2010-Jul-12	2014-Jul-12		
Porcupine - 60	Transition Pipestone West	Prosser	4253014	2010-Feb-02	2013-Feb-02		
Porcupine - 60	Transition Pipestone West	Prosser	4255012	2010-Mar-09	2013-Mar-09		
Porcupine - 60	Transition Pipestone West	Prosser	4255234	2010-Apr-26	2013-Apr-26		
Porcupine - 60	Transition Pipestone West	Wark	4252998	2010-Apr-27	2013-Apr-27		
Porcupine - 60	Transition Pipestone West	Wark	4252999	2010-Apr-26	2013-Apr-26		
Porcupine - 60	Transition Pipestone West	Wark	4253007	2010-Feb-02	2013-Feb-02		
Porcupine - 60	Transition Pipestone West	Wark	4253009	2010-Feb-02	2013-Feb-02		
Porcupine - 60	Transition Pipestone West	Wark	4253010	2010-Feb-02	2013-Feb-02		
Porcupine - 60	Transition Pipestone West	Wark	4253011	2010-Feb-02	2013-Feb-02		
Porcupine - 60	Transition Pipestone West	Wark	4253012	2010-Feb-02	2013-Feb-02		
Porcupine - 60	Transition Pipestone West	Wark	4253013	2010-Feb-02	2013-Feb-02		
Porcupine - 60	Transition Pipestone West	Wark	4255013	2010-Mar-09	2013-Mar-09		
Porcupine - 60	Transition Pipestone West	Wark	4255233	2010-Apr-26	2013-Apr-26		
Porcupine - 60	Transition Pipestone West	Wark	4255235	2010-Apr-26	2013-Apr-26		
Porcupine - 60	Guidoccio Tully East	Tully	4269722	2012-Mar-08	2014-Mar-08		
Porcupine - 60	Guidoccio Tully East	Tully	4269723	2012-Mar-08	2014-Mar-08		
Porcupine - 60	GW Pipestone East	Little	4270230	2012-May-04	2014-May-04		
Porcupine - 60	GW Pipestone East	Little	4270231	2012-May-04	2014-May-04		
Porcupine - 60	GW Pipestone East	Little	4270232	2012-May-04	2014-May-04		
Porcupine - 60	GW Pipestone East	Little	4270233	2012-May-04	2014-May-04		
Porcupine - 60	GW Pipestone East	Little	4270234	2012-May-04	2014-May-04		
Porcupine - 60	GW Pipestone East	Little	4270235	2012-May-04	2014-May-04		
Porcupine - 60	GW Pipestone East	Little	4270236	2012-May-04	2014-May-04		
Porcupine - 60	GW Pipestone East	Evelyn	4270237	2012-May-04	2014-May-04		
Porcupine - 60	GW Pipestone East	Evelyn	4270238	2012-May-04	2014-May-04		
Porcupine - 60	GW Pipestone East	Evelyn	4270239	2012-May-04	2014-May-04		
Porcupine - 60	GW Pipestone East	Evelyn	4267266	2012-May-04	2014-May-04		

Porcupine - 60	GW Pipestone East	Evelyn	4267267	2012-May-04	2014-May-04	
Division	**Project/Property**	**Township**	**Lease or License**	**Claim No.**	**Start/Anniversary**	**Lease Expiry**
Porcupine - 60	Dowe	Tully	107242	101372	1999-Feb-01	2020-Jan-31
Porcupine - 60	Dowe	Tully	107242	101373	1999-Feb-01	2020-Jan-31
Porcupine - 60	Dowe	Tully	107242	101374	1999-Feb-01	2020-Jan-31
Porcupine - 60	Dowe	Tully	107242	101375	1999-Feb-01	2020-Jan-31
Porcupine - 60	Texmont/Frankfield	Prosser	107280	508392	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Prosser	107280	508394	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107280	508389	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107280	508395	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107280	508396	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107280	508398	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107280	508397	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107280	508399	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107280	508400	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107280	508401	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107280	508402	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Prosser	107281	508391	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Prosser	107281	508393	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107281	508390	1999-Dec-01	2020-Nov-30
Porcupine - 60	Texmont/Frankfield	Tully	107335	97938	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107335	97941	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107335	97942	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107335	97943	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107335	97939	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107335	97940	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107335	97948	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107335	97949	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107336	97944	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107336	97945	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107336	97947	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107336	97946	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107360	99286	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107360	99287	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107360	99289	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107360	99288	2000-Oct-01	2021-Sept-30
Porcupine - 60	Texmont/Frankfield	Tully	107361	100440	2001-Jun-01	2022-May-31
Porcupine - 60	Texmont/Frankfield	Tully	107361	100437	2001-Jun-01	2022-May-31
Porcupine - 60	Texmont/Frankfield	Tully	107361	100441	2001-Jun-01	2022-May-31
Porcupine - 60	Texmont/Frankfield	Tully	107361	100438	2001-Jun-01	2022-May-31

Porcupine - 60	Texmont/Frankfield	Tully	107361	100442	2001-Jun-01	2022-May-31
Porcupine - 60	Texmont/Frankfield	Tully	107361	100439	2001-Jun-01	2022-May-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101255	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101256	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101257	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101258	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101259	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101260	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101261	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101262	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101948	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101949	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101950	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101951	2003-Sept-01	2024-Aug-31
Porcupine - 60	GC Tully North Block-1	Tully	107484	101952	2003-Sept-01	2024-Aug-31
Division	**Project/Property**	**Township and Location**				
Porcupine - 60	Boudreau purchase	Tully	SE1/4 &SW1/4 N1/2 and S1/2 of Lot 1, Conc 1			

Other than the claims labeled with the Transition name in the Table 4-1 that are discussed below, all of these claims are wholly owned by Gowest.

The claims that are labeled with the Transition name are held by Gowest under a joint venture with Transition Metals Corp. Under the terms of the agreement, dated February 10, 2011, Gowest may earn either a 60% equity interest or a 75% equity interest in the claims subject to various conditions. To earn a 60% undivided interest, Gowest must;

- Make a C$50,000 payment upon execution (**Paid**).
- Pay a further C$50,000 on the one year anniversary of the agreement (**Paid**).
- Incur exploration expenditures of C$200,000 by the 18-month anniversary of the agreement (**Incurred**).
- Incur aggregate exploration expenditures of C$1,000,000 by the 36-month anniversary of the agreement.
- Issue 100,000 shares upon execution of the agreement (**Issued**).
- Issue 300,000 shares before the 18-month anniversary of the agreement.

For Gowest to increase its interest to 75%, Gowest must advise Transition of its intention to do so within 30 days of when it has earned 60%. Further Gowest must;

- Incur additional exploration expenditures of C$2,000,000 within a 2-year period.
- Issue a further 150,000 shares of Gowest to Transition. Once this stage is reached, the partners have deemed expenditure positions and normal dilution provisions would prevail.

Gowest has advised the authors that there are no known environmental encumbrances on any of the North Timmins claims.

Gow is advised that property maintenance costs of the Gowest land package is $2,635.87.

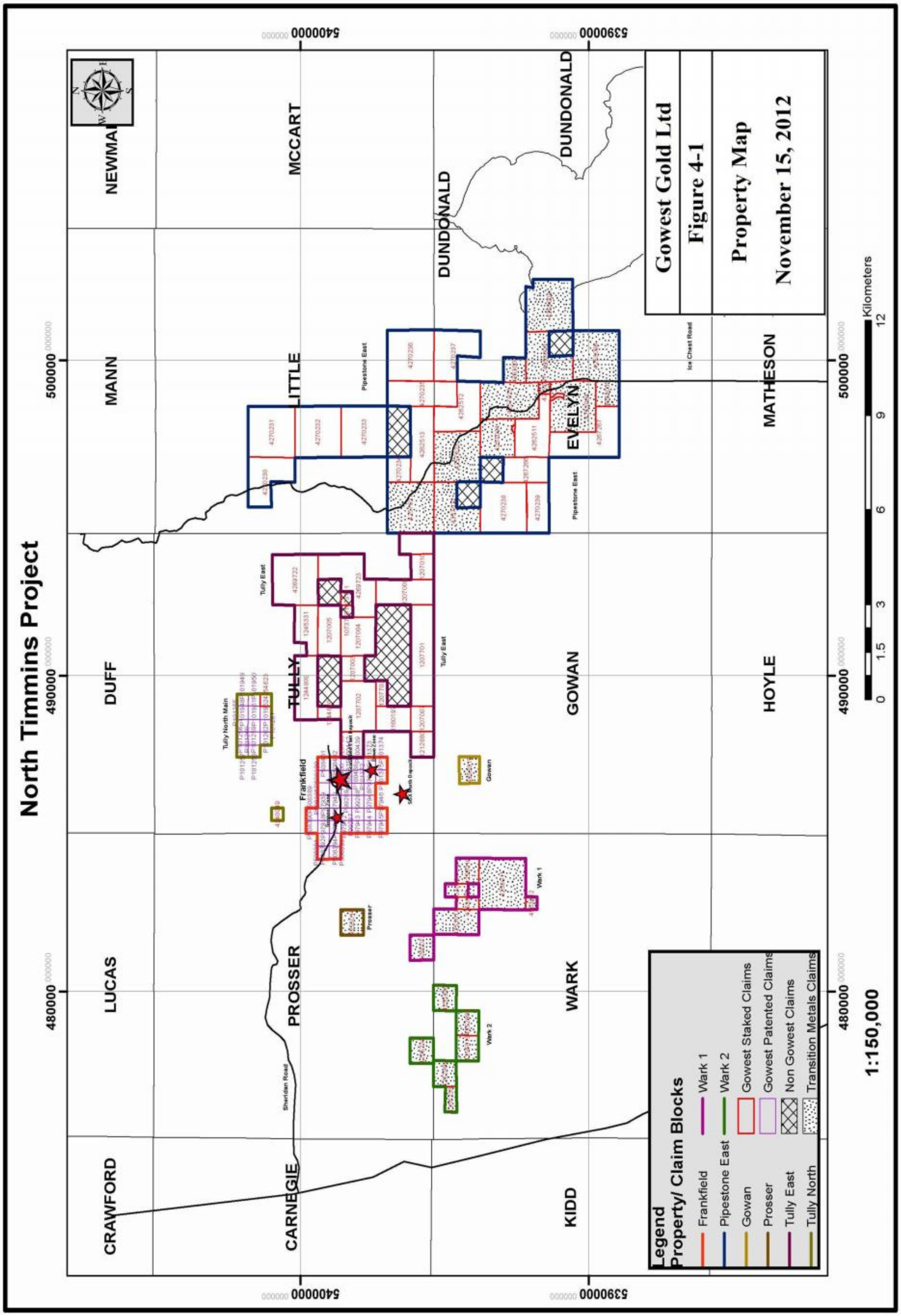

FIGURE 4-1   PROPERTY MAP

5. ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND PHYSIOGRAPHY

5.1. ACCESSIBILITY

The Frankfield Gold Project is located in the southwest part of Tully Township, approximately 32 km north-northeast of the City of Timmins, Ontario. Surface access to the Frankfield Block is easily gained from Timmins via Highway 655 and an all-weather gravel road that turns east off Highway 655, 33.2 km north of the intersection Highways 101 and 665 and 11.5 km north of the Kidd Creek Mine access road. This 13.5 km long all-weather road ends at the Prosser/Tully Township line. The site of Gowest's Frankfield East Deposit and drilling program is approximately 1.5 km further east along a drill road. Alternate access to the property is by charter helicopter service from Timmins.

The eastern portion of the North Timmins Project area is easily accessed from Timmins via Highway 101 East and 13 km north of the highway via the all-weather Ice Chest Lake gravel road. Various ATV trails provide access from this road to the Project area; however an Argo is required to ford streams and negotiate the swampy conditions. Alternate access to the Project is by charter helicopter service from Timmins.

5.2. CLIMATE

The climate is typical of northern boreal forest areas with the Project area experiencing four distinct seasons. There are extended periods of subzero temperatures during the winter months of November through March. Daily average winter temperature in January is -17.5° C with daily average maximum and minimums of -11° C and -23.9° C respectively and an extreme daily minimum of -44.2° C. Daily average summer temperature in July is +17.4° C with daily average maximum and minimums of +24.2° C and +10.5° C respectively and an extreme daily maximum of +38.9° C. The region has average annual precipitation of approximately 83 cm including approximately 56 cm of rain, largely during the months of April to October and up to 3.1 m of winter snow accumulation, occurring largely between the months of November and April (Environment Canada, 2011).

Mineral exploration can be conducted year-round, however because of the swampy ground conditions on the Project, exploration activities such as geophysical surveys and diamond drilling are more easily conducted in the winter due to better accessibility after freeze-up.

5.3. LOCAL RESOURCES AND INFRASTRUCTURE

All-weather gravel road access is currently available to the Prosser/Tully Township line in the north-western part of the Project. Access to the Frankfield East Deposit could be achieved by constructing approximately 1.0 km to 1.5 km of new gravel road to connect with the existing gravel road network. Numerous drill trails crosscut the Project area. Despite wet and swampy ground conditions common throughout the Project area, the drill trails can be accessed by all-terrain vehicles and industrial equipment such as dozers, skidders and muskeg tractors during summer months. Access is easier during the winter months when the ground is frozen.115 kV and 500 kV electric transmission lines paralleling Highway 655 are located approximately 10 km and 13.5 km west of the property respectively. The West Buskegau River, located 1.6 km east of the Frankfield claim block offers an abundant source of process water. Large quantities of aggregate resources are located adjacent to Highway 655, approximately 15 km west of the Frankfield claim block.

Gowest maintains a secure and well equipped, combined field office and core logging-sampling facility at 115 Jubilee Avenue East, Timmins.

The City of Timmins is the nearest source of mining related commercial services and an abundant pool of managerial and skilled labour. Timmins is serviced by modern telecommunications, commercial airlines, rail service and truck transportation.

Gowest holds sufficient surface rights necessary for potential future mining operations including tailings storage areas, waste disposal areas and a processing plant.

5.4. PHYSIOGRAPHY

Regional-scale poorly drained swamp dominates the Project area. The area topography is flat with an elevation of approximately 295 m above sea level. Relief is only a few metres with drier clay ridges rising above open and forested swampy areas. All streams and rivers in the area are part of the Arctic watershed. The West Buskegau River, although a potential source of abundant water for the Project, provides little drainage for the low-lying terrain. Drainage patterns are poorly developed due to the low topographic relief and to the extensive clay cover immediately below the vegetation layer. Many of the diamond drill holes form natural wells. Overburden is generally deep in the region, with depths up to 65 m; however overburden in the area of Frankfield East drilling is generally shallow, ranging from 2 m to 10 m thick. Isolated rock exposures are present in the vicinity of the Texmont deposit and approximately 300 m northeast of the Frankfield East Deposit; the latter outcrop area may be an ideal location for establishment of an underground ramp.

Vegetation consists of poorly developed black spruce, patches of alders and low shrubs. The immediate vicinity of the deposit has been partially cleared of trees, due to diamond drilling campaigns over the years.

6. HISTORY

Previous NI 43-101 reports have dealt with the Frankfield Claim Block in isolation. This current report discusses the Frankfield property and claims that are contiguous with Frankfield or closely related and which make up the North Timmins Project. In the interests of simplicity, the claims have been divided up into township claim groupings (Figure 4-1).

6.1. FRANKFIELD BLOCK

The following description of exploration history is adapted and updated from Harron (2006).

Following the discovery of the nearby Kidd Creek Mine in 1964, exploration activity intensified in Tully and other surrounding townships. In 1964, Texasgulf Sulphur Co. Ltd. completed one diamond drill hole ("DDH") in the S1/2 Lot 10, Concession III of Tully Township (current claim 508402) to test an airborne electromagnetic ("AEM") conductor, which proved to be graphite.

In 1965, Patino Mining Corporation held the S1/2 of Lot 11 Concession III, Tully Township and the S1/2 of Lot 1 Concession III Prosser Township (most of the current Gowest / New Texmont block) and completed both a magnetic and electromagnetic ("EM") surveys. The claims were allowed to lapse.

Texasgulf Sulphur Co. Ltd. in 1963-64, and Texmont Mines Ltd. (Texmont) in 1968 covered the four Prosser Township claims with magnetic and EM surveys. In 1969, Texmont completed two (2) diamond drill holes in the southeast corner of Lot 1 Concession III Prosser Township (current claim 508394) to investigate an EM conductive horizon. The causative source was graphite.

In 1968,Acme Gas and Oil Ltd. (Acme) staked eight (8)claims in the south half of Lots 10 and 11, Concession III, Tully Township (area of current claims 508395to 508402). Magnetic and vertical loop EM ("VLEM") surveys were completed on four (4) claims in Lot 10 Concession III Tully Township (area of current claims 508399-508402). Acme optioned the 8 claims to McIntyre Mines Limited (McIntyre) in 1969. McIntyre completed three (3) diamond drill holes in the east central part of the Acme claim block to test magnetic and electromagnetic responses (area of current claims 508398 and 508400). The diamond drill holes encountered low values of Cu, Zn and Au in diorite and intermediate volcanic rocks. In 1975 Acme optioned the 8 claims to Frankfield Explorations Ltd. ("Frankfield"). The Acme claims lapsed in 1978.

In 1978, Gold Shield Syndicate (Gold Shield) staked claims 508391-508394 being the S1/2 Lot 1, Concession III Prosser Township, and claims 508389 and 508390 being the S1/2 of N1/2 Lot 12 Concession III Tully Township, as well as claims 508395-508402 being the S1/2 of Lots 10 and 11, Concession III Tully Township. These claims cover the northern (down-dip) portion of the Frankfield East Deposit and make up a part of Gowest's current Frankfield Gold Project (the Gowest-New Texmont block). Gold Shield Syndicate completed ground magnetic and VLEM surveys on claims 508395-508398 (S1/2 of Lot 11 Concession III, Tully Township). The geophysical surveys utilized N-S lines 122 m apart. The magnetic survey defined a northwest trending fault diagonally across the S1/2 of S1/2 Lot 11 Concession II. Also defined was a fault on the north flank of a magnetically positive feature interpreted as ultramafic rocks, extending N70°E from the southwest corner of S1/2 of Lot 11 Concession III. The VLEM survey defined several weak conductive features in the S1/2 of the 4 claim group. Three conductive horizons interpreted to be graphite and disseminated sulphides were located. The conductors trend N050°E in the SW corner to N070°E in the central part and 090° in the south eastern part of the 4 claim block. The entire 122 m width of the combined conductive horizons is interpreted as a shear zone (Bradshaw, 1978).

In June 26, 1979, Romex Resources Inc. (Romex) entered into an option/joint venture agreement with Gold Shield Syndicate to earn an interest in the 14 claims.

In 1980, Gold Shield completed magnetic and Crone “Radem” electromagnetic surveys on 10 claims (508391 to 508394 in Prosser township; 508389, 508390 and 508399 to 508402 in Tully Township). In Prosser Township, the magnetic data defined a positive magnetic feature interpreted as folded ultramafic flows. In the S1/2 Lot 10 Tully Township claims, the magnetic data defined a 60° fabric and a N-S diabase dyke. The Radem electromagnetic survey did not define any noteworthy conductive horizons due to the instruments limited penetration of the extensive clay overburden.

Six holes (1,025 metres) drilled in 1980 and 1982 (80-1 to 80-4 and 82-2 and 82-4) tested the down dip extension of the Frankfield East Zone on the Gold Shield property (claims 508396, 508397 and 508400). In 1983, Romex Resources Inc. (Romex) earned a 17% interest in the 14 claims, pursuant to the 1979 option / joint venture agreement. Gowest subsequently acquired Gold Shield’s 83% interest in the 14 claim property.

The Frankfield East Deposit is located on the north boundary of the Intex-Frankfield block, immediately adjacent and south of the Gowest block. To cover the northward down-dip extension of the Frankfield East Deposit onto Gowest-Romex ground, New Texmont Explorations Ltd., (which owned 50% of Intex Mining Company at the time) entered into an option / joint venture agreement with Gowest and Romex on October 21, 1987. Under the terms of the agreement, New Texmont could earn a 50% interest in the Gowest-Romex Property by expending $400,000 prior to June 30, 1989 (Pearson, 1989).

On March 17, 1989 Gowest purchased Romex’s 17% interest in 14 claims P 508389 to 508402 (situated in Tully and Prosser townships) resulting in a 50:50 joint venture between Gowest and New Texmont.

In 1989 New Texmont and Intex Mining Co. Ltd (50% owned by New Texmont) entered into a joint venture agreement with Zenmac Zinc Ltd. (an affiliated corporation) to finance the continued drilling and underground exploration of the Frankfield East Deposit occurring on both the Gowest / New Texmont and Intex properties . Drilling by the Intex / Texmont / Zenmac joint venture in 1988 amounted to 5,350 m at 20 sites (DDH’s 88-1 to 88-19 and 88-21).

Two holes (89-GO-1 and 89-GO-3, totaling 1,216 m) were drilled in 1989 to test the Frankfield East Deposit at depth. 89-GO-3 returned an assay of 5.45 g/t Au over a core length of 22.65 m at an approximate depth of 488 m vertical.

In 1990, the Gowest / New Texmont joint venture completed diamond drill holes 90-GO-4 (666.6 m) and 90-GO-5 (715.4 m), to test areas approximately 61 m east and west of previous gold intersections of 5.45 g/t Au over 22.65 m and 4.79 g/t over 8.07 m (89-GO-3). Drill hole 90-GO-4 returned gold values of 6.30 g/t over 4.9 m and 3.33 g/t over 10.42 m at a vertical depth of 518 m. Drill hole90-GO-5 returned a gold assay of 2.39 g/t Au over 11.7 m at a vertical depth of approximately 564 m.

In 1990, Cyprus Gold (Canada) Ltd. (Cyprus) acquired an option to earn a 70% interest in the Frankfield East Deposit from the Gowest / New Texmont joint venture, and the neighbouring Texmont deposit from Intex and Frankfield. The exploration program consisted of core re-logging and sampling of 15 previous drill holes (209 samples), magnetic and HLEM surveys and diamond drilling of 7 holes totalling 3,638 m (T-91-1 to T-91-6 and T-91-9). The object of the drilling was to test the gold mineralization potential of the Frankfield East Deposit to a depth of 600 m. Drill hole T-91-6 penetrated the Main Zone at approximately 600 m and returned a value of 2.37 g/t Au over a core length of 3.0 m, indicating a significant depth potential for the Main Zone mineralization. Cyprus concluded that the Frankfield East Deposit is approximately 480 m long at the bedrock surface which diminishes with increasing depth along a steep westward plunge to about 200 m strike length at a depth of 300 metres. Cyprus dropped the option in 1991.

In 2004, the Gowest / New Texmont joint venture proceeded with a diamond drilling program which consisted of 23 holes totaling 6,538 m (GW04-01 to GW04-22 and GW04-25). The diamond drill program was designed to intersect the northerly dipping mineralized horizons of the Frankfield East Deposit at 50 m intervals, both horizontally and vertically, between a depth of 100 and 300 m. The 2004 drill program is discussed in Section 10. Two drill holes (GW04-22 and GW04-25) successfully intersected the target at about a 300m depth. At the end of this drill program the Main Zone gold mineralization (M1 & M2) was recognized as being 600 m long, to a drilled depth of 300 m, with indications that the gold mineralization continues to a depth of at least 600 m. The steeply north dipping Main zone (-71°) appeared to have an average width of 3.7 m in the eastern part and 8.3 m, in the western part. Assay results from mineralized zones in the hangingwall of the Main zone (Quartz Breccia zones B1 and B2) were beginning to show potentially economic mineralization, but were poorly understood.

6.2. PROSSER BLOCK

Work on the Prosser Block is included in Table 6-1. Much of the geophysical work is old and has probably been superseded by more recent Government work.

TABLE 6-1 WORK HISTORY PROSSER PROPERTY				
YEAR	**AFRIFILE #**	**COMPANY**	**WORK TYPE**	**RESULTS**
1966	42A14SE0106	CANICO	AEM, AMAG	Airborne survey covering Abitibi-Price claims in ten townships including Prosser Twp.
1964-1966	42A11NE0188	KENILWORTHMINES	DD	Ground Mag & EM followed by one drill hole (93.5 m) no assays reported.
1968	T1448	TEXMONT MINES	EM, MAG	Ground Mag & VLEM.
1970	42A14SE8398	McINTYRE PORCUPINE MINES	COMP	Geophysical and Geological Compilation
1975	42A11NE0191	GEOEX LTD	EM	Ground VLEM over 4 claims in Central Prosser Twp.
1988	42A11NE0181	FALCONBRIDGE	EM, MAG	Ground HLEM & Mag over 4 claims in Central Prosser Twp.
1999	42A11NE0097	PENTLAND FIRTH	EM, MAG	Ground HLEM & Mag over 4 claims in Central Prosser Twp.
1999	42A11NE2006	PENTLAND FIRTH	IP	IP survey over 4 claims central Prosser. Weak conductor located.
2001	42A11NE2011	PEGG C.	GEOL,GEOC, EM	Geological mapping located intermediate to mafic volcanic outcrops in the south end. VLF survey conducted. Soil sampling (70samples) over VLF survey grid. No assay data for sampling.
2005	2000000976	PEGG C.	GEOC	Soil pH survey- 70 samples
2011		GOWEST GOLD	GEOL	Geological mapping confirmed above results.

6.3. TULLY EAST CLAIMS

A summary of the previous assessment work on Tully East claim block is set out in Table 6-2. The Tully East claim block is contiguous with the Frankfield Block.

TABLE 6-2 WORK HISTORY TULLY EAST PROPERTY

YEAR	AFRI FILE #	COMPANY	WORK TYPE	RESULTS
1964	42A11NE0240	DAERING EXPLORERS CANADIAN AUSTRALIAN	DD	5 ddh, 65-1 to 65-5 totaling 5,839 m in central Tully Twp., no assay data.
1964	42A11NE0070	DAERING EXPLORERS CANADIAN AUSTRALIAN	MAG,EM	Mag and HLEM over 8 claims.
1964	42A11NE0071	LABOW	MAG,EM	Mag and HLEM over 2 claims in central Tully Twp
1965	42A11NE0041	HOLLINGER CONSOLIDATED	DD	1 ddh, LT-2 (183.5 m) in western Tully Twp, no assay data. (Guidoccio claims)
1966	42A14SE0106	ABITIBI-CANICO	COMP	Geophysical and Geological compilation of Tully Twp.
1967	42A11NE0069	MESPI MINES	MAG,EM	Mag and VLEM survey over 4 claims in west central Tully Twp., 2 outcrops located in central part of property.
1967	42A11NE8616	KEEVIL MINING	GEOP	Mag and VLEM over 4 claims.
1968	42A14SE0159	BW LANG MESPI MINES	AEM, AMAG,MAG .EM	Airborne Mag, Airborne EM , ground Mag and ground VLEM survey over 2 claim groups in west central Tully Twp.
1968	42A11NE0067	NEW CALUMET MINES	MAG,EM	Ground mag and EM. (Guidoccio claims)
1969	42A11NE0048	MCINTYRE PORCUPINE MINES	DD,MAG,E M	4 ddh, 022-69-1 to 022-69-4 (471.5 m) in SE Tully Twp., no assay data.
1969	42A14SE0148	NORANDA	MAG,EM	Mag and VLEM survey over 14 claims in south central Tully Twp.
1969	42A14SE0365	NORANDA	MAG,EM	Mag and VLEM survey over 4 claims in south central Tully Twp.
1969	42A11NE0058	MCINTYRE PORCUPINE MINES	MAG,EM	Mag and EM survey over 15 claims
1969	42A11NE0062	NORANDA	MAG,EM	Mag and VLEM survey over 7 claims.
1969	42A11NE0061	NORANDA	MAG,EM	Mag and VLEM survey over claims in central Tully Twp.
1969	42A11NE0066	NORANDA	MAG,EM	Mag and VLEM survey over 19 claims in east central Tully Twp. and 3 claims Little Twp. (Guidoccio claims)
1970	42A11NE0060	LAROMA-MIDLOTHIAN	MAG,EM	Mag and EM over 16 claims.
1971	42A11NE0049	LAROMA-MIDLOTHIAN	DD	1 ddh, T667-1 (137.2 m), central Tully Twp.
1971	42A11NE0045	LAROMA-MIDLOTHIAN	DD	1 ddh, T-1 (153.3 m), vertical hole in southeast Tully Twp., no assay data.
1971	42A11NE0057	TEXMONT MINES	MAG,EM	Mag and EM on 11 claims in the SE corner of Tully Twp.
1972	42A11NE0176	TEXAS GULF	MAG,EM	Mag, horizontal and vertical loop EM over 4 claims in the SE corner of Tully Twp
1972	42A14SE0174	DOME EXPLORATION	MAG,EM	Mag and Turam EM survey over 5 claims SE Tully Twp. (Guidoccio claims)
1974	42A14SE0170 42A11NE0055	QUESTMONT MINES	MAG,EM	Mag and EM over 8 claims in south central Tully Twp.
1974-76	42A11NE0037	QUESTMONT MINES	RC,DD	10 RC holes, 74-1 to 74-11 in south central Tully Twp., best values in drill hole 74-10 of 1.3 gpt Au over 3.0 metres. 5 ddh, 76TT-1 to 76TT-4 in south central Tully Twp.

1975	42A11NE0052	QUESTMONT MINES	EM	VLEM over 36 claims SW Tully Twp.
1977	42A11NE0035	ST.JOSEPH EXPLORATION	MAG,EM	Mag and HLEM survey over 11 claims SE Tully Twp. (Guidoccio claims)
1978	42A11NE0235	ST JOSEPH EXPLORATION	DD	4 ddh totaling 502.6 m, 134-1,1A,1B and 134-2. No significant gold assays.(Guidoccio claims)
1978	42A14SE0126	NORANDA-MATTAGAMI LAKE MINES	DD	2 ddh, T1-78-2 and 3 (389.8 m) in NE Tully Twp. NSV. Minor IP stacked sections on ddh section, no IP survey filed for assessment. (GuIdoccio claims)
1978	42A16SE8615	AMOCO PETROLEUM	DD	2 ddh, 5A-1 and 5A-2 (total of 331.9 m) in SE Tully Twp, sampling but no assay values.
1980	42A11NE0027	ROSARIO RESOURCES	DD	6 ddh, T80-1 to 6 totaling 1,830 m in south central Tully Twp. Partial assays reported no significant gold. 1 ddh T80-11 (137.2 m) was drilled in the north part of Tully East no significant gold reported.
1980	42A11NE0030	ROSARIO RESOURCES	DD	1 ddh T80-14 (190.5 m) in SE Tully Twp. No significant gold assays.
1980	42A11NE0032	NORCEN ENERGY RESOURCES	DD	1 ddh, TP1980-1 (172 m), no significant gold reported. Mag & HLEM, 444 and 1777 Hz.
1980	42A11NE0025	ROSARIO RESOURCES	EM	Max-Min survey over portions of claim groups in south Tully Twp.
1980	42A14SE0122	NORCEN ENERGY	AEM	Airborne INPUT electromagnetic survey by Questor Surveys Ltd over Tully and Little Townships.
1980	42A11NE0024	NORCEN ENERGY RESOURCES	MAG,EM	Mag & EM
1981	42A11NE0019	LACANA	RC	32 RC holes, LBT-01 to 16 and LBT-18 to 33. High value of 14260 ppb Au in hole LBT-05, additional anomalous values in the 1700 to 4000 ppb Au range in holes LBT-02, LBT-03, LBT-11, LBT-12 and LBT-13.
1982	42A11NE0013 42A11NE0022	LACANA	DD,MAG, EM	2 ddh, T82-15, 15A, (totalling 276.8 m) was drilled in the north part of Tully East no significant gold reported. Ground Mag and max-min survey.
1982	2531	KIDD CREEK MINES	RC	3 RC holes, H-82-96 to 98 in SW Tully Twp. No assay values.
1983	2750	COMINCO	RC	25 RC holes, TO-1 to 12, TO-12A, TO-13 to TO-20, TO-22 to 23 and TO-25 to 26. No assay values.
1983	42A11NE0011	LACANA	DD	1 ddh, T83-19b, (totalling 188.7 m) was drilled in the north part of Tully East no significant gold reported.
1985	42A14SE0103	TEXAS GULF- KIDD CREEK MINES	MAG,EM	Ground mag and Max-Min over 8 claims SE Tully Twp. Airborne Mag over 8 claims SE Tully Twp.
1985	42A11NE0301	COMINCO	MAG,EM	Ground mag and EM. (Guidoccio claims)
1987	42A11NE0006	ESSO MINERALS	MAG,GEOL	Magnetic survey and Geological mapping on 1 claim central Tully Twp.
1989	42A14SE0101	HOMESTAKE	MAG,EM	Mag and Max-Min survey over 24 claims in SE Tully Twp.(Guidoccio claims)
1990	42A11NE0002	C.S. HANNINAN	MAG,EM	Mag and VLF survey over 11 claims SW Tully Twp.(Guidoccio claims)
1991	42A11NE0004	HOMESTAKE	DD	1 ddh T91-1 (372.4 m) in central Tully Twp. No significant gold assays.
1992	42A11NE0079 42A11NE8618	C.F.DESSON	DD	1 ddh 92CD-1 (207.3 m) in SE Tully Twp. No significant gold assays.(Guidoccio claims)
1993	42A11NE0043 42A11NE0078	C.F.DESSON	DD	1 ddh 93CD-2 (233 m) in SE Tully Twp. No significant gold assays.(Guidoccio claims)
1995	3531	C.F.DESSON	DD	1 ddh 95CD-3 in SE Tully Twp. NSV. Minor FP intrusions in 95CD-3. (Guidoccio claims)
1995	42A11NE0082	D. GAMBLE	MAG,EM	Mag and Max-Min survey over 12 claims in east central Tully Twp. (Guidoccio claims)
1997	42A11NE0093	D. GAMBLE	DD	1 ddh LD10/18 97-1 in east central Tully Twp. No significant gold values.(Guidoccio claims)

1997	42A11NE2002 42A11NE2003	KINROSS GOLD	MAG,EM	Mag survey over 73 claims SE Tully Twp.
1999	42A14SE2004	PENTLAND FIRTH	MAG	Mag survey over 12 claims in south central Tully Twp.
1999	4211	KINROSS GOLD	GEOP	IP survey over selected areas on 73 claims SE Tully Twp.
2001	42A11NE2001	FALCONBRIDGE	MAG,EM	Mag and Max-Min I-5 survey over portions of 2 claim groups in south central Tully Twp.
2001	42A11NE2001	FALCONBRIDGE	DD	1 ddh TU16-01 in south central Tully Twp.
2002		KINROSS GOLD	DD	6 ddh, TU02-1 to 6 totaling 1,134 m in central Tully Twp., following up IP anomalies, no significant values.
2002		KINROSS GOLD	COMP	Emerald Services completed an exploration work compilation of geophysics, geology, geochemistry and diamond drilling in Tully Twp.
2005		KINROSS GOLD	MAG & IP	16.3 line km of ground magnetic and IP surveying in west central portion of the existing property.
2007	20000746 20000747	KINROSS GOLD	DD	1 ddh , TU07-01 (200m) on claim 1160197. Tested IP anomaly which was thought to be fault gouge at sediment/ultramafic contact. 2 lithochemical samples taken.
2011		GOWEST GOLD	AMAG,AEM , GEOC	Helitem EM amd Mag conducted by Fugro Airborne Surveys over the Timmins North Project. Soil Gas Hydrocarbon Survey (SGH) over the southeast portion of the Tully East property.

It is apparent that a significant amount of work has been carried out over many years. A full assessment of the results of the various programs will take some time.

6.4. TULLY NORTH CLAIM GROUP

This claim group is 2 km northeast of the Frankfield Block and previous assessment work on the group is detailed in Table 6-3.

TABLE 6-3 WORK HISTORY, TULLY NORTH PROPERTY

YEAR	AFRI FILE #	COMPANY	WORK TYPE	RESULTS
1968	42A14SE0157	CINCINNATI PORCUPINE MINES	AEM, MAG, EM	Prior to 1968 an airborne EM survey was conducted.. Mag and VLEM over 7 claims.
1969	42A14NE0236	CINCINNATI PORCUPINE MINES	DD	3 ddh, T-69-1 to 3 in NW Tully Twp., no assay data. Holes intersected a NW trending carbonate zone in basalts on the south side of an ultramafic body. Apparently a gold value was encountered in either hole 1 or 2.
1977	42A14SE0129	WESTERN MINES	AEM	Airborne INPUT electromagnetic survey by Questor Surveys Ltd over 6 claims west central Tully Twp., which covers the SW 1/4 of the Tully North Property.
1982	42A14SE0107	NEWMONT EXPLORATION	EM, MAG, IP	Mag, Max-Min HLEM and IP surveys over the entire Tully North Property.
1983	2451	NEWMONT EXPLORATION	DD	11 ddh MN81-1, MN81-3 to 12, in NW Tully Twp. Follow up to Cincinnati Porcupine Mines drilling. Multiple gold values with best value of 7.1 gpt Au over 1.5 metres in hole MN83-1. The gold zone is characterized by disseminated arsenopyrite-pyrite cut by ankerite veinlets and hosted in a broad zone of carbonated-silicified basalts.
1987	42A14SE0102	ESSO MINERALS	GEOL, EM	Geological mapping on present claim 4254623, no outcrop on the claim but 4 pillowed mafic volcanic outcrops just south of SW corner.. HLEM survey but results not reported.
1990	42A14SE0100	L.SALO	EM, MAG	Mag and VLF survey over present claim 4254623.

2011		GOWEST GOLD	AMAG,AEM	Helitem EM amd Mag conducted by Fugro Airborne Surveys over the Timmins North Project.

6.5. WARK 1 CLAIM GROUP

This is the eastern most of two claim groups in Wark Township and is located 2.5 km southwest of the Frankfield Block. Previous assessment work is documented in Table 6-4.

TABLE 6-4 WORK HISTORY, WARK 1 PROPERTY

YEAR	AFRI FILE #	COMPANY	WORK TYPE	RESULTS
1964	42A11NW0008	NATIONAL EXPLORATION	EM, MAG. GEOL	Ground Mag & VLEM surveys and geological mapping over NW corner of property.
1964	42A11NW0002	NATIONAL EXPLORATION	DD	8 ddh, 64-1 to 8 totalling 1015 m tested 5 conductive zones. Some assaying for gold but only trace values. Drilling encountered intermediate volcanics and mafic volcanics.
1964	42A11NE0564	NORTH AMERICAN RARE METALS	EM, MAG	Ground HLEM & Mag over South half of the property.
1966	42A11NE0570	NORTH AMERICAN RARE METALS	DD	1 ddh NAR-11 (128.6 m) on the present property. Nio sampling reported.
1969	42A11NE0561	MESPI MINES	EM	Ground VLEM over central-north part and outlined 3 conductors.
1970	42A11NE0562	FALCONBRIDGE	EM, MAG	Ground VLEM & Mag over South half of the property.
1972	42A11NW0004	TEXAS GULF	EM, MAG	Ground HLEM & Mag over the NW corner of the property.
1975	42A11NE0566	McINTYRE PORCUPINE MINES	DD	3 ddh, 051-75-5 to 7 totaling 471 m. No assay data. One hole intersected dacitic tuffs interbedded with argillites, the other cut quartz veins in graphitic argillite above a peridotite and the third was lost in overburden.
1980	42A11NE0186	P. HUNKIN	EM, MAG	Ground VLEM & Mag over north half of the property.
1981	42A14SE0208	PLACER	AMAG	Airborne Magnetic survey conducted by Questor Surveying covering part of Prosser and Wark townships.
1983	42A11NE0553	COMSTATE RESOURCES	AEM	Airborne Mark VI INPUT survey conducted by Questor Surveying covering Prosser, Wark and Murphy townships. No INPUT anomalies detected.
1985	42A11NE0185	GOLDEN RANGE RESOURCES	GEOC	Seven hole wacker till sampling program in the NW corner of the Property. No anomalous gold or base metal values encountered. Overburden depths of 10 to 25 m.
1985	42A11NE0183	GOLDEN RANGE RESOURCES	EM, MAG	Ground VLF & Mag over north half of the property.
1990	T3386	COMINCO	EM, MAG	Mag and Max-Min II survey over 5 claims in NE Wark Twp. and 8 claims in SE Prosser Twp. 4 weak EM conductors outlined.
1997	42A11NE0097	PENTLAND FIRTH	EM, MAG	Ground HLEM & Mag over the north half of the property. Three HLEM conductors detected.
1999	42A11NE2006	PENTLAND FIRTH	IP	IP survey over the north half of the property. Three strong IP responses 2 of which coincide with the HLEM conductors.
2001	42A11NE2011	PEGG C.	GEOL,EM	Geological mapping and VLF conducted on north-central part of existing property. No outcrops found.
2011		GOWEST GOLD	AMAG,AEM, GEOC	Helitem EM and Mag conducted by Fugro Airborne Surveys over the Timmins North Project Soil Gas Hydrocarbon Survey (SGH) over entire property.

6.6. WARK 2 CLAIM GROUP

This claim group is situated 2.5 km west of the Wark 2 claim group and previous assessment work is summarized in Table 6-5.

TABLE 6-5 WORK HISTORY, WARK 2 PROPERTY

YEAR	AFRI FILE #	COMPANY	WORK TYPE	RESULTS
1964	42A11NW0527	GLENN EXPLORATIONS	EM, MAG, DD	Ground Mag & VLEM surveys over north part of the southern claim. Numerous weak EM conductors detected. Two holes G-1 to G-2 totaling 495 m drilled (no logs in file). Hole 1 tested the strongest EM conductor. Holes encountered sediments and intermediate volcanics, but EM conductors not explained. No economic mineralization reported.
1964	42A11NW0535	WINDFALL OIL & MINES LTD	DD	3 ddh, holes 5, 7 and 8 totaling 475 m on the NE claim. Holes cut ultramafic volcanics, 1 assay reported nil gold and base metals.
1964	42A11NW0536	PCE EXPLORATION LTD.	DD	2 ddh, holes P-3 and P-4 totaling 293 m on the western claim. Holes cut ultramafic volcanics and felsic to intermediate volcanics, 2 assays reported trace gold.
1969	42A11NE0561	MESPI MINES	EM	Ground VLEM over south half of the central claim. No conductors were detected.
1970	42A14SE8398	McINTYRE PORCUPINE MINES	COMP	Geophysical and Geological Compilation
1971	42A11NW8400	TEXAS GULF	EM, MAG	Ground HLEM & Mag over the north half of the central claim. One weak conductor.
1981	42A14SE0208	PLACER	AMAG	Airborne Magnetic survey conducted by Questor Surveying covering part of Prosser and Wark townships.
1989	42A11NW0502	FALCONBRIDGE	EM, MAG	Ground HLEM & Mag over west half of the central claim. One weak EM conductor.
1993	42A11NW0072	FALCONBRIDGE	DD	1 ddh W62-01 (269 m) on the SW1/4 of the central claim. Hole intersected argillite followed by mafic breccia and then mafic flows. 4 assays reported nil gold and base metals along with 8 whole rock samples
1996	42A11NW0068	MEUNIER-PEGG	TR	Manual stripping off of overburden from two outcrop areas of mafic volcanics on the western claim.
1998	42A11NW2005	MEUNIER	TR	same as above
2001	42A11NE2011	PEGG C.	GEOL,EM	Geological mapping and VLF conducted on the north half of the central claim. No outcrops were found.
2011		GOWEST GOLD	AMAG,AEM, GEOC	Helitem EM and Mag conducted by Fugro Airborne Surveys over the Timmins North Project. Soil Gas Hydrocarbon Survey (SGH) over western half of the property.

6.7. GOWAN BLOCK

This is the southernmost claim block in the North Timmins Project and is located 2.4 km south of the Frankfield Block. Previous exploration on the property is detailed in Table 6-6.

TABLE 6-6 WORK HISTORY, GOWAN PROPERTY

YEAR	AFRI FILE #	COMPANY	WORK TYPE	RESULTS
1965	42A11NE0531	NEW CALUMET MINES LTD.	EM, MAG	Ground Mag & VLEM.
1982	42A11NE0508	COMINCO	RC	2 RC drill holes, GO-124 & 125. hit bedrock at 14 m & 29 m depths. No assay data. No bedrock descriptions.

1983	42A11NE0509	COMINCO	RC	6 RC drill holes, GO-133 to 139. all hit bedrock at16 to 23.5 m depths. No assay data. Bedrock descriptions too vague to determine rock type.
2011		GOWEST GOLD	AMAG,AEM, GEOL	Helitem EM amd Mag conducted by Fugro Airborne Surveys over the Timmins North Project Geological mapping confirmed the 2001 mapping.

6.8. PIPESTONE EAST GROUP

This claim group is comprised of 12 unpatented mineral claims under option from Transition and 12 unpatented mineral claims staked by Gowest Gold. The group is located in southeastern Little Township and northwestern Evelyn Township. A summary of the previous assessment work on the Pipestone East claim block is set out in Table 6-7.

TABLE 6-7 WORK HISTORY, PIPESTONE EAST PROPERTY

YEAR	AFRI FILE #	COMPANY	WORK TYPE	RESULTS
1964	42A11NE0929	FIDELITY MINING	EM, MAG	Ground VLEM & Mag over part of present claims 4270231 and 4270234
1964	42A10NW0008	AUGUSTUS EXPLORATION	EM, MAG	Ground Turam EM & Mag over part of present claims 4270235 and 4270237.
1964	42A11NE0550	ALDAGE MINES	EM, MAG	Ground Turam EM & Mag over part of present claims 4270236 and 4270238.
1964	42A11SE0164	HOLLINGER	EM, MAG	Ground Turam EM & Mag over part of present claim 4270230.
1964	42A11NE0551	MARCH MINMERALS	EM, MAG	Ground VLEM & Mag over part of present claims 4262511 and 4267267
1965	42A10NW0009	AREA MINES	EM, MAG	Ground VLEM & Mag over part of present claims 4270239 and 4267266
1965	42A11NE0550	TREND EXPLORATION	EM, MAG	Ground VLEM & Mag over part of present claims 4253004 and 4262511
1965	42A11SE0027	SHIELD EXP & DEV	EM, MAG	Ground Turam EM & Mag over part of present claims 4270232 and 4270233.
1966	42A11NE0134	JASCO PROSPECTING	DD	One hole JL-1 (31.5 m) drilled on outcrop cut carbonate altered andesite. No assays reported. Claim 4257021.
1967	42A11NE0813	HOLLINGER	DD	One hole E-1A (140.5 m) drilled 137.3 m of overburden then hit ultramafic. One very low Ni assay reported. Claim 4257023.
1967	42A11NE0812	HOLLINGER	DD	One hole E2 (70.3 m) drilled overburden did not hit bedrock. No assays reported. Claim 4262512.
1968	42A11NE0121	NORANDA	EM, MAG	Ground VLEM & Mag over part of present claim 4270233.
1968	42A10NW0516	HOLLINGER	DD	One hole E3 (119.8 m) drilled overburden till 104 m then finished in ultramafic. Three Ni samples but no assays reported. Claim 4253006.
1968	42A11NE0931	McINTYRE PORCUPINE MINES	EM, MAG, GEOL	Ground VLEM & Mag and geological mapping over part of present claims 4257021 and 4270231. One outcrop of intermediate volcanics located same as the Jasco Prospecting outcrop.
1969	42A11NE0119	NORANDA	EM, MAG	Ground VLEM & Mag over part of present claim 4270231.
1970	42A10NW0695	HOLLINGER	DD	One hole E4 (103 m) hole cut dacitic tuff followed by ultramafic .No assays reported. Claim 4253003.
1972	42A11NE0918	TEXAS GULF	EM, MAG	Ground VLEM, HLEM & Mag over part of the present claim 4270231. No conductors detected.
1973	42A14SE0402	DR DERRY	EM, MAG	Ground Turam EM & Mag over part of present claim 4270230.
1973	42A14SE0403	NORANDA	EM, MAG	Ground VLEM & Mag over part of present claim 4270230.
1973	42A11NE0116	DR DERRY	EM, MAG	Ground Turam EM & Mag over part of present claim 4270232.

1978	42A11NE0114	NORANDA	DD	2 ddh, holes TK-1-78-4 and 5 totaling 411.4 m on present claim 4270233. Holes cut intermediate volcanics and sediments. Holes sampled and no anomalous Au, Ague and Zn values.
1978	42A15NE0015	AMOCO PETROLEUM	DD	1 ddh, 5-1 (172.8 m) drilled on claim 4257021. It cut ultramafic volcanics followed by mafic volcanics that contained graphitic sediment units. No assay data.
1978	42A11NE8377	AMOCO PETROLEUM	DD	1 ddh, 5-2 (158 m) drilled on claim 4257022. It cut mafic volcanics. Two holes (18-1 & 18-2) totaling 294.7 m on claim 4270237. Holes intersected mafic volcanics, sediments and ultramafic volcanics. No assay data.
1968	42A11NE0114	NORANDA		
1979	42A11NE0712	ROSARIO RESOURCES	EM	HLEM, max-min 1777,444 Kz. On claims 4257021 and 4257022.
1979	42A15SW0151	NORCEN ENERGY	AMAG	Airborne Magnetic survey by Questor Surveys Ltd over several townships including the property's northern claims in Little TWP.
1980	42A14SE0122	NORCEN ENERGY	AEM	Airborne INPUT electromagnetic survey by Questor Surveys Ltd over Tully and Little Townships.
1980	42A11NE0111	LACANA MINING	DD	1 ddh, T80-7 (176 m) drilled on claim 4257021. It cut mafic volcanics that contained graphitic sediment units. Core and sludge sampling with low gold values.
1983	42A10NW0027	L JOLIN	MAG	Ground Mag over part of present claims 4270235 & 4270236
1984	42A11NE0003	COMINCO	MAG	Ground Mag over part of present claim 4270238.
1986	42A15SW8860	ANGELA DEVELOPMENTS	AEM, AMAG	Airborne survey by Ferderber Geophysics covering several townships including Evelyn & Little Townships.
1988	42A10NW0027	ALLERSTON	MAG	Ground Mag over part of present claim 4253006
1991	42A11NE0999	FALCONBRIDGE	AEM, AMAG, AVLF	Helicopter survey by Aerodat Ltd covering several townships including Evelyn & Little Townships.
1993	42A10NW0035	HUTTERI	EM, MAG	Ground HLEM & Mag over present claim 4253006.
1993	42A11NE0102	PEPLINSKI	MAG	Ground Mag over part of present claim 4270234.
1996	42A10NW0034	ARISTA RESOURCES	AMAG, AVLF	Helicopter survey by Aerodat Ltd covering part of Evelyn Township. Geological and geophysical compilation.
1997	42A10NW0040	OREZONE RESOPURCES	DD	One hole E3 (161.7 m) drilled overburden till 67 m then intersected sediments interbedded with andesite flows. Nine core samples returned nil gold values. Claim 4270236.
1998	42A11NE2001	WIN-ELDRICH MINES	MAG	Ground Mag over parts of 4 present claims Se of Lizard Lake Evelyn Twp.
2004	20001019	INCO/AURO PLATINUM	EM, MAG, GEOL	Deep 2002 OGS Megatem conductor was covered by a 6 claim unit property. Mapping indicated no outcrop. Ground Mag and HLEM surveys, no conductor detected so overburden deeper than 100 m. Claim 4257024.
2011		GOWEST GOLD	AMAG,AEM, GEOC	Helitem EM and Mag conducted by Fugro Airborne Surveys over the Timmins North Project. Soil Gas Hydrocarbon Survey (SGH) over the entire property.

It is apparent that a significant amount of work has been carried out over many years on the claim blocks (properties) that make up the Gowest North Timmins Project. A full assessment of the results of the various programs will take some time.

7. GEOLOGICAL SETTING AND MINERALIZATION

7.1. REGIONAL AND LOCAL GEOLOGY

The following has been extracted from Harron (2006) and Bradshaw (2008) with minor edits.

Tully Township, situated in the Abitibi Greenstone Belt ("AGB"), is underlain by Neoarchean supracrustal rocks of the Abitibi Subprovince of the Canadian Shield. Supracrustal rocks are divided into tectonostratigraphic units called assemblages for descriptive purposes. The reader is referred to Jackson and Fyon (1991) for a full discussion of the Archean geology of the Superior Province and Ayer et al. (2002) for a more recent interpretation of the AGB geology. Gold deposits are structurally controlled and are widely distributed within the AGB, but all of the large deposits occur within 2 km of the Destor-Porcupine Fault Zone, the Pipestone Fault Zone and the Cadillac-Larder Lake Shear Zone. As of 1990, 70% of all gold production in Canada has come from the AGB. Gold production plus reserves for AGB deposits (Ontario and Quebec) calculated in 1991 were estimated at about 615 million tonnes (678 million tons) grading 7.54 g/tonne (0.22 oz/ton) Au.

Two dominantly volcanic assemblages and one dominantly sedimentary assemblage underlie Tully Township (Ayer and Trowell, 2001). To the west of the northwest-trending Buskegau River Fault, the Porcupine (sedimentary) assemblage (2696-2675 Ma) underlies the extreme southwestern corner of the township and unconformably overlies the Kidd-Munro (volcanic) assemblage (2719-2711 Ma). The Kidd-Munro underlies the central part of the township and is in fault contact to the northwest with the upper Tisdale (volcanic) assemblage (2710- 2703 Ma). To the east of the Buskegau River Fault Kidd-Munro assemblage rocks underlie the extreme southeastern corner of the township. Upper Tisdale assemblage rocks overlie the Kidd-Munro assemblage to the north, and possibly interfolded Porcupine assemblage rocks near the contact between these two tectonostratigraphic units.

The Kidd-Munro assemblage is divisible into two distinct suites:

- A tholeiitic to komatiitic suite, which consist of komatiites, magnesium and iron-rich tholeiites; and;

- A calc-alkaline suite consisting of intermediate to felsic pyroclastic rocks, including FIIIb type rhyolites (Lesher, et al, 1986).

Rare sedimentary rocks are generally confined to narrow interflow units within the mafic volcanic rocks. Synvolcanic felsic intrusions and later diabase dykes intrude the sequence. The calc-alkaline portion of the assemblage is host to the Kidd Creek volcanogenic massive sulphide (VMS) deposit and several smaller VMS deposits located in Munro Township. The ultramafic / mafic suite is host to Gowest's Frankfield East gold deposit and other gold deposits within Tully Township.

A Geological Survey of Canada ("GSC") regional airborne magnetic survey shows considerable relief within the Kidd-Munro assemblage (Dumont et al. 2002a, b). Magnetic highs appear to be coincident with unaltered ultramafic flows and magnetic lows appear to be coincident with mafic flows and altered ultramafic flows. The magnetic patterns also appear to define west verging folds, or possibly transposed stratigraphy along contact parallel faults. Airborne electromagnetic patterns appear to be following stratigraphic horizons, and drill hole data indicates that most conductive horizons are graphitic responses.

The upper Tisdale (volcanic) assemblage occurs east and west of the Buskegau River Fault in the northeastern part of Tully Township and remote from the Frankfield Gold Project. The basal mafic / ultramafic portion of this assemblage is host to the major gold deposits of the Timmins camp, such as the Hollinger, McIntyre and Dome mines. The upper Tisdale assemblage disconformably overlies the Kidd-Munro assemblage and is comprised of intermediate and felsic, epiclastic and pyroclastic volcanic rocks of calc-alkaline affinity. The magnetic pattern over this assemblage is subdued, with low amplitude magnetic responses over stratiform gabbroic sills. Electromagnetic (“EM”) responses within this assemblage are diffuse and of low conductivity. In the northwestern part of Tully Township, a zone of high conductivity EM responses caused by graphite and massive pyrrhotite marks the contact between the Tisdale and Kidd-Munro assemblages.

Porcupine assemblage rocks unconformably overlie the Kidd-Munro assemblage immediately south of the Frankfield Block. The sedimentary rocks are composed predominantly of fine-grained turbiditic sedimentary rocks with minor graphitic argillite and conglomerate horizons. A detrital zircon U/Pb age of 2698 Ma (Heather et al., 1995) for similar sediments at the Kidd Creek Mine defines a maximum age of the assemblage. Porcupine assemblage rocks are also thought to occur east of the Buskegau River Fault in the east central part of the township (Berger, 2000). The magnetic pattern associated with this assemblage is subdued with stratiform electromagnetic responses.

Structural features of the bedrock are mainly interpreted from airborne magnetic surveys. Stratigraphic units as represented by their magnetic signatures generally trend east-northeast within the Kidd-Munro assemblage. This trend is also characterized by a well-developed penetrative foliation. Fold axes also appear to trend east-northeast as noted by reversals in younging directions determined from flow features. Stratigraphy parallel shear zones, such as at the Frankfield East gold deposit are developed at some lithological contacts. Extensional lineations developed in the shear zones are moderately northeast plunging, a direction that is similar to lineations observed in the Timmins area (Pyke, 1982) and Hoyle Pond gold mines geology (Berger, 2000). This observation implies a similar and contemporaneous geodynamic process and possibly a similar metallogenic connotation, suggesting an untested gold potential along these structures in Tully Township.

Within the upper Tisdale assemblage, magnetic patterns indicate northwest-trending lithologies cut by east-northeast-trending late faults. Stratigraphic facings indicate younging directions towards the northeast within this assemblage (Berger, 2000). The distribution of EM conductors in the northwestern part of Tully Township suggests large amplitude northwest-trending folds.

7.2. PROPERTY GEOLOGY

The following geology of the Frankfield Block has been extracted from Harron (2006) and Bradshaw (2008) with minor edits.

Holocene organic deposits of peat and black muck cover much of the map area. Underlying the organic deposits are a really extensive Quaternary glaciolacustrine deep water varved silts and clays of the Barlow–Ojibway Formation up to several metres thick overlying Matheson Till.

The bedrock geology of the Project is mainly derived from drill core observations and geophysical interpretations due to the extensive overburden and swamp lands characteristic of the region. The bulk of the property is underlain by tholeiitic basalt flows and komatiitic basalt and peridotite flows of the Kidd-Munro assemblage (Figure 7-2).

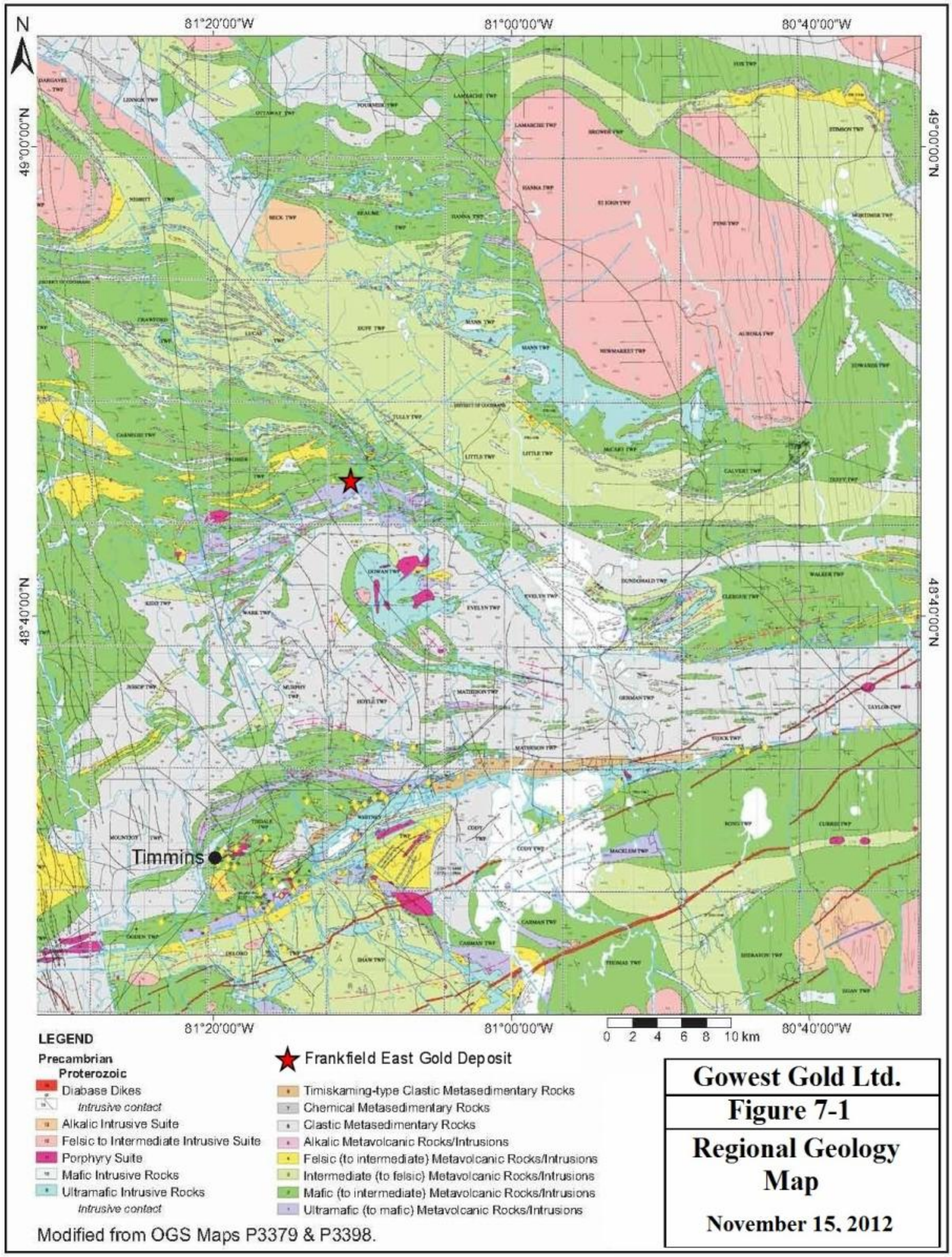

FIGURE 7-1 REGIONAL GEOLOGY, NORTH TIMMINS PROJECT

In detail, the Kidd-Munro assemblage on the property consist of magnesium-rich and iron-rich tholeiites, which range from pale green-gray to dark green in colour. Textures include massive and pillowed flows with abundant flow top breccia and occasional variolitic and spherulitic horizons. Drilling also suggests that thin (5-30 m) komatiitic peridotite flows are intercalated in the tholeiitic volcanic sequence. Thin (<10 m) units of pyritic graphitic argillite interflow sediments are commonly at or close to the contacts of the komatiitic peridotite flows in the tholeiitic volcanic sequence. Quartz-calcite veinlets cut the various units at all angles. Minor amounts of pyrite and pyrrhotite are common throughout the sequence and concentrations are slightly enhanced near pillow rims and siliceous flow top breccias. Depositional indicators demonstrate a steeply north dipping and north younging direction for the volcanic sequence. Highly altered ultramafic rocks, which are probably komatiitic flows, occur in the southern and central portions of the Project. The ultramafic flows are generally altered to fine grained talc-serpentine-carbonate mineralogy.

Structural geology of the property is largely unknown. Previous operators interpreted a north trending dextral fault at the western end of the Frankfield East Deposit. Berger (2000) suggested that the region (including this property) is characterized by early northwest trending faults and later N70°E trending faults. The stratigraphy has been deformed by at least two periods of deformation, as is common in the AGB. However the paucity of outcrops severely hampers the elucidation of the fold patterns on the property. Further interpretation of Gowest’s detailed airborne magnetic survey and compilation with other exploration datasets may assist in determining the Projects structural geology.

7.3. MINERALIZATION

7.3.1. GENERAL

The main bodies of mineralization located to date lie within the Frankfield Block.

7.3.2. FRANKFIELD EAST DEPOSIT

The Frankfield East Deposit comprises a Main Zone and several lesser Hanging Wall Zones. Gold mineralization in the Main Zone occurs primarily within a fractured and brecciated altered horizon previously interpreted as a shear zone in hangingwall basaltic flow rocks at or near the contact with steeply north-dipping (85°) footwall ultramafic rocks to the south.

The mineralization is not confined to narrow vein-like structures (as can be seen in many other deposits in the area) but rather in a more massive/tabular structure that is consistently present throughout the mineralized horizon. This characteristic is shared by the major past gold producers in the Porcupine camp including Hollinger, McIntyre and present producer Goldcorp at their Dome and Hoyle Pond deposits.

Within the geological Main Zone, higher-grade gold mineralization is localized along the footwall of the horizon, termed the MZ1 Zone (previously referred to as M1 Zone – Harron, 2006) and occasionally along the hanging wall of the horizon, termed the MZ2 Zone (previously referred to as M2 Zone – Harron, 2006). Both gold mineralized zones appear to rake steeply to the east based on current drill data. Their variation in widths may reflect tectonically controlled shoots or boudinage structures. Sporadic, anomalous to lower grade gold mineralization is present between these subzones. Pervasive silicification, minor quartz-ankerite veining, hematite staining and presence of tourmaline generate a

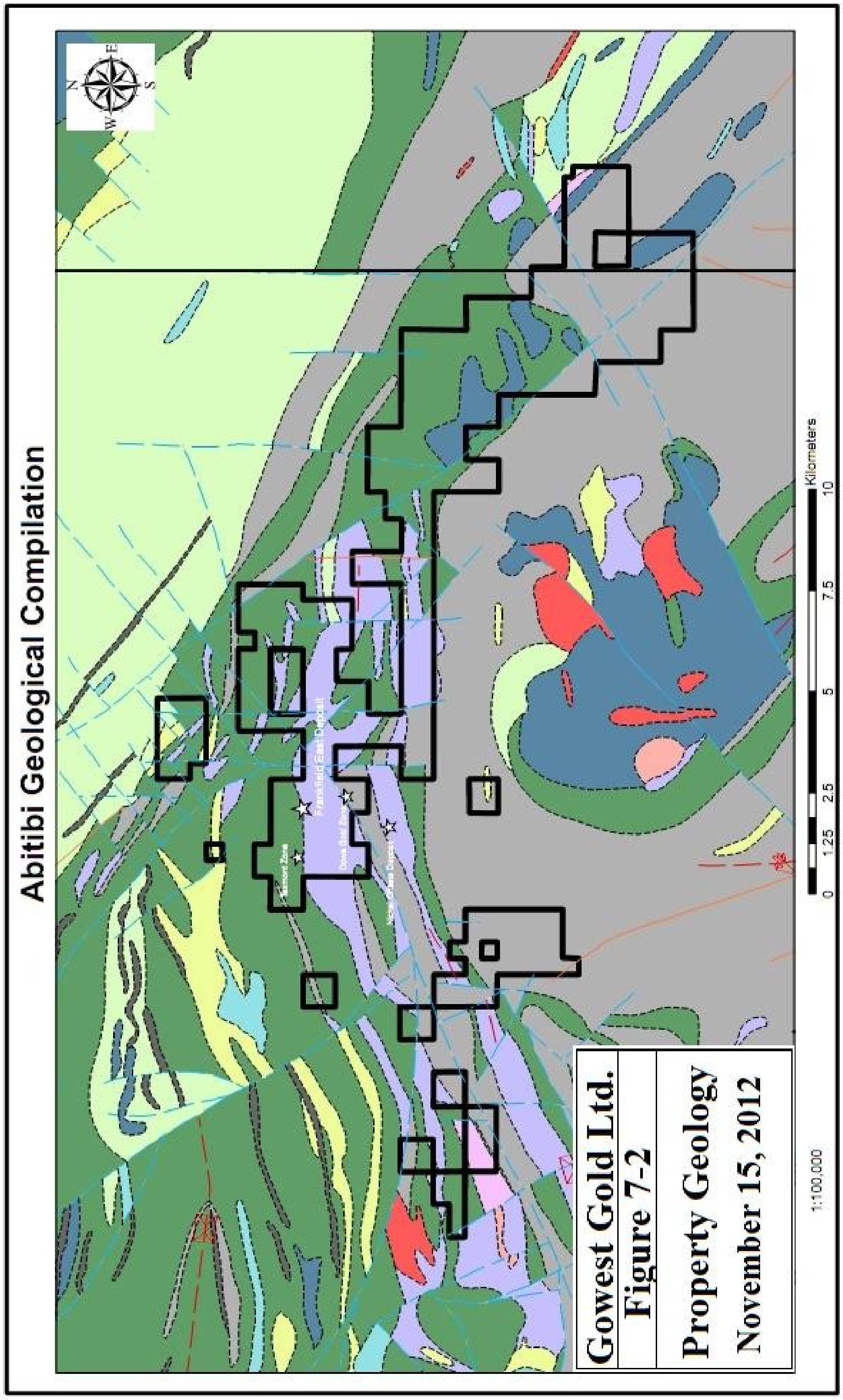

FIGURE 7-2 PROPERTY GEOLOGY, NORTH TIMMINS PROJECT

recognizable mauve to pinkish-grey hue for the mineralized zone. Total sulphide content of the mineralized horizon varies from 3-30% with occasional 2-5 cm wide bands of massive arsenopyrite and pyrite. Most of the sulphide component in the main zone is in the form of seams, bands and clots of sulphides accompanied by zones of heavy disseminations of 5-15% sulphides over 5-10 cm core lengths. The largest concentrations of arsenopyrite correspond to the highest gold concentrations. Visible gold is not a feature of this type of mineralization. Some late stage fracturing and brecciation of the mineralized horizon has caused varying amounts of sulphide remobilization (Roussain, 2004).

Similar mineralization forms multiple structures believed to be subparallel to the strike and dip of the Main Zone and are referred to as Hanging Wall Zones as they are located immediately north of the Main Zone. They are highly silicified zones accompanied by intense bleaching, brecciation and quartz flooding, tourmaline, 5-10% pyrite and arsenopyrite. The overprint of silica flooding and white quartz veining makes the hanging wall zones appear different from the Main Zone but the gold is associated with the sulphide component as in the Main Zone. As in the Main Zone, higher concentrations of arsenopyrite give rise to higher gold values. A total of three such parallel structures (HWZ1 to HWZ3) have been identified in locations and are significant contributors to the total number of ounces of gold contained within the overall Frankfield East Deposit.

To date, the deposit has a drilled strike length in excess of 950 m, trending N070-080°E, and has been tested to a depth in excess of 1,000 m. The width of the Main Zone varies from 2 m to 22 m. MZ1 Zone mineralization ranges in width from 1-12 m (true width). The MZ2 Zone mineralization ranges in width from 1 to 6.9 m wide (true width). The widths of the Hanging Wall Zones typically vary from 2 to 4 m up to a maximum of 12 m. The deposit remains open at depth.

Overburden depth along the strike length of the deposit ranges from 2 to 15 m and averages approximately 10 m deep, indicating relatively easy underground access to the deposit.

7.3.3. TEXMONT DEPOSIT

The Texmont deposit is hosted in a carbonate, hematite and sericite altered shear zone within a sequence of tholeiitic basalt flows. Outcrops immediately north of the mineralized zone strike N075°E and dip steeply to the north (Berger, 2000). The shear zone strikes N086°E and dips 75° to the north. Mineralization is reported to be similar to the Frankfield East deposit.

The Texmont deposit has a strike length of approximately 150 metres and a width of approximately 3 metres. Texmont outlined mineralization to a depth of approximately 75 metres (Pearson, 1989). Subsequent drilling by Cyprus in 1991 showed that the deposit extended to at least a depth of 360 metres. Gowest drilled six diamond drill holes ion 2010. The two best intersections obtained were 4.1 g/t Au over a down-hole length of 13.7 m and 4.1 g/t Au over 0.6 m. Gowest has not prepared a mineral resource estimate for this deposit.

7.3.4. DOWE GOLD SHOWING

The Dowe showing is located on the southeast part of the Frankfield Block. Gowest has not carried out any detailed exploration on the showing. Some drilling is reported by previous owners of the property. Intersections of 2.86 g/t Au over 3.38 m, 1.8 g/t Au over 12 m and 1.9 g/t Au over 3.4 m were reported at that time. Mineralization is reported to occur in quartz veins within a wedge of mafic volcanic rocks enclosed in ultramafic rocks. The mafic rocks are reported to be ankeritized and slightly silicified.

Visible gold has been reported, together with pyrite. No arsenopyrite has been reported. The showing is reported to have a strike length of at least 150 m and has not been closed off.

8. DEPOSIT TYPES

The sulphide enrichment gold deposit model best describes the mineralisation of the Frankfield East Deposit.

The sulphide enrichment deposit model is characterized by a dominance of sulphide minerals over quartz veins, and is localized in shear zones adjacent to rheologically differing mafic to ultramafic volcanic rocks of tholeiitic petrochemistry. Mineralization typically comprises native gold associated with disseminated to massive arsenopyrite and vein hosted pyrite and arsenopyrite in silicified chloritic and sericitic schists, within a broad zone of potassium metasomatism and wall rock sulphidation (disseminated pyrrhotite and pyrite). Carbonatization of the wall rocks is a less conspicuous feature than silicification. Pervasive silicification and silicate alteration minerals developed within the shear zone consists of quartz, albite, chlorite, actinolite, tourmaline and amorphous carbon, suggesting a dominance of silicic and potassic alteration. Canadian examples of sulphide enrichment gold deposits include the Madsen and Starratt-Olsen deposits in the Red Lake Camp, (Durocher, 1983) and the ULU deposit in the High Lake Greenstone Belt in Nunavut. The best Ontario examples of sulphide enrichment gold zones include the gold zones of the Holloway and Holt mines about 100 km east of Timmins (Valliant and Bergen, 2008), and the flow ores of the historic giant Kerr Addison Mine about 150 km southeast of Timmins. In the Porcupine Timmins Gold Camp documented examples include the Bell Creek Mine Zone (Pressacco, 2011) and the historic Moneta Mine gold zones.

In the search for sulphide enrichment and quartz lode gold mineralization magnetic, induced polarization/resistivity (IP/RES) surveys can define favourable host environments. Alteration destroys the magnetic minerals in mafic and ultramafic rocks resulting in subdued magnetic patterns. Silica alteration results in enhanced resistivity, while the presence of arsenopyrite and other sulphide species in the quartz veins and their alteration envelopes produce a positive chargeability response. Surveys over other Canadian examples of this type of mineralization have demonstrated the utility of IP/RES and mise-à-la-masse survey methods in defining mineralization. Previous geophysical surveys on the Project have not included IP/RES surveying due to the thick clay overburden of the area, but have relied on HLEM surveys to delineate graphitic horizons in the volcanic stratigraphy (Trinder, 2011).

Typical soil geochemical surveys are not particularly effective in the North Timmins Project area, as a result of extensive thick overburden cover (greater than 15 m and locally up to 50 m thick). Gowest has conducted several SGH geochemical surveys over various parts of the Project area in an effort to “see through” the deep overburden. The SGH results are being evaluated and compiled by Gowest with other exploration data sets to determine its effectiveness on the North Timmins Project.

9. EXPLORATION

9.1. AIRBORNE GEOPHYSICS

Gowest has undertaken a number of exploration campaigns almost entirely centred on the Frankfield claim block in the past. In 2009, Fugro Airborne Surveys Corp. conducted helicopter-borne DIGHEM V electromagnetic/resistivity/magnetic survey. A total of 438 line-km were flown. The details and results of the survey have been discussed in previous reports, including Ling (2012). The survey was helpful in that it appears to show that mineralization is associated with bedrock features.

Once the Transition claims were optioned in early 2011, Gowest Gold contracted Fugro Airborne Surveys to conduct a HELITEM electromagnetic and magnetic airborne geophysical survey over the North Timmins Project. It was flown between June 26th and July 9th, 2011 and amounted to 1,822.3 line km. The airborne geophysical survey was carried out to map the geology and structure of the area. Data was acquired using a HELITEM electromagnetic system, supplemented by a high-sensitivity cesium magnetometer. A GPS electronic navigation system ensured accurate positioning of the geophysical data with respect to the base map coordinates. The geophysical data obtained by Fugro was processed and interpreted for Gowest by Mark Shore a consulting geophysicist. A series of geophysical maps were produced of the survey area. These updated geophysical maps along with Ontario geological and drill hole data were utilized by Dr. Philips Thurston (Laurentian University) to produce an updated geological/structural base for the project area.

As most of the exploration has concentrated on testing the Frankfield East deposit, full use has not been made of the airborne geophysical survey results. As Gowest is able to develop exploration campaigns to test claims away from the Frankfield Block, the results of the airborne survey may be more useful.

9.2. SOIL GAS HYDROCARBON (SGH) SURVEYS

Gowest undertook a SGH geochemical survey in 2009 on the Frankfield Block. The technique is marketed by Activation Laboratories (ActLabs) of Ancaster, ON. The results of the survey have been discussed in some detail previously. The results of the survey are not particularly useful by themselves and further follow-up work is required. As with the airborne magnetic survey, little follow-up has occurred because all of the Gowest effort has gone into the drill testing of the Frankfield East deposit.

In late 2011, an SGH survey was conducted, on the Wark 1 Property, to evaluate its gold mineralization potential. A total of 680 soil samples were collected. The interpretation of the SGH survey results by Dale Sutherland of ActLabs outlined four REDOX cells have weak to moderate potential to be a gold mineralization target. An SGH survey was conducted, on the Wark 2 Property from October 7 to 13, 2011. Soil samples were collected from 130 sites on the western half of the Wark 2 Property. The interpretation of the SGH survey results outlined a strong 1,500 m long oval REDOX cell trending east-west in the survey area. This REDOX cell was judged by Dale Sutherland of ActLabs to have a strong potential to be a base metal mineralization target. The details and results of these SGH surveys were filed for assessment with the Ontario Ministry of Northern Development Mines (MNDM) in 2012.

A third larger SGH survey consisting of 2,320 samples was carried out on the Transition claims of the Pipestone East Property, from July to September 2011. The interpretation of the SGH survey results by Dale Sutherland of ActLabs outlined a well-defined gold halo anomaly in the central portion of the northern half of the survey area. This oval REDOX cell is very large 2.5 x 4 km in size. A more intense nested halo REDOX cell (800 m x 1,000 m) occurs in the eastern central portion of the larger cell and was interpreted to be a strong gold mineralization target. The Pipestone East SGH survey has not been filed for assessment with the Ontario MNDM.

9.3. GEOLOGY SURVEYS

Gowest Gold conducted geological mapping on the Prosser and Gowan claim blocks in 2011. This was carried out to satisfy assessment work requirements and filed with the Ontario MNDM on November 15, 2011. No bedrock exposure was located on the Gowan block and a single mafic volcanic exposure was found along the northern claim boundary of the Prosser block. Rock samples for gold analysis were not collected during the geological surveys.

10. DRILLING

10.1. GENERAL

Drilling of the Frankfield property, and in particular the Frankfield East deposit, has continued for many years. Details of the pre-2004 drilling are sketchy and it is likely that sampling and quality control/quality assurance were not up to current standards.

10.2. DIAMOND DRILLING 2004 TO 2011

There has been a significant amount of diamond drilling since 2004. Drilling in the period 2004 to 2011 is summarized in Table 10-1 and details of the various drilling programs are summarized by Trinder (2011).

TABLE 10-1 DIAMOND DRILLING 2004 TO 2011
Frankfield Property – Gowest Gold Ltd.

Program	Drill Hole Series	Total No. Drill Holes	Total Metres
2004	GW04-01 to GW04-22, GW04-25	25	6,538
2005	GW05-23 to GW05-24 GW05-26 to GW05-30	7	2,809
2006	GW05-31 GW06-32 to GW06-38	8	1,407
2008	GW08-39 to GW08-44	6	1,275
2010	GW10-45 to GWH10-120 GW10-60WA, GW10-60WB GW10-122 to GW10-138 GW10-140 to GW10-146	102	30,621
2011*	GW11-121, GW11-139 GW11-147 to GW11-162	18	8,586
Total			42,650

Note: As at April 24, 2011 (Trinder, 2011)

10.3. DRILLING 2011 TO 2012

Diamond drilling continued during 2011 and in 2012. A further 46 holes were drilled for an aggregate depth of 14,835 m.

Details of the most recent drilling campaign are set out in Table 10-2.

TABLE 10-2 FRANKFIELD BLOCK DRILL HOLE DATA							
Frankfield Property – Gowest Gold Ltd.							
Hole ID	**Northing**	**Easting**	**Elevation**	**Azimuth (°)**	**Dip (°)**	**Length (m)**	**Core Size**
GW11-163	5399400	487050	290.1	180	-70	1107	NQ
GW11-164	5398630	486299	296.9	179.8	-56	226	NQ
GW11-165	5398561	486298	297.7	179.8	-50	114	NQ
GW11-166	5398626	486249	296.8	180.3	-57	237	NQ
GW11-167	5398551	486251	296.4	180	-50	162	NQ
GW11-168	5398763	487104	291.9	180	-50	120	NQ
GW11-169	5398808	487098	295.1	180	-50	185	NQ
GW11-170	5398906	486950	295.2	179.9	-50	383	NQ
GW11-171	5398735	487025	298.2	180.5	-50	108	NQ
GW11-172	5398704	486979	295.6	180.2	-50	96	NQ
GW11-173	5398677	486654	297.2	180	-50	144	NQ
GW11-174	5398693	486601	297	180	-55	174	NQ
GW11-175	5398683	486501	295.2	180.1	-53	171	NQ
GW11-176	5398647	486567	296.7	180	-50	123	NQ
GW11-177	5398620	486628	296.9	180.1	-50	78	NQ
GW11-178	5398650	486777	294.8	180	-50	90	NQ
GW11-179	5398778	486882.8	294.3	180.1	-50	213	NQ
GW11-180	5398778	486882.8	293.4	180	-59	228	NQ
GW11-181	5398878	487152.6	292.2	180	-52	225	NQ
GW11-182	5398656	486886.5	293.6	360	-75	165	NQ
GW11-183	5398635	486888.4	292.9	360	-47	126	NQ
GW11-184	5399076	487007.5	293.5	180	-64	600	NQ
GW11-185B	5398952	486877.1	295.1	180	-66	488	NQ
GW11-186	5398970	487032.3	292.3	180	-61	456	NQ
GW11-187	5398960	486804.8	295.6	180.4	-62	486	NQ
GW11-188	5398614	486198.4	295.1	180.3	-50	270	NQ
GW11-189	5398450	486200	295	180	-50	269	NQ
GW11-190	5398629	486003.1	295.7	180.3	-50	309	NQ
GW11-191	5398666	486152.8	294.1	180.1	-50	324	NQ
GW11-192	5398668	486097	296.4	180.6	-50	321	NQ
GW11-193	5398778	486001.5	297.3	179.9	-50	314	NQ
GW11-194	5398753	485850.8	296.3	180.7	-50	300	NQ
GW11-195	5398914	487249.1	288.3	178.9	-50	180	NQ
GW11-196	5399006	487248.8	291.8	179.8	-53	300	NQ
GW11-197	5399022	487349.3	293.1	179.7	-50	219	NQ
GW11-198	5398604	486789.9	292.3	0	-78	171	NQ

GW11-199	5398584	486786.9	293.8	0	-70	300	NQ
GW12-200	5399102	487348.5	293.4	179.9	-50	302	NQ
GW12-201	5399670	486695.6	293.1	180	-76	306	NQ
GW12-201B	5399669	486695	292.9	180.2	-78	1523	NQ
GW12-202	5398975	487198.6	291.6	180	-53	317	NQ
GW12-203	5398897	486449.6	292	179.5	-65	599	NQ
GW12-211	5399674	486876.3	291.3	180	-78	139	NQ
GW12-211B	5399687	486877.4	290.4	180	-78	1396	NQ
GW11-198	5398604	486789.9	292.3	0	-78	171	NQ
GW11-199	5398584	486786.9	293.8	0	-70	300	NQ
Total						**14,835**	

The above 2011-2012 drilling was carried out by Norex Drilling limited (Norex) of Porcupine, ON. Norex is reputable drilling contractor with a good reliable record.

Drill hole collars were positioned by Gowest Gold personnel with a hand held GPS unit. All diamond drill holes were aligned by drilling crews employing an Azimuth Pointing System (APS) rented from Reflex instruments of Timmins Ontario. The Azimuth Pointing System (APS) is a GPS based compass that provides a True North Azimuth measurement and position. Since the APS is not using the earth's magnetic field to determine the azimuth, it is not affected by ferrous anomalies (metal) from the ground or surrounding structures. The APS uses two antennas to calculate an azimuth solution. The APS surveys the drill hole collar coordinates and elevation in UTM coordinates (NAD83) utilizing total station GPS instrumentation. This data was recorded and subsequently inputted by Gowest Gold personnel into a Surpac computer database. As a verification of the collar co-ordinates, Gowest Gold resurveyed with the APS approximately 10% of the holes.

During drilling, the contractor conducted down hole surveying utilizing a Reflex EZ-Shot®, an electronic single shot instrument. It accurately measures six parameters in one single shot; azimuth, inclination, magnetic tool face angle, gravity roll angle, magnetic field strength and temperature. Single shot tests were taken 15 m or so below the casing and every 50 m down the drill hole. Casing was left in each of the holes and the stand pipes were capped.

Industry standard core sampling protocols are used by Gowest Gold on all drill holes. These protocols are documented in hard copy Gowest Gold sampling procedures, which are described in this section.

At the drill site, the drilling contractor places drill core into wooden tray boxes along with 'marker blocks" to indicate measured distances down the drill hole from the collar. During drilling programs, drill core is collected by Gowest Gold technicians at the drill sites or the drill access trail every drilling day and moved to a secure logging facility. The secure logging facility is located at 115 Jubilee Avenue East Timmins, Ontario.

At the logging facility, the length of drill core recovered was compared to the position of depth markers in the core boxes by a technician in order to check for misplaced markers and to calculate the amount of core loss, if any. Prior to lithological logging and sampling, a Gowest geo-technician takes digital photographs of the core, cleans the core if necessary, completes a geotechnical log of core recovery, RQD and fracture analysis measurements, and conducts magnetic susceptibility on the core. The core is then logged and sampled by qualified geologists. Geological descriptions of the core and sampling intervals with corresponding identifier numbers were entered onto a “diamond drill log record” captured on a laptop computer. Sampling of the core was based on visual observations of sulphide mineralization and samples were collected within lithologically homogeneous intervals with due regard for varying mineralogy and textures. Sample intervals did not cross geological boundaries. Generally, the sample length within mineralized zones was on the order of 0.5 to 1.0 metre or less. The NQ core selected for sampling was split in half by a hydraulic splitter and a half bagged with the first part of a three-part assay tag bearing a unique identifier number. The other half of the core was stored at the logging facility with the second part of the three part assay tag bearing an identical unique identifier number placed in the core box at the beginning of the sample interval. Records of the sampled intervals and sample numbers are recorded in the computerized drill logs, and the third part of the assay tag is filed.

The spilt drill core is securely stored at the Norex Drilling office/core storage facility, 7210 Highway 101 East in Timmins and the whole core is stored outside at Rob Roy Contracting, 6033 King Street in Timmins.

Both Gow and Montgomery examined the logging procedures. The work was completed by experienced personnel with a history of work in the Timmins camp. In the opinion of the authors, Gowest Gold personnel used industry best practices in the collection, handling and management of drill core assay samples. There is no evidence that the sampling approach and methodology used by Gowest Gold introduces any sampling bias or contamination.

10.4. DRILLING OUTSIDE THE FRANKFIELD BLOCK

Gowest Gold conducted exploration drilling outside of the Frankfield Block in 2012 and this drilling is summarized in Table 10-3. On the southeast portion of the Tully East Property, five holes (GW 12-204 to 209) were drilled totaling 1,172 m. They were drilled from February 7 to March 8, 2012. These holes tested airborne electromagnetic conductors at or near lithological contacts thought to be similar settings as the Frankfield East deposit. Although, the holes returned no significant gold values they provided valuable information on the geology of the areas tested.

A three hole diamond drilling program totalling 1,291 m was conducted on the Pipestone East Property (Transition.). The three holes were labelled as GW12-212/213/214 and were drilled from March 7 to April 20, 2012. Hole GW12-212 targeted an EM conductor proximal to Cross Lake Fault, Hole GW12-213 targeted the north portion of a large SGH gold anomaly coinciding with a magnetic low-magnetic high contact and Hole GW12-214 targeted central portion of a large SGH gold anomaly and a weak EM conductor. The holes returned no significant gold values but Hole GW12-213 intersected strongly carbonate-sericite altered volcanic rocks about a quartz vein zone which is encouraging for gold mineralization.

TABLE 10-3 OUTSIDE DRILL HOLE DATA

Tully East & Pipestone East Properties – Gowest Gold Ltd.

Hole ID	Northing	Easting	Elevation	Azimuth (°)	Dip (°)	Length (m)	Core Size
GW12-204	5395725	493250	295	180	-55	263	NQ
GW12-205	5395850	492249.2	302.5	200	-55	269	NQ
GW12-206	5396450	492800	295	180	-60	257	NQ

GW12-209	5396575	492800	295	180	-55	81	NQ
GW12-210	5396575	492800	295	180	-55	302	NQ
GW12-212	5395672	494797.4	306.6	225	-55	530	NQ
GW12-213	5394748	497001	340.6	180	-57	372	NQ
GW12-214	5394340	497001.3	329.7	180	-57	450	NQ
Total						**2,524**	

Core handling procedures for the drilling outside the Frankfield Block was the same as for the Frankfield Block discussed above.

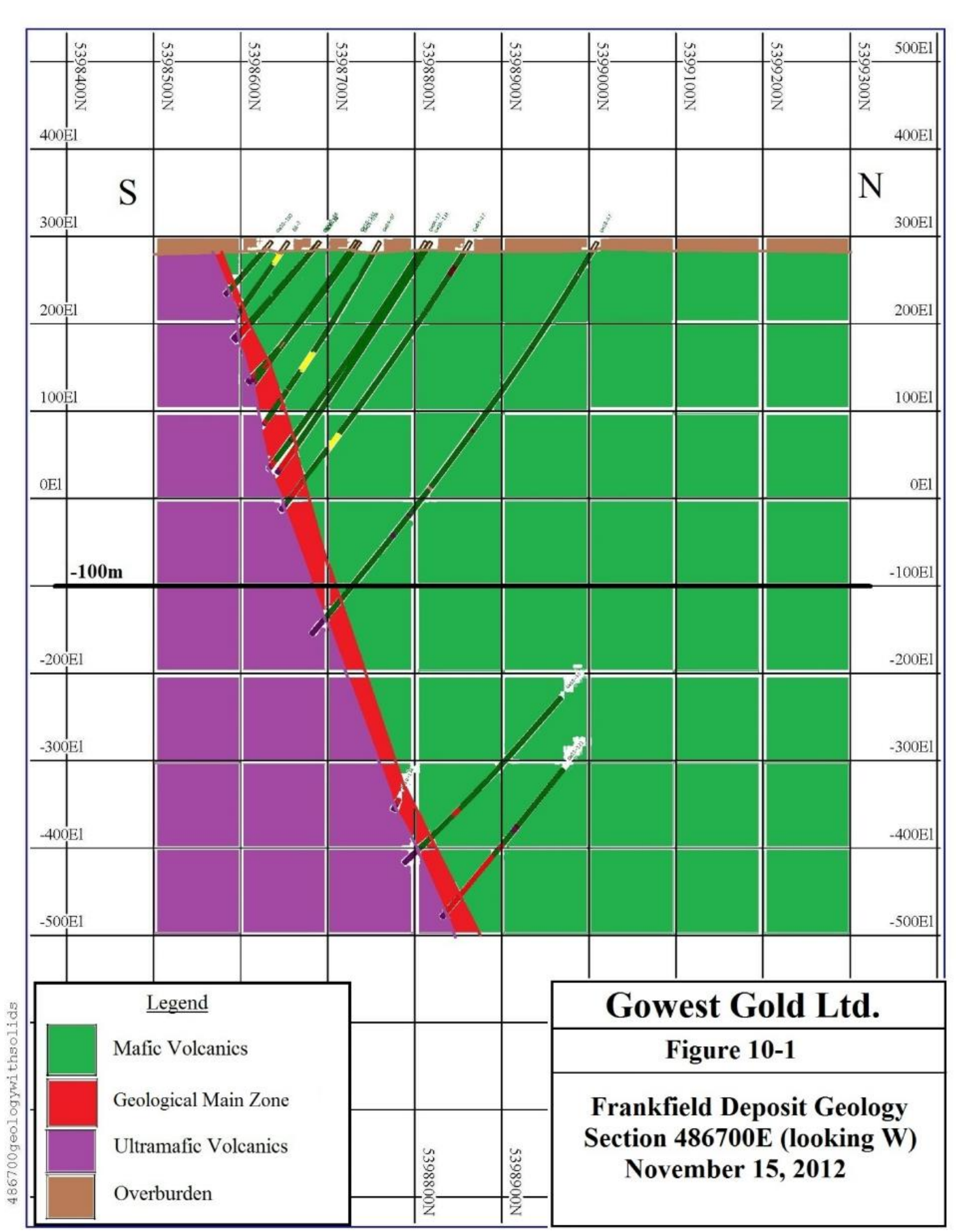

FIGURE 10-1 SECTION 486700, FRANKFIELD EAST DEPOSIT

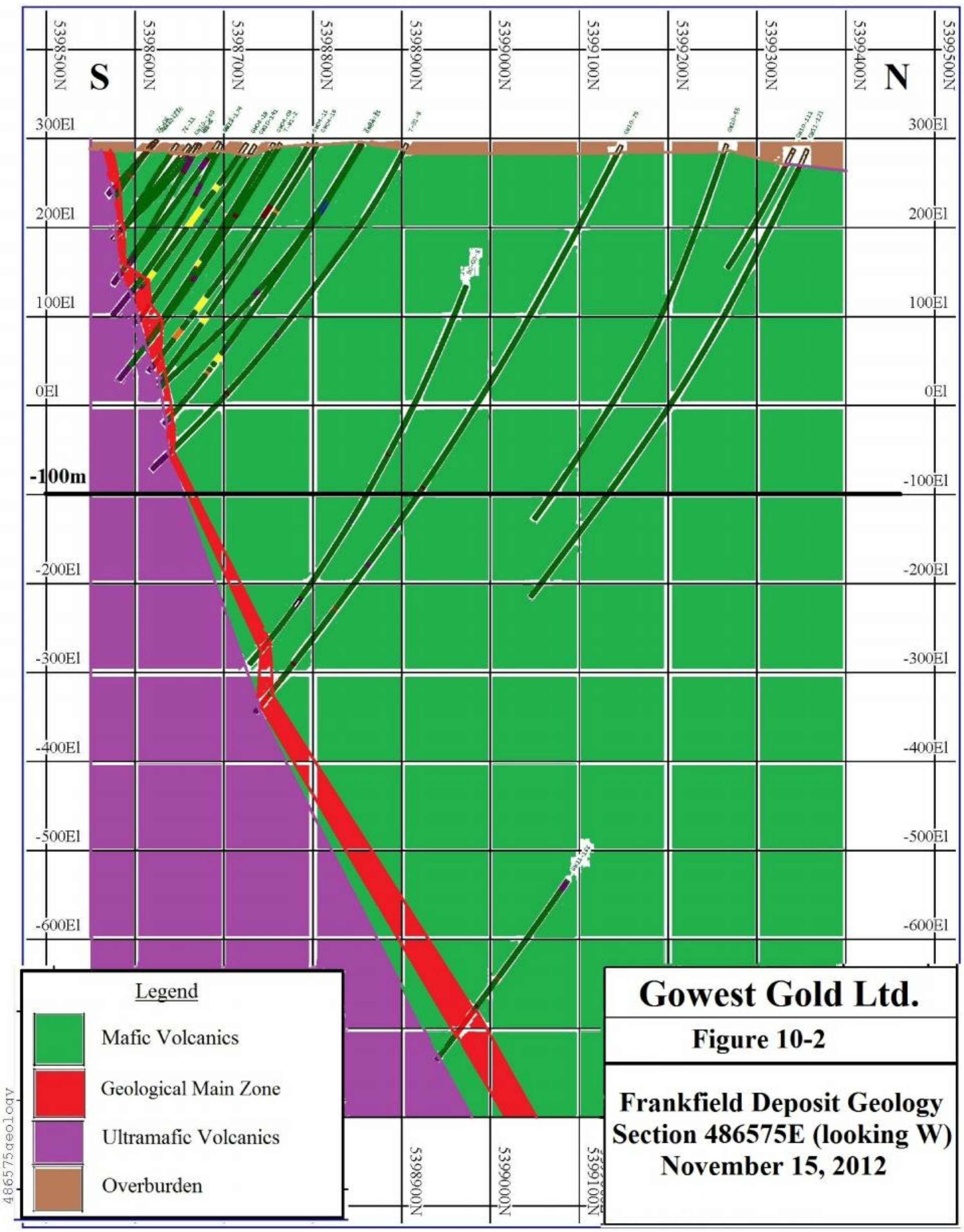

FIGURE 10-2 SECTION 486575, FRANKFIELD EAST DEPOSIT

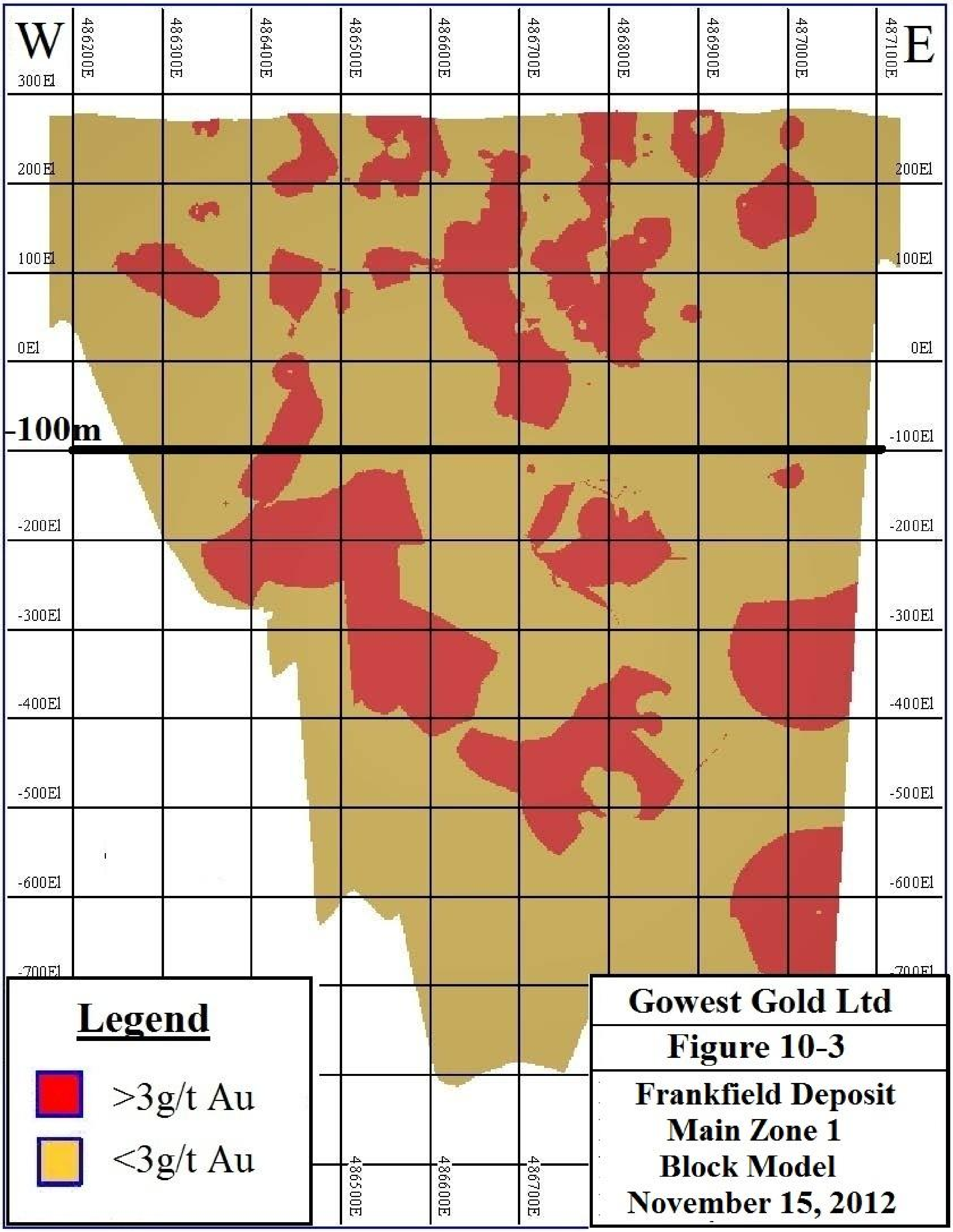

FIGURE 10-3 LONGITUDINAL SECTION, MAIN ZONE ONE

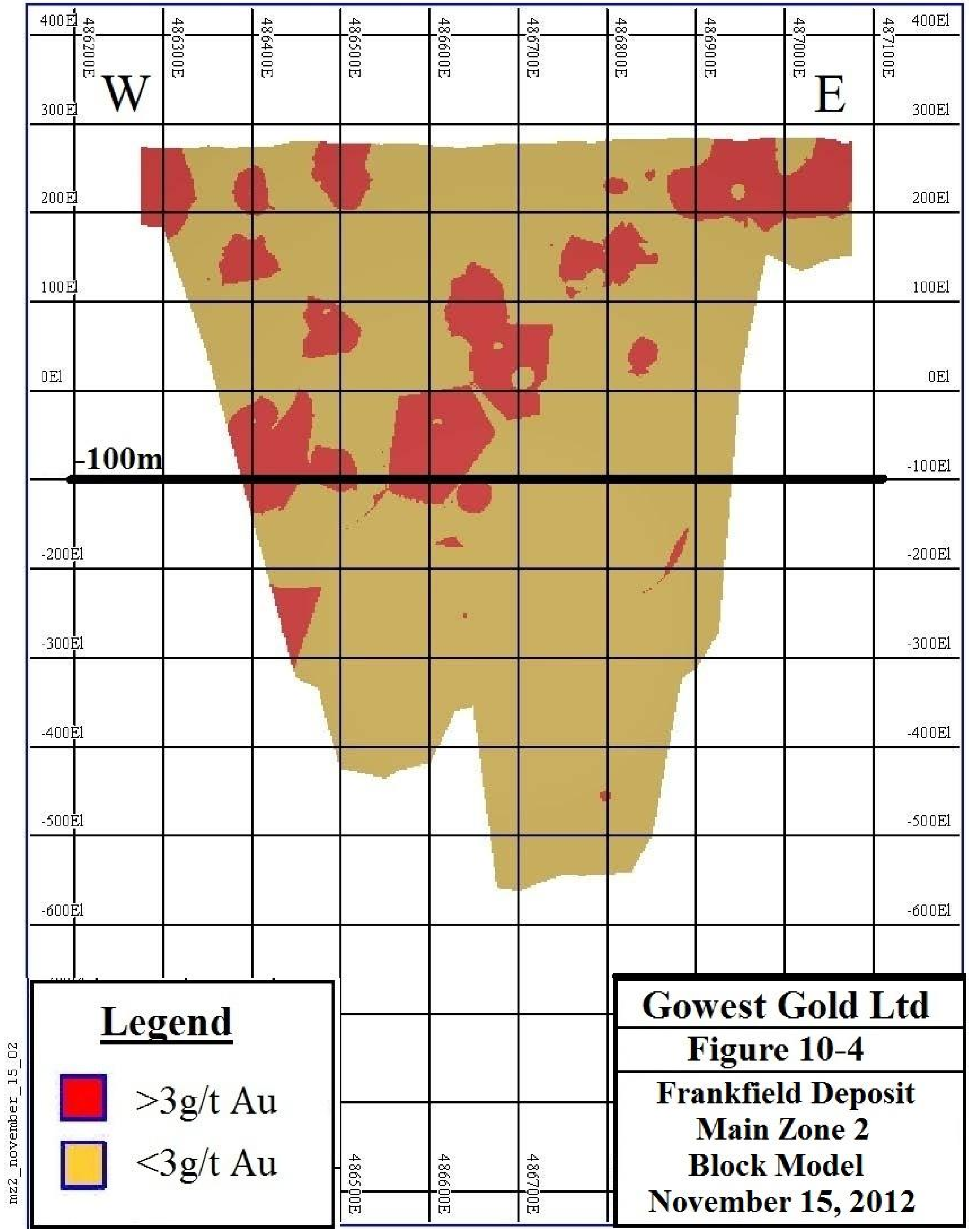

FIGURE 10-4 LONGITUDINAL SECTION, MAIN ZONE TWO

11. SAMPLE PREPARATION, ANALYSES A SECURITY

11.1. SAMPLE PREPARATION PRIOR TO 2010

The following has been extracted from Trinder (2011).

Security of samples prior to dispatch to the analytical laboratory was maintained by limiting access of un-authorized persons to the secure core handling facility. Detailed records of sample numbers and sample descriptions provided integrity to the sampling process. Labelled samples packed in sealed bags robust enough to survive the journey to the assay laboratory also provided sample integrity. The assay laboratory completed sample preparation operations at their locations, and employed bar coding and scanning technologies that provided complete chain of custody records for every sample.

The security and integrity of the samples submitted for analyses was un-compromised, given the secure (fenced) core handling location, adequate record keeping, prompt expediting of samples, and the analytical laboratories' chain of custody procedures.

Assaying of the samples from the 2004 to 2008 drill programs was completed by Swastika Laboratories Limited (Swastika), P.O. Box 10, 1 Cameron St., Swastika, Ontario, P0K 1T0. Swastika participates in the Proficiency Testing Program for Mineral Analysis Laboratories, a testing program conducted bi-annually by the Standards Council of Canada. Swastika is the holder of a Certificate of Laboratory Proficiency. Sample preparation follows industry best practices and procedures. The analytical methods used are routine and provide robust data associated with a high degree of analytical precision.

Sample preparation at Swastika starts comprised drying of the samples and crushing to ½ inch in a jaw crusher and then to –10 mesh in a roller crusher. The sample was split with a Jones riffle, and 350 g of material taken for analysis; the remainder was placed in a numbered plastic bag and stored. The 350 g sample was then pulverized (85-95% passing minus 150 mesh) and homogenized, and was then ready for assay. Compressed air was used to clean the equipment between samples, and the roller crusher is also cleaned with a wire brush. Barren material was crushed between sample batches. All Gowest samples were analysed for Au using fire assay/atomic absorption (FA/AA) techniques on 30 gram samples. Samples that returned Au values greater or equal to 10 g/t were re-assayed by FA/gravimetric methods using a 30 g sample.

In addition to standards submitted by Gowest, Swastika conducted check assays on 10% of the samples to monitor assay repeatability, and analysed a second pulp for samples that return high assays. They also analysed their own standards and blanks with every batch of samples. Swastika's employees are independent from Gowest and Gowest personnel were not involved in sample preparation and analysis.

The security, sample collection, preparation and analytical procedures undertaken on the Frankfield Gold project during the 2004 to 2008 drill programs is considered to conform to industry standards.

11.2. GOWEST 2010 TO 2012 SAMPLE PREPARATION, ANALYSIS AND SECURITY

The following is a description sample preparation, analyses and security protocols and procedures utilized by Gowest for the 2010 to 2012 drill programs, as previously discussed by Trinder, (2011).

Security of samples prior to dispatch to the analytical laboratory is maintained by limiting access of un-authorized persons to the secure core handling facility. Detailed records of sample numbers and sample descriptions provide integrity to the sampling process. Labelled samples packed in sealed bags robust enough to survive the journey to the assay laboratory also provide sample integrity. The assay laboratory completes sample preparation operations at their locations, and employ bar coding and scanning technologies that provide complete chain of custody records for every sample.

It is considered that the security and integrity of the samples submitted for analyses is un-compromised, given the secure core handling and storage locations, adequate record keeping, prompt expediting of samples, and the analytical laboratories' chain of custody procedures.

Samples are delivered to ALS Minerals (ALS) Timmins branch laboratory, 2090 Riverside Drive, Unit 10, Timmins, Ontario. Samples are prepared at the Timmins facility and sample pulps are forwarded to the ALS' Mineral Laboratory in North Vancouver, British Columbia for analysis. The Timmins branch laboratory is individually certified to standards within ISO 9001:2008. The North Vancouver analytical facility is individually certified to standards within ISO 9001:2008 and has received accreditation to ISO/IEC 17025:2005 from the Standards Council of Canada (SCC) for methods including: Fire Assay Au by Atomic Absorption (AA); Fire Assay Au and Ag by Gravimetric finish; Aqua Regia Ag, Cu, Pb, Zn and Mo by AA and Aqua Regia Multi-element by ICP and MS. Sample preparation follows industry best practices and procedures. The analytical methods used are routine and provide robust data associated with a high degree of analytical precision.

At the Timmins facility, the sample is logged in the tracking system, weighed, dried and finely crushed to better than 70 % passing a 2 mm (Tyler 9 mesh, US Std. No.10) screen. A split of up to 1000 g is taken using a riffle splitter and pulverized to better than 85 % passing a 75 micron (Tyler 200 mesh) screen. Compressed air is used to clean the equipment between samples. Barren material is crushed between sample batches. ALS then forwards a split of the sample pulp to the North Vancouver Mineral Laboratory for analysis.

Gowest requests the following analyses on all drill core samples in the period 2010 to 2012:

- Gold Fire Assay – AAS Finish (ALS Code Au-AA23)
  - A 30 gram prepared sample is fused with a mixture of lead oxide, sodium carbonate, borax, silica and other reagents as required, is quartered with 6 mg of gold-free silver and then cupelled to yield a precious metal bead.
  - The bead is digested in 0.5 mL dilute nitric acid in the microwave oven, 0.5 mL concentrated hydrochloric acid is then added and the bead is further digested in the microwave at a lower power setting. The digested solution is cooled, diluted to a total volume of 4 mL with de-mineralized water, and analyzed by atomic absorption spectroscopy against matrix-matched standards.
  - Lower detection limit: 0.005 ppm; Upper detection limit: 10 ppm

- Multi-Element ICP-AES Analysis (ALS Code ME-ICP41)
  - A prepared sample is digested with Aqua Regia in a graphite heating block. After cooling, the resulting solution is diluted to 12.5 mL with deionized water, mixed and analyzed by

inductively coupled plasma-atomic emission spectrometry. The analytical results are corrected for inter-element spectral interferences.

    - Partial leach.

- Bulk Sample Density (ALS Code OA-GRA08)
    - The core section (up to 6 kg) is weighed dry. The sample is then weighed while it is suspended in water. The specific gravity is calculated from the following equation:
      SG= Weight in air (g) / (Weight in air (g) – Weight in Water (g))

Overlimit results (gold, arsenic and sulphur) are analysed by the following methods:

- Gold Fire Assay – Gravimetric Finish (ALS Code Au-GRA21)
    - A 30 gram prepared sample is fused with a mixture of lead oxide, sodium carbonate, borax, silica and other reagents in order to produce a lead button. The lead button containing the precious metals is cupelled to remove the lead. The remaining gold and silver bead is parted in dilute nitric acid, annealed and weighed as gold.
    - Lower detection limit: 0.05 ppm; Upper detection limit: 1000 ppm

- Ore-Grade Multi-Element ICP-AES Analysis (ALS Code ME-OG46)
    - A prepared sample is digested in 75% aqua regia for 120 minutes. After cooling, the resulting solution is diluted to volume (100 mL) with de-ionized water, mixed and then analyzed by inductively coupled plasma - atomic emission spectrometry or by atomic absorption spectrometry.

- Total Sulphur - Leco Analysis (ALS Code S-IR08)
    - The sample is analyzed for Total Sulphur using a Leco sulphur analyzer. The sample (0.01 to 0.1 g) is heated to approximately 1350 °C in an induction furnace while passing a stream of oxygen through the sample. Sulphur dioxide released from the sample is measured by an IR detection system and the Total Sulphur result is provided.
    - Lower detection limit: 0.01%; Upper detection limit: 50%

In addition to routine screen tests, sample preparation quality is monitored internally at ALS Minerals through the insertion of sample preparation duplicates. For every 50 samples prepared, an additional split is taken from the coarse crushed material to create a pulverizing duplicate. The additional split is processed and analyzed in a similar manner to the other samples in the submission.

Internal quality control samples including certified reference materials, blanks, and duplicates are inserted within each analytical run. The blank is inserted at the beginning, standards are inserted at random intervals, and duplicates are analyzed at the end of the batch. The minimum number of quality control samples required to be inserted are based on the rack size specific to the method.

All ALS Minerals analytical facilities in North America participate in round robin & external proficiency tests for the analytical procedures routinely done at each laboratory. The laboratories also routinely participate in proficiency tests organized by the Canadian Certified Reference Materials Projects, Geostats and a number of independent studies organized by consultants for specific clients.

ALS employees are independent from Gowest and Gowest personnel are not involved in sample preparation and analysis.

The security, sample collection, preparation and analytical procedures undertaken on the Frankfield Gold Project during the 2010 to 2012 drill programs are considered by Gow to conform to industry standards.

11.3. GOWEST QUALITY CONTROL 2010 TO 2012

The monitoring and assessment of QA/QC data attempts to provide adequate confidence that sample and assay data obtained from these laboratories can be used for resource estimation. Gowest Gold has implemented formal analytical quality control measures since 2004. Details of the 2004-2008 QA/QC sampling protocol are summarized in Trinder (2011).

11.3.1. BLANKS

Gowest Gold inserted a blank into the sample stream at a rate of about 1 in 20 samples. A total of 460 blank samples were inserted during the 2010 to 2012 drilling campaign which represents about 3.9% of the sample database for this period. The blank material used was pre-pulverized silica flour.

Of the 460 blank samples analysed from 2010 to 2012 at the ALS laboratory, 95.00% correctly identified the blank sample as having a gold content below or at the lower limit of detection (0.005 ppm Au). An additional 4.35 % of the analyses identified the blank sample as containing less than or equal to 0.015 ppm Au. Only three of the blank material values failed (>0.015 ppm Au, three times detection limit) which represents about 0.65 % of all the blank samples submitted for this period (January 2010 to June 2012). Although any failure during a QA/QC program should be investigated, the sizes of the failures were not enough to be of a serious concern for the purposes of this report.

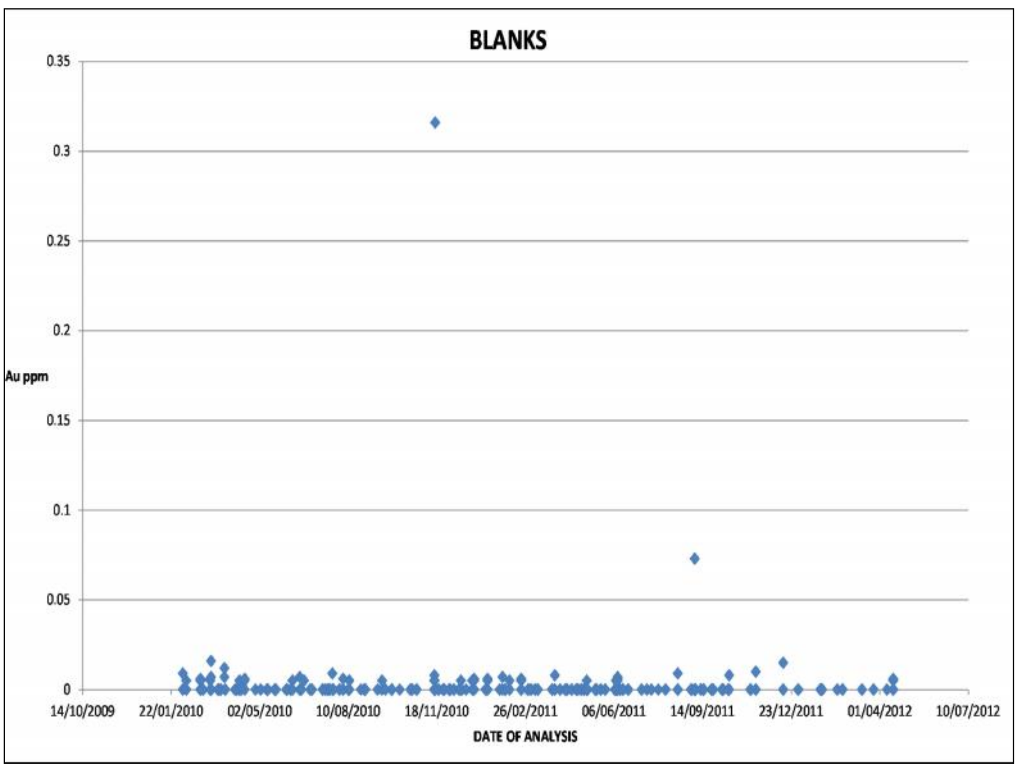

FIGURE 11-1 BLANKS

The results imply that the lab has minimal cross sample contamination, or analytical error in the assaying of blank material. The authors recommend that Gowest Gold continues to use and monitor blank samples and flag any serious concerns with the laboratory staff, as soon as a failure is observed. In addition, if possible, replace the silica flour with some locally sourced material that can be sufficiently used as a blank. The purpose of the blank QA/QC sample is to monitor the preparation laboratory crushing and pulverizing for cross contamination. The current blank is already crushed and pulverized.

11.3.2. STANDARDS

A certified standard was inserted into the sample stream at a rate of about 1 in 20 samples. A total of 472 standard samples were inserted during the drilling campaign which represents about 4 % of the sample database for this period. Three certified standards are currently used by Gowest Gold for the QA/QC assessment of the ALS laboratory (see Table 11-1). Standard OREAS-19A has the largest number of assays and was used throughout the 2010-2012 drilling campaign while standards OREAS-16A and OREAS-16B were introduced in early 2011. All three standards were obtained from Ore Research & Exploration Pty Ltd (ORE) of Australia through Analytical Solutions Ltd. of Toronto Ontario.

They range in certified mean grade from 1.81 to 5.49 g/t Au and represent well the gold grades of the Frankfield East gold deposit. Control plots for the assaying of each standard by ALS Laboratory are presented in Figure 11-2 to Figure 11-4.

TABLE 11-1 STANDARDS 2010 TO 2012

North Timmins Project Drilling - Gowest Gold Ltd

Standard	No. of Analyses	Certified Grade	Stdv	+ 3 Stdv	-3 Stdv
OREAS 16A	75	1.81	0.18	1.63	1.99
OREAS 16B	67	2.21	0.07	2.00	2.42
OREAS 19A	330	5.49	0.10	5.19	5.79

The low grade OREAS16A has an accepted value of 1.81 g/t Au with a between lab's 99th confidence of 0.18 g/t Au. The mean grade of the QA/QC samples submitted was 1.81 g/t Au, equal to the accepted certified value and within the confidence level set for between labs. There were no failures within the QA/QC sample suite submitted (Figure 11-2). Overall there is some variance in the sample results throughout the 2010-2012 drill campaign, but there is no drift evident.

The medium grade OREAS16A has an accepted value of 2.21 g/t Au with a between lab's 99th confidence of 0.07 g/t Au. The mean grade of the QA/QC samples submitted was 2.20 g/t, very slightly below the accepted value and within the confidence level set for between labs. There were no failures within the QA/QC sample suite submitted (Figure 11-3). Overall there is some variance in the sample results throughout the campaign, but there is no drift evident.

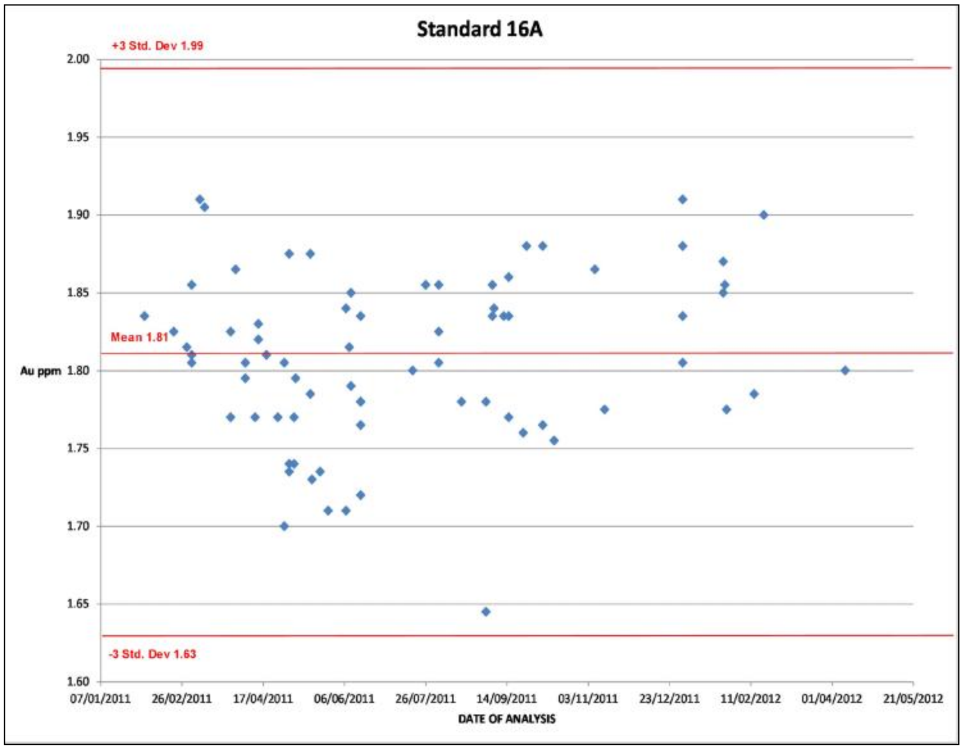

FIGURE 11-2 STANDARD 16A

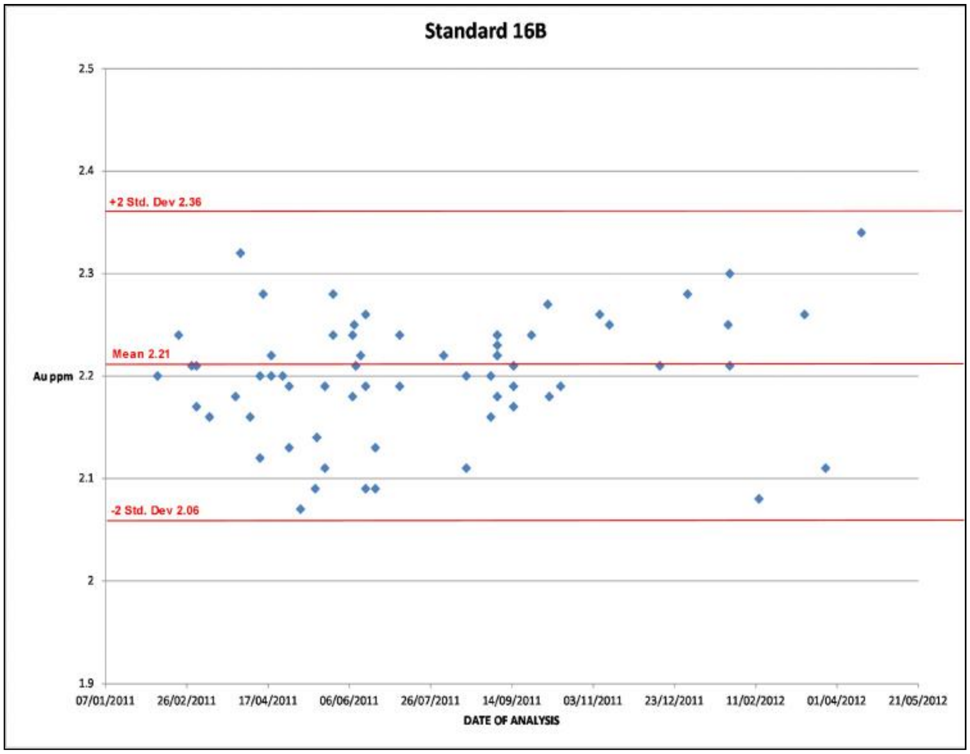

FIGURE 11-3 STANDARD 16B

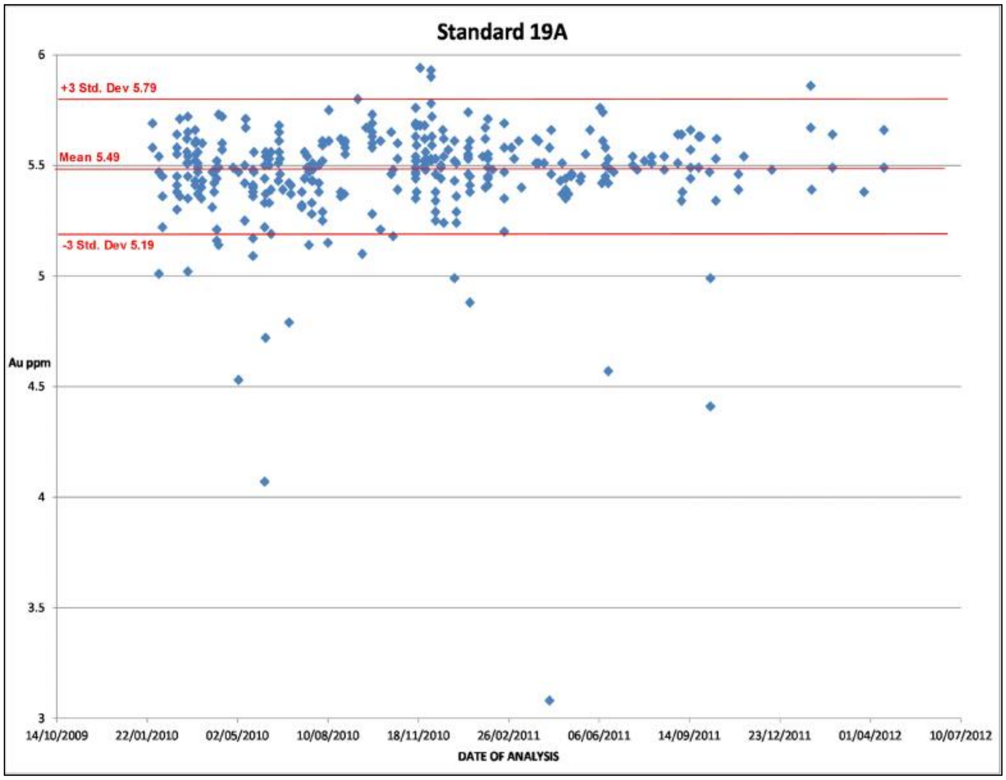

FIGURE 11-4 STANDARD 19A

Standard OREAS-19A has the largest number of assays and was used exclusively for the quality control of drill holes GW10-45 to GW10-110. The higher grade OREAS19A has an accepted value of 5.49 g/t Au with a between lab's 99th confidence of 0.10 g/t Au. The mean grade of the QA/QC samples submitted was 5.46 g/t Au, very slightly below the accepted value and within the confidence level set for between labs.

There are some occasions where there are Standard OREAS-19A assays beyond -3SD, 93 % of samples are within 3SD of the certified standard grade of 5.49 ppm Au. Of the 23 samples outside of 3SD, 19 are below -3 SD indicating that there is potential for underreporting of gold grades. There were three failures of concern (< 4.5 g/t Au) within the QA/QC sample suite submitted (samples #E497554, #E501041,and #E502913). These failures should be examined further to determine the potential source of the error (Figure 11-4). A mean difference between the standard grade the assayed grade of 5.5 % suggests that the bias is slight.

11.3.3. DUPLICATES

CORE DUPLICATES

In 2010, 8 quarter core duplicates were taken from holes GW10-113, GW10-114, GW10-119 and GW10-125. The core duplicates show good repeatability, 75% of samples have a HARD value less than 20% of the sample mean (5). The repeatability of field duplicates is indicative of a low nugget effect (the inherent variability of gold content in samples from the same piece of core) and demonstrates acceptable levels of assay lab precision.

There are an insufficient number of samples to determine the precision of all ALS analyses or the natural variability of gold in core samples (Trinder, 2011).

REJECT DUPLICATES

Gowest has conducted reject duplicate sampling of approximately 5% of coarse crush rejects of samples from previously sampled holes GW10-45 to GW10-163. A total of 374 samples were sent to Activation Laboratories (Actlabs) in Timmins for gold analysis. The comparison of the original ALS to the check Actlabs gold values for the samples are displayed in Figure 11-5.

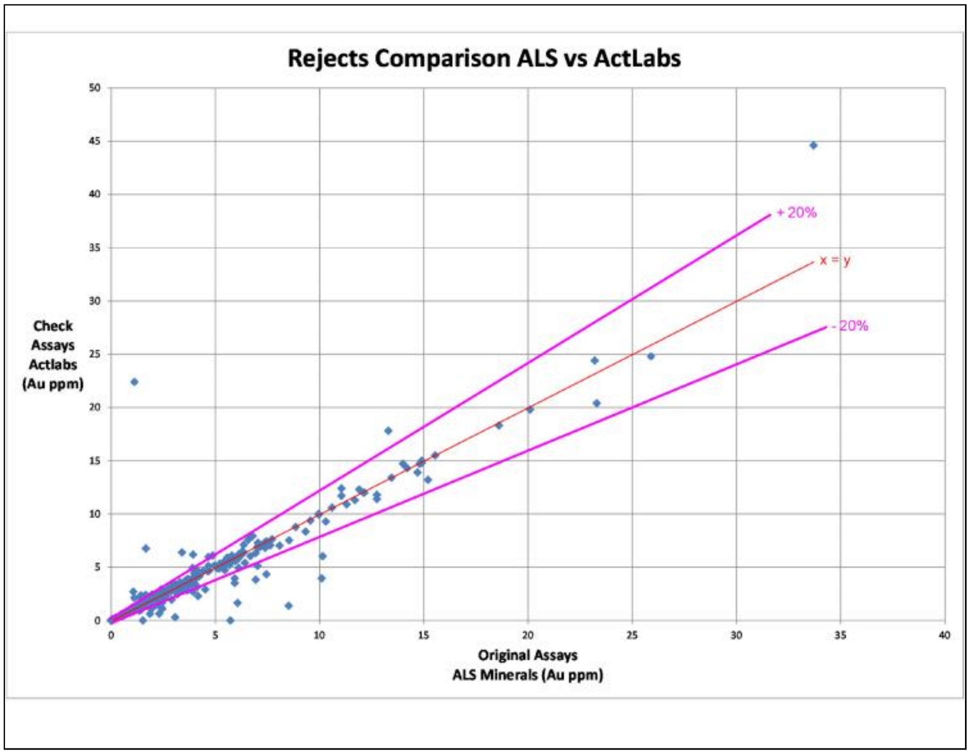

FIGURE 11-5 REJECTS COMPARISON ALS VS ACTLABS

The reject duplicates showed very good repeatability with 93% of the samples being within +/- 20% of the sample mean. The precision of the ALS analyses for holes GW10-45 to GW10-163 is very good when one takes into account the inherent natural variability of gold in rock or core samples.

PULP DUPLICATES

From hole GW10-164 onwards Gowest established a protocol of having ALS Labs forward a cut of the master pulp to Actlabs for pulp duplicate (check) analysis, at a rate of about 1 in 25 samples. To date a total of 72 pulp samples have been analyzed at Actlabs and the process is ongoing.

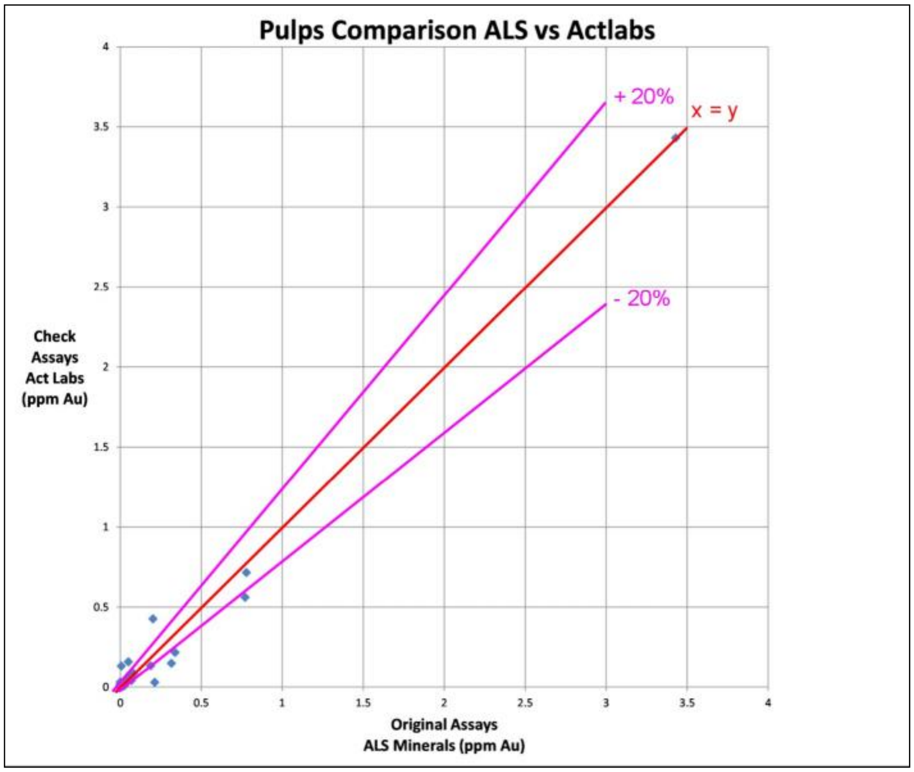

FIGURE 11-6   PULPS COMPARISON ALS VS ACTLABS

At the present time based on the number of samples it appears the precision of the ALS analyses is good.

11.4. QA/QC CONCLUSIONS

The QA/QC program at the Frankfield Gold project has allowed a broad assessment of analytical accuracy and precision since 2004. A total of 548 QA/QC samples amounts to 4.1 % of drill core samples (13,482 assays) have been assessed. There is no QA/QC data available for assays obtained prior to 2004 and when those assays are included the overall percentage of QA/QC samples drops to 3.2%.

Positive QA/QC results obtained between 2004 and 2008 at Swastika Laboratories, support previous assertions that despite the greater degree of uncertainty in Swastika assays obtained prior to 2004 due to the lack of QA/QC programs, they are suitable for use in resource estimation (Trinder, 2011).

Standards OREAS-16A and OREAS-16B performed well however, OREAS-19A standard results from the ALS laboratory indicate a slight occasional bias towards under-reporting of gold grades. Under-reported gold grades often occur as outliers associated with troughs in cyclical trends indicative of instrumental analytical drift. It is best practice to alert the assay laboratory when successive standard analyses are beyond 3 standard deviations from the standard value. If necessary, the batch should be reanalysed. The situation of successive standards beyond 3 standard deviations did not occur during the 2010 to 2012 Gowest drilling program.

The authors recommend that Gowest Gold maintain their thorough duplicate sample program involving the submission of core, reject and pulp duplicates to its primary assay laboratory (ALS) and check pulp duplicates to its secondary laboratory (Actlabs).

It is considered that QA/QC results provide sufficient confidence in assay values for use in the estimation of CIM compliant inferred and indicated resources. The number of QA/QC core duplicate analyses is low and there is no QA/QC for pre 2004 exploration.

12. DATA VERIFICATION

There have been a number of programs of verification sampling in the past. As well as the visit discussed below, verification sampling had been completed by A.C.A. Howe in 2011.

Mr. Neil Gow visited Timmins March 16, 2011. The offices of Gowest were visited and log from a number of holes was examined. Logging and sampling were found to be reliable and the drill logs were accurately maintained. Gow also visited the Gowest property. Drilling was in progress at the time of the visit. Various collar sites were visited. Work was proceeding satisfactorily.

Eight core samples were taken by quartering as a test of the previous sampling and assay. These samples were selected to test a range of values with a concentration on values close to the likely cut-off grade of the mineral resource to give some indication of reliability at this important level. Table 14-1.shows the sample data and results.

TABLE 12-1 CHECK SAMPLE RESULTS

Frankfield Property – Gowest Amalgamated Resources Ltd.

Sample ID	Hole ID	From (m)	To (m)	Length (m)	Original Value g/t Au	Check Value g/t Au
503109	GW10-113	38.0	38.5	0.5	4.42	3.8
503110	GW10-113	39.1	39.7	0.6	2.29	1.33
503111	GW10-114	60.8	61.8	1.0	3.62	3.99
503112	GW10-114	61.8	62.6	0.8	1.885	4.03
503113	GW10-114	70.7	71.4	0.7	6.49	6.59
503114	GW10-119	125.9	126.3	0.4	2.21	1.78
503115	GW10-125	38.9	39.3	0.4	1.755	1.72
503116	GW10-125	36.4	37.0	0.6	2.53	1.8

These results are interpreted to indicate reasonably good correlation for the number of samples collected. It is noticeable that there is good correlation for the samples close to 2 g/t Au. The mineralization of the Gowest deposit is fine grained and does not lend itself to sample selectivity. Further, there is no significant nugget effect.

13. MINERAL PROCESSING AND METALLURGICAL TESTING

13.1. GENERAL

Chapter 13 of this report is taken from the report of Ling and Trinder, (2012).

13.2. 2008 TESTWORK

Bradshaw (2008) reported on preliminary metallurgical tests undertaken by Gowest at SGS Lakefield Research Limited (SGS) in 2008.

A gold deportment study was completed to examine the distribution of the gold in the Frankfield East mineralized samples. The study consisted of a microscopic evaluation for visible gold and secondary ion mass spectroscopy (SIMS) for the quantification of submicron gold in sulphide particles. The study concluded:

- Approximately 4% of the gold in the ores sample occurred as visible gold with an average size of 13 microns.
- 96% of the gold in the sample exists as submicroscopic gold within the mineralization particles.
- The main submicroscopic gold carrier in the mineralization is arsenopyrite.
- The mineralization's pyrite content is only a minor carrier of submicroscopic gold.
- Gold content in the arsenopyrite grains ranged from 130 to +200 ppm while that in the pyrite grains was generally on the order of a few ppm or less.

Direct cyanidation testwork was completed at SGS in 2008. The goal of this testwork was to determine the response of the Frankfield East mineralization to direct cyanidation. The testwork program consisted of grinding the sample to approximately 80% minus 45 microns. A series of 6 cyanidation tests were then performed at 48, 72 and 96 hours with carbon additions of 0 and 15 g/L for each leach period.

The cyanidation tests with no carbon addition resulted in a gold recovery to solution of 5%. With carbon addition, the gold recoveries ranged from 6 to 9%. Cyanide consumptions for all the tests were reasonable and ranged from 1-2.4 kg/t. Lime consumptions ranged from 0.7-1.2 kg/t.

It was concluded from the direct cyanidation testwork that the gold in the Frankfield East mineralization is refractory and is contained within the mineralization's sulphide content. It appears from the testwork that the carbonaceous content (organic and graphitic) in the mineralization is low and unlikely to present problems for processing via cyanidation.

Preliminary flotation studies on the Frankfield East composite sample were performed at SGS in 2008 to examine gold recoveries to a concentrate. Testwork consisted of a rougher flotation step followed by a two-stage cleaner flotation. Gold recovery during rougher flotation was 90% into a concentrate that consisted of 21% of the original sample mass. The recovery curve at this point remained quite steep and therefore it is expected that recovery improvements could be achieved by increasing mass recovery. Gold and arsenic recoveries to the concentrate were almost identical due to the fact that the vast majority of the gold in the Frankfield East mineralization is submicroscopic and contained within arsenopyrite. Cleaner flotation testwork produced a final high grade sulphur/iron/arsenic concentrate assaying 34% iron, 32% sulphur, 16% arsenic and 44 g/t gold. Overall gold recovery to the cleaner concentrate was 78%.

Due the refractory nature of the Frankfield East mineralization, some preliminary pressure oxidation testwork was performed at SGS in 2008. The testwork consisted of grinding the composite sample to a size of 80% passing 50 microns followed by a rougher flotation stage to produce a gold-bearing concentrate for pressure oxidation. Pressure oxidation was performed in an agitated batch reactor with oxygen injection for sulphide decomposition. The reactions were allowed to occur for a period of two hours at a temperature of $200^{O}C$ and an operating pressure of 310 psig (75 psig of oxygen over pressure). Following pressure oxidation, the residue solids were filtered from the slurry and subjected to 48 hours of conventional cyanidation with the addition of 10 g/L of carbon to the slurry. The overall gold recovery to solution during cyanidation of the pressure oxidation residues was 98%. Silver recovery was lower at 41%. Cyanide consumption was reasonable at 1.1 kg/t of solids. As a result of the promising initial results additional testwork was recommended to better define the optimal parameters for pressure oxidation of the Frankfield East mineralization.

13.3. 2010/11 METALLURGICAL TESTWORK

A series of metallurgical testwork has been completed for the Frankfield East deposit. The information presented in this section is based primarily on testwork performed by SGS Canada (Lakefield), Ontario and follows industry accepted standard practices.

Additional testwork performed as part of the ongoing metallurgical evaluation of the Frankfield East deposit also involved:

- Golder Associates Ltd., ON
- McGill University, QC

13.3.1. METALLURGICAL SAMPLE PREPARATION

In 2010 Gowest drilled a series of HQ size drill holes for the purpose of generating a composite sample for metallurgical testing. The holes were located adjacent to two existing exploration holes – GW06-33/38 – which were located approximately 100m apart and intersected significant intervals of typical Main Zone style mineralisation.

Preparation of the drill core for metallurgical testwork was performed in Timmins. The Main Zone core sections were removed in ~1 metre intervals and individually bagged for shipping. A total of 181 sample bags were delivered to SGS Canada in large crates. Samples were received at SGS approximately 8 kg each representing ~1 meter of drill core (HQ). The samples were individually inventoried and weighed then crushed to 100% passing ¼ inch. A single 500 g sample was riffled from 30 randomly selected intervals to be reserved for comminution tests (crusher work index (CWI), ball mill work index (BWI), and abrasion index (Ai) tests). The remaining material was crushed to 100% passing 10 mesh. A 250g aliquot of each sample was riffled out and pulverized. From the 181 pulverized aliquots, a sample of each was submitted for gold analysis and ICP scan.

A 250 kg master composite sample (MC1) was prepared by combining the 32 individual intervals with head assays in excess of 2 g/tonne gold. The head grade of the MC1 composite was 5.95 g/tonne

Au. A detailed analysis is included as Table 13-1. The MC1 composite was used in flotation, pressure oxidation and bacterial oxidation testwork as described in the remainder of this section.

TABLE 13-1 ANALYTICAL SCAN OF MC1 COMPOSITE

Element	Assays
Au g/t	5.95*
S %	3.43
$S^=$ %	3.30
Semi Quantitative ICP Scan	
Ag g/t	< 2.00
Al g/t	53000
As g/t	2800
Ba g/t	32.00
Be g/t	< 0.50
Bi g/t	< 20
Ca g/t	39000
Cd g/t	< 10
Co g/t	45.0
Cr g/t	56.0
Cu g/t	75.0
Fe g/t	93000
K g/t	4400
Li g/t	< 5

Element	Assays
Semi Quantitative ICP Scan	
Mg g/t	14000
Mn g/t	2100
Mo g/t	< 5
Na g/t	33000
Ni g/t	28.0
P g/t	420
Pb g/t	< 40
Sb g/t	35.0
Se g/t	< 30
Sn g/t	< 20
Sr g/t	59.0
Ti g/t	8300
Tl g/t	< 30
U g/t	< 20
V g/t	290
Y g/t	25
Zn g/t	98

Subsequent to the preparation of composite MC1 a second series of HQ drill holes was completed to provide additional metallurgical testwork feed material (Master Composite 2 – MC2). These holes were drilled in the same general locations and prepared using the same procedures outlined for composite MC1. A comparison of the head assays for the two composites is presented in Table 13-2

TABLE 13-2 HEAD ANALYSES OF MASTER COMPOSITES

Element		Master Comp 1	Master Comp 2
Gold	g/t Au	5.95	6.75
Sulphur	% S	3.43	2.79
Sulphide Sulphur	% $S^=$	3.30	NA
Arsenic	% As	2.19	1.81
Iron	% Fe	9.3	NA

Sample MC2 was divided and utilized primarily to prepare larger representative sulphide concentrate samples for analysis by third party groups interested in processing the Frankfield East flotation concentrate. These samples were also utilized for filtration and thickening data as well as pressure oxidation optimization studies that are currently underway at SGS Canada.

13.3.2. MINERALOGY STUDIES

Early on in the recent exploration activities (subsequent to 2008) it was determined that the mineralogy at Frankfield East was unlike many of the more “conventional” gold deposits in the Timmins area. Although highly silicified, the mineralized zones are largely absent of large structures of white quartz and visible gold. Instead, the brecciated and altered host rock is filled with fine sulphides that comprise anywhere from a few percent to in excess of 30% of the overall rock matrix. Historically, the zones were further subdivided into “main zone” material located close to the contact between the mafic and ultramafic rock units and a series of sub-parallel “hanging wall” zones that were more distal to the contact and somewhat different visually with more apparent bleaching and quartz veining.

Prior to the initiation of the 2010/11 metallurgical testwork program a series of rock samples from different zones within the deposit were subjected to a program of QEMSCAN™ and XRD analysis (SGS Lakefield) to identify the type and nature of the mineral species present in the deposit. The results of this program provided insights into the physical characteristics of the deposit. This included:

- Arsenopyrite and pyrite were the primary carriers of gold with the fine gold grains (submicron to 10 microns in size) being largely attached to or locked within the sulphides.
- Sulphide minerals were comprised almost exclusively of pyrite and arsenopyrite with variations in the ratio of these species in the different mineral zones.
- Sulphide grain sizes were very similar in the different ore zones (main vs. hanging wall) with >80% liberation at a particle size of 20-30 microns.
- The non-sulphide minerals in the different ore zones were relatively similar with the exception of a quantity of micas/clays in the hanging wall areas that was largely absent in the main zone.

Overall, the QEMSCAN™ and XRD data confirmed that differences between the mineralization present in the historically identified main and hanging wall zones were in fact minimal and both areas should respond similarly to metallurgical treatments

13.3.3. FLOTATION

Gowest initiated an extensive program of flotation testwork at SGS in 2010/11. The program was divided according to two general methodologies. First, a bulk concentrate was produced containing both the pyrite and arsenopyrite. After this work was completed a second part of the program examined the production of separate pyrite and arsenopyrite concentrates. In both cases, cleaning stages were utilised to upgrade the initial rougher concentrate. Following the completion of the single stage batch tests a program of locked-cycle tests was completed to simulate the operation of the flowsheets with recycling of the intermediate products.

13.3.3.1. BULK SULPHIDE FLOTATION

Bulk sulphide flotation resulted in high gold recoveries. With staged additions of sodium hydrosulphide and potassium amyl xanthate, 96% of the gold was recovered to a concentrate containing 25% of the feed mass and assaying 21 g/t Au, 12% S and 7.4% As. It was possible to lower the mass recovery of the concentrate material to less than 16% by adding sulphide cleaners after the rougher circuit. The batch results are summarized in Table 13-3.

TABLE 13-3 BULK CLEANER FLOTATION TEST RESULTS

Product	Wt	Assays, g/t, %			% Distribution		
	%	Au	S	As	Au	S	As
2nd Cl Concentrate	15.5	36.1	21.0	12.7	93.2	93.1	92.2
1st Cl + Cl Scav Conc	23.7	24.5	14.3	8.64	96.4	96.6	95.8
Rougher Concentrate	33.7	17.4	10.1	6.15	97.7	97.5	97.2
Rougher Tailing	66.3	0.21	0.13	0.091	2.3	2.5	2.8
Head (calc)	100.0	6.00	3.49	2.13	100.0	100.0	100.0

*Test F16 – SGS Project 12416-001 Final Report (June 29, 2011)

The results of the bulk concentrate batch testwork completed to date indicate the potential for recovery of up to 98% of the gold during rougher flotation into a concentrate that represents approximately 25% of the initial ore mass (assuming recycle of middlings). Cleaner flotation is able to upgrade this concentrate resulting in a product with a final mass representing 15-20% of the initial ore mass and a gold grade of 30-35 g/t Au.

13.3.3.2. SELECTIVE ARSENOPYRITE-PYRITE FLOTATION

Bulk sulphide flotation was able to recover the gold into a concentrate with high gold recoveries for further processing. In order to reduce the amount of material being shipped and/or processed and therefore to reduce overall processing costs, selective arsenopyrite-pyrite flotation was investigated. The opportunity for a selective flotation process results from the strong association of gold and arsenopyrite in the Frankfield East deposit.

For the production of separate pyrite and arsenopyrite concentrates two different general flowsheets were examined:

- bulk flotation followed by separation of the pyrite/arsenopyrite and
- sequential flotation.

Although both arrangement were promising it was determined that the sequential flotation process offered advantages in maintaining high gold recoveries while also providing better concentrate upgrading (higher gold grade in final concentrates). The sequential flotation flowsheet was optimized using single stage tests and then simulated with a final locked-cycle program.

In the sequential arsenopyrite-pyrite process the ore was ground with lime and conditioned at pH 11 in order to depress pyrite flotation. Stage additions of CMC for gangue depression, copper sulphate for arsenopyrite activation and a thionocarbamate as a collector were made to selectively recover an arsenopyrite rougher concentrate containing 92% of the gold, 18% of the pyrite and 90% of the arsenopyrite. The results of the best batch test are shown in Table 13-4.Subsequently, three locked cycle tests (LCT) were conducted to investigate the effect of recirculating middling streams on the sequential arsenopyrite-pyrite flotation process. The test LCT3 flowsheet is shown in Figure 13-1. The projected results from these cycle tests are presented in

Table 13-5.

Overall, the locked cycle testwork program was able to recover 92-93% of the gold into an arsenopyrite cleaner concentrate with 6-7% of the original ore mass. The grade of this concentrate was +90 g/t Au. The final pyrite concentrate contains ~1.5% arsenic with a mass recovery of approximately 5%. The effectiveness of the selective flotation process at separating and concentrating the sulphide minerals is apparent when examining the final concentrates. The combined arsenopyrite + pyrite concentrate has the same overall gold recovery that was achieved in the prior bulk flotation testwork with only half of the concentrate mass. Further optimization work is underway to determine the best conditions for maximizing gold grades and recoveries.

TABLE 13-4 RESULTS OF BATCH SEQUENTIAL ARSENOPYRITE-PYRITE FLOTATION TEST

Product	Wt %	Assays, g/t, %					Distribution, %				
		Au	S	As	Py*	Aspy*	Au	S	As	Py*	Aspy*
Aspy 2ndCl Conc	4.1	95.3	20.1	33.4	10.9	72.6	63.5	24.2	61.1	9.7	61.1
Aspy Ro Conc	10.8	52.3	12.0	18.7	7.5	40.6	92.2	38.3	90.3	17.9	90.3
Py Ro Conc 1	5.7	3.77	32.7	1.61	59.9	3.5	3.5	55.4	4.1	75.6	4.1
Py Ro Conc 1+2	8.0	3.72	24.7	1.63	44.8	3.5	4.9	58.4	5.9	78.9	5.9
Aspy + Py Ro Conc	18.8	31.6	17.4	11.4	23.4	24.8	97.1	96.6	96.2	96.8	96.2
Rougher Tailing	81.2	0.22	0.14	0.11	0.2	0.2	2.9	3.4	3.8	3.2	3.8
Head (calc)	100.0	6.11	3.38	2.23	4.5	4.8	100.0	100.0	100.0	100.0	100.0

*Test F17, SGS Project 12416-001 Final Report (June 29, 2011). Calculation based on the assumption that all arsenic was present as arsenopyrite and the remaining sulphur was present as pyrite

TABLE 13-5 PROJECTED RESULTS FROM LOCKED CYCLE TESTS

Test No.	Product	Wt %	Assays, g/t, %					Distribution, %				
			Au	S	As	Py*	Aspy*	Au	S	As	Py*	Aspy*
LCT3	Aspy 3rd Cl Conc	6.4	93.7	16.2	24.3	10.8	52.9	92.7	40.3	90.2	20.2	90.2
	Py Ro Conc	4.8	4.64	28.6	1.54	52.3	3.4	3.5	54.1	4.3	74.3	4.3
	Rougher Tailing	88.8	0.27	0.16	0.11	0.2	0.2	3.8	5.5	5.5	5.5	5.5
	Head (calc)	100.0	6.44	2.56	1.72	3.4	3.7	100.0	100.0	100.0	100.0	100.0

*calculation based on the assumption that all arsenic was present as arsenopyrite and the remaining sulphur was present as pyrite

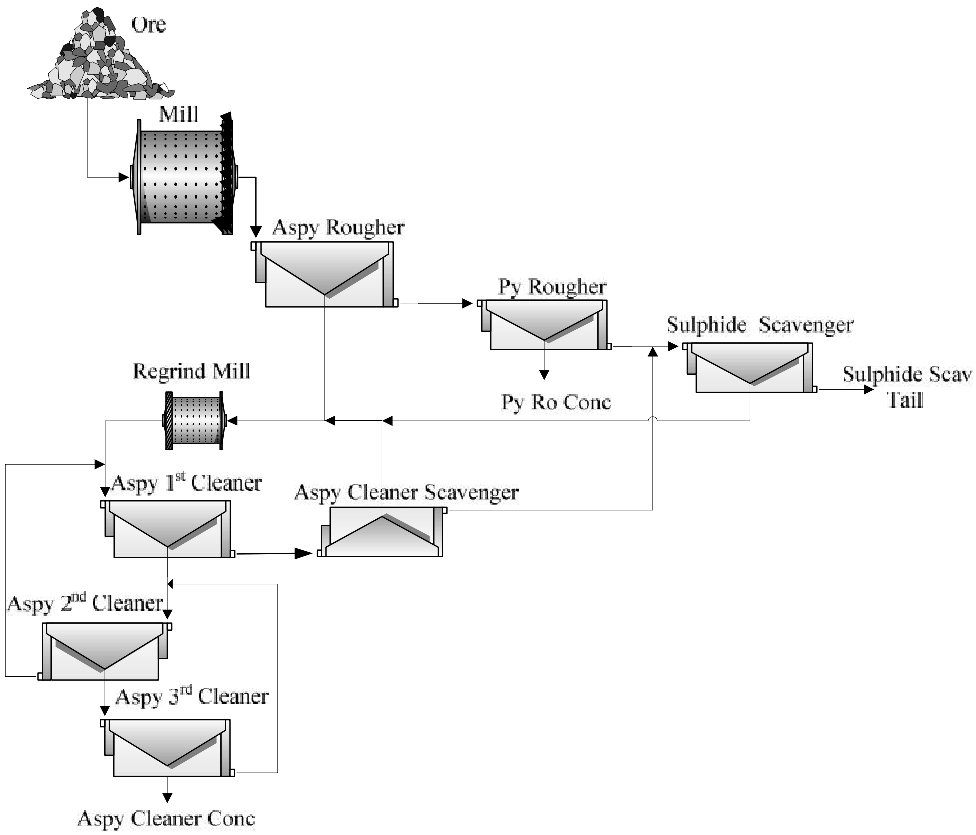

FIGURE 13-1 FLOWSHEET UTILIZED FOR LOCKED-CYCLE FLOTATION TESTWORK (LCT3)

13.3.4. PRESSURE OXIDATION

Pressure oxidation testwork (POX) was first commissioned by **G**owest and conducted at SGS in 2010 and more tests were completed in 2011. A bulk arsenopyrite/pyrite flotation concentrate was produced and subjected to pressure oxidation in a batch reactor under a range of conditions. Four POX tests were carried out to evaluate different test conditions, namely, retention time, acid concentration and partial acid recycling. The standard POX conditions are given below:

Agitation Speed = 720 rpm
Reaction Temperature: = 200^{o}C
Oxygen Flow = ~250 mL /min
Total Pressure: = 315 psi

Table 13-6 presented test results of test performed to date.

TABLE 13-6 RESULTS OF PRESSURE OXIDATION TESTS (2011)

POX Test No	Pre-Acidulation H_2SO_4 (kg/t)	Pre-Acidulation pH	POX Retention Time (min)	POX Final Filtrate Redox pot (mV Ag/AgCl)	Fe_T (mg/L)	Fe^{2+} (mg/L)	As (mg/L)	Acid (g/L H_2SO_4)	Molar ratio Fe^{3+}/Fe^{2+}	Molar ratio Fe/As	POX Final Residue Solid Mass change (%)	S_T (%)	S^{2-} (%)	**S^{2-} Oxidation (%)**
POX 1	85.6	1.8	60	505	17700	911	1930	39	18.4	12.3	-17.9	3.11	0.14	**99.0**
POX 2	85.6	1.8	120	575	13600	128	1820	40	105.3	10.0	-14.4	4.00	0.17	**98.8**
POX 3	57.0	3.5	90	520	13000	191	1530	38	67.1	11.4	-13.9	3.11	0.64	**95.4**
POX 4[#]	82.5	2.2	60	521	19700	202	2640	40	96.5	10.0	-15.1	3.81	0.17	**98.8**

*POX 4: the acid solution was made up of recycled acid solution from POX 1 &2 at 39.5 g/L H2SO4 and concentrated H2SO4 and demineralised water.

Following pressure oxidation, the residue solids were filtered from the slurry, neutralised and subjected to conventional cyanidation for gold recovery.

Cyanidation tests were performed on flotation concentrate directly and on concentrate after POX. The leach results are presented in Table 13-7 (Direct Cyanidation of Flotation Concentrate) and Table 13-8 (Cyanidation of Pressure Oxidation Residue). The leach retention time used was 48 hours for direct cyanidation and 24 hours for POX residue cyanidation.

TABLE 13-7 DIRECT CYANIDATION OF FLOTATION CONCENTRATE

Test No	Lead Nitrate (kg/t)		Residue Assays (g/t)		**Extraction (%)**		Calc Head Assays (g/t)		Reagent Consumption (kg/t CIL feed)	
	Preaeration	Cyanidation	Au	Ag	**Au**	**Ag**	Au	Ag	NaCN	CaO
CIL-1	0.0	0.0	17.7	0.8	**7.4**	**69.3**	19.1	2.6	5.42	2.23
CIL-2	5.5	0.5	21.4	1.0	**8.7**	**46.4**	21.4	1.9	0.62	0.69

TABLE 13-8 CYANIDATION OF PRESSURE OXIDATION RESIDUE

CIL Test No	POX Test No	Residue Assays (g/t)		**Extraction (%)**		Calc Head Assays (g/t)		**Reagent Consumption (kg/t CIL feed)**	
		Au	Ag	**Au**	**Ag**	Au	Ag	**NaCN**	**CaO**
CIL-3	POX 1	0.86	0.9	**96.5**	**60**	24.8	2.2	**0.51**	**2.03**
CIL-4	POX 2	0.51	1.4	**97.8**	**28**	22.8	1.9	**0.71**	**7.93**
CIL-5	POX 3	0.66	1.6	**97.2**	**35**	23.3	2.5	**0.43**	**2.67**
CIL-6	POX 4	0.73	2.2	**96.8**	**22**	22.9	2.8	**0.69**	**4.84**

Processing the Frankfield East Deposit mineralization via flotation followed by pressure oxidation and cyanidation produced overall gold extractions of 94-95% (total of flotation/POX/cyanidation). Other highlights include:

- Up to 99% oxidation of the sulphide minerals in the concentrate at 200 deg C with a retention time of 60 minutes
- High iron/arsenic ratios in the POX discharge solutions (good for production of stable arsenic precipitate)
- 97-98% gold extraction from the neutralized POX discharge solids with 24 hours of cyanidation
- low reagent consumptions for the cyanidation of the oxidized concentrates

Further optimisation studies are currently underway to optimise conditions including oxygen partial pressure and retention time.

13.3.5. BACTERIAL OXIDATION

Bacterial oxidation of the Frankfield East flotation concentrates was also examined as an alternative to pressure oxidation. Testwork was initiated in 2010 under the supervision of Goldfields (BIOX™ process) and performed by SGS (Booysens,South Africa). A bulk arsenopyrite/pyrite flotation concentrate was used for the testwork which was completed in stirred reactors that contained bacteria that attack the sulphide minerals in the concentrate. Following oxidation the solids were filtered from the slurry, neutralised and subjected to cyanidation for gold recovery. A summary of the results is shown in Table 13.6. Highlights include:

- Sulphide oxidation levels of +96% (100% arsenic solubilisation) after 5 days of bacterial oxidation and 98-99% after 10-15 days of treatment
- Gold dissolution of 95-96% from the oxidised solids
- Reasonable reagent consumptions were achieved

TABLE 13-9 FRANKFIELD EAST BACTERIAL LEACH RESULTS

BIOX®				Gold Dissolution (%)	
Treatment Period (days)	% Solids	Acid Consumption (kg/t)	Sulphide Oxidation (%)	Direct Cyanidation	After BIOX® Treatment
			0	3.52	
10	20	25.6	98.4		94.8
15	20	24.1	99.1		95.9
10	25	4.7	96.5		94.2
15	25	-24.0	98.1		96.0

A stage batch neutralisation test performed on the BIOX effluent indicated that a stable ferricarsenate precipitate can be produced using limestone and lime. The testwork results confirmed that the arsenic content in the neutralised effluents (<0.24 ppm) conforms to the US-EPA standards (EPA standard below 0.5ppm). The precipitates can therefore be considered stable for disposal to a tailings dam.

13.3.6. FLOTATION TAILINGS

Golder Associates Ltd. was retained to evaluate the geochemical characteristics of combined rougher / flotation tailings samples (which is the combined tailings from the Frankfield Project). Metallurgical testing of the flotation tailings was carried out at SGS Lakefield, Ontario. Bulk rougher and bulk cleaner flotation tailings produced during the flotation were blended in the relative proportions that would be produced during processing and then were used for geochemical testing.

Tests carried out as part of the geochemical characterization program include:

- Elemental chemical composition
- Acid Base Accounting (ABA)
- Net Acid Generation (NAG) testing
- Short-term leach testing, including de-ionized (DI) water leach testing, detailed analysis of the NAG leachate;
- Decant water analysis
- Kinetic testing.

Results of the ABA and NAG testing indicate that the combined tailings sample is non-acid generating. The tailings contain relatively low sulphide concentrations, and the complete oxidation of sulphide minerals is predicted to take significantly less time than the depletion of available neutralization minerals. The neutralization potential of the tailings is high, and comprised primarily of carbonate minerals, which provide significant buffering capacity. Humidity cell testing has achieved metal concentrations decreased to stable concentrations where depletion calculations indicate that it could take several years to deplete the sulphide and/or Neutralisation Potential (NP) from the sample.

14. MINERAL RESOURCE ESTIMATES

14.1. GENERAL STATEMENT

An updated mineral resource estimate was prepared for the Frankfield East deposit. This estimate is in accordance with the Mineral Resources/Reserves Classification as recommended by the CIM Committee on Mineral Resources/Reserves (CIM definitions). The estimates are set out in Table 14-1.

Estimate is based on drilling information up to February 2012.

TABLE 14-1 MINERAL RESOURCE ESTIMATE				
Frankfield East deposit –Gowest Gold Ltd.				
Indicated Resources				
Lens ID	**Volume**	**Tonnes**	**Oz Au**	**Grade g/t Au**
MZ1	521,908	1,487,438	241,497	**5.05**
MZ2	469,064	1,336,832	200,283	**4.66**
HWZ1	484,036	1,379,503	214,659	**4.84**
HWZ2	451,000	1,285,350	207,033	**5.01**
HWZ3	185,060	527,421	82,070	**4.84**
Totals	**2,111,068**	**6,016,544**	**945,542**	**4.88**
Inferred Resources				
Lens ID	**Volume**	**Tonnes**	**Oz Au**	**Grade g/t Au**
MZ1	995,816	2,838,076	425,198	4.66
MZ2	33,232	94,711	9,987	3.28
HWZ1	189,852	541,078	69,409	3.99
HWZ2 (50m)	41,856	119,290	16,951	4.42
HWZ3 (50m)	34,988	99,716	15,228	4.75
Totals	**1,295,744**	**3,692,871**	**536,773**	**4.22**

Notes:
1. CIM (Canadian Institute of Mining, Metallurgy and Petroleum) definitions were followed for Mineral resources.
2. Mineral Resources are estimated at a cut-off grade of 3 g/t Au.
3. Mineral Resources are estimated at a long-term gold price of US$1,200/oz, and a US$/C$ exchange rate of 1:1.
4. A minimum width of 2 m was used.
5. The mineral Resource estimate is based on drilling up to February 2012.

The mineral resource estimates reported here were completed by a geologist, Ms Angela Falcon, trained in the use of Surpac 6.3.1. This work was supervised by Gow and Montgomery and both authors had input into the details of the methodology.

14.2. DATABASE

The current mineral resource estimate consists of 292 drill holes that intersected at least one of the mineralized lenses with an aggregate length of 86,408 m.

The first step required the development of an appropriate database that was up-to-date. Steps were taken to validate the database. Once the database was updated, a three-dimensional model that incorporated the various intersections was developed. As noted above, the Frankfield mineralization is present in a number of sub-parallel east-west striking lenses.

The rock density is based on readings taken in the laboratory. All of the samples from the holes drilled in the current campaign that were assayed were also tested for rock density. A reading of 2.85 was accepted as the appropriate value for the density of mineralization.

14.3. GEOLOGICAL INTERPRETATION AND 3D SOLIDS

After the database was validated, a deposit model was developed. Mineralization is present in a number of subparallel lenses.

A block model was developed with blocks 2 m X 2 m X 1 m. The small block size was selected because the individual zones of mineralization are relatively narrow. A topographic surface was digitized from drill hole collar data and the bedrock/overburden surface was also obtained from drill hole data.

A wire frame was prepared. Ultimately, a hybrid wire frame boundary was prepared. While a 1 g/t Au boundary was used for many of the intersections in places the boundary was set at 3 g/t Au. The wireframe model is shown in Figure 14-1

Attempts were made to develop semivariograms for the data but none of these were considered stable enough to allow geostatistics to be employed. As a result, grades were interpolated into the model blocks using ID2.

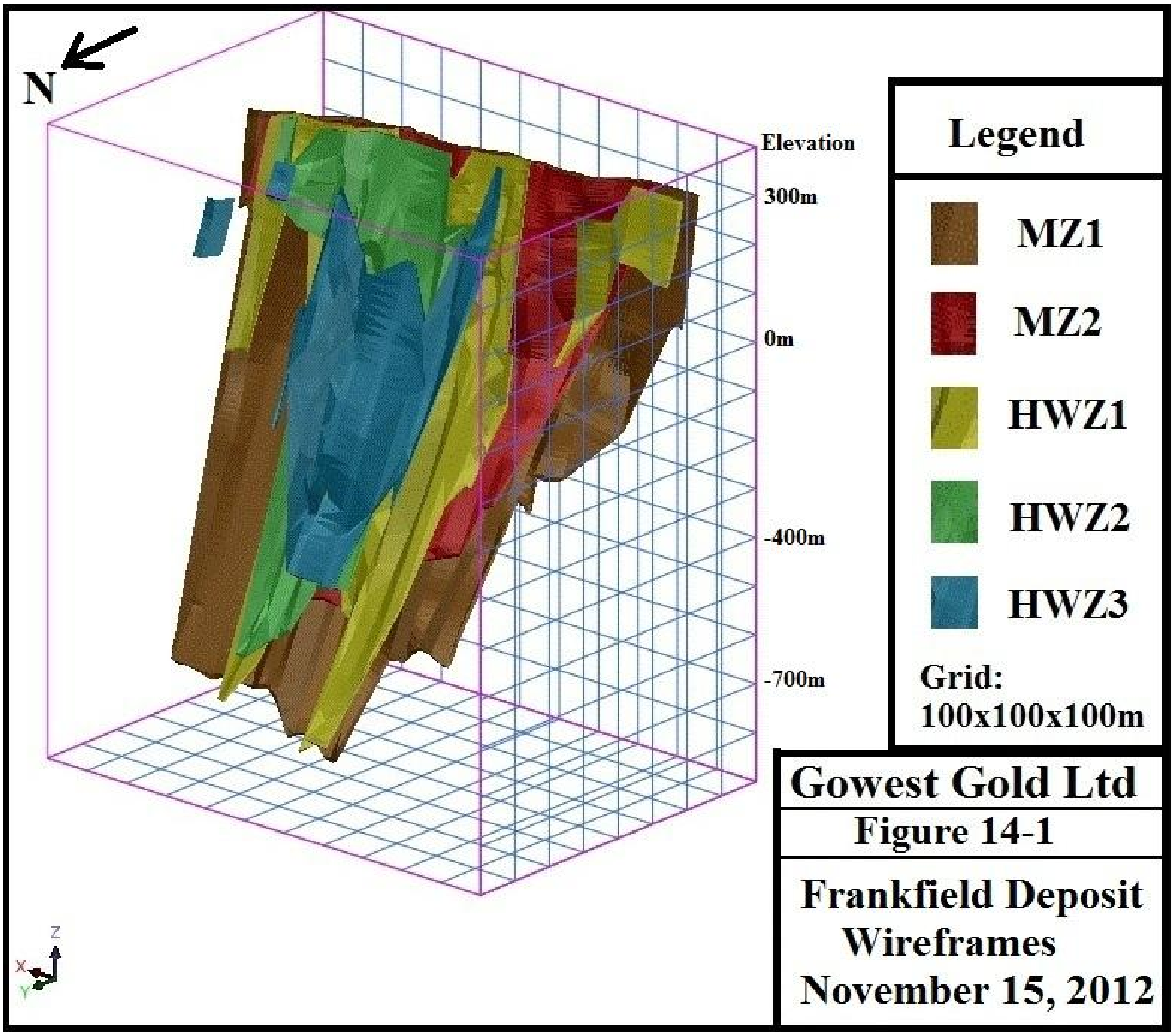

FIGURE 14-1 WIREFRAME MODEL

14.4. CUT-OFF GRADE

A cut-off grade of 3 g/t Au was selected for the model. Based on analogy with other operations in the Timmins camp, this value was considered appropriate. Separately, based on a conservative gold price of US$1,200/oz gold and operating costs and treatment costs taken from the PEA of Ling and Trinder (2012), a cut-off grade of 3.0 g/t Au is seen to also be conservative.

14.5. COMPOSITING AND STATISTICS

Basic statistics for all of the drill hole assays used in the preparation of the estimate are listed in Table 14-2.

TABLE 14-2 BASIC STATISTICS OF THE DRILL HOLE ASSAYS		
Frankfield Deposit – Gowest Gold Ltd.		
Statistics	**Core Length**	**Au Grade**
N=2,662		
Mean	0.97 m	2.17 g/t Au
Median	1.0 m	0.36 g/t Au
Maximum Value	2.35 m	39.5 g/t Au
Standard Deviation	0.28	4.07
Coefficient of Variation	0.28	1.88

The assays were composited into 1 m intervals downhole for intersections within the mineralized lenses. Basic statistics for the composite data are shown in Table 14-3.

TABLE 14-3 STATISTICS OF DRILL HOLE COMPOSITE ASSAYS		
Frankfield Deposit – Gowest Gold Ltd.		
Statistics	**Core Length**	**Au Grade**
N=2,045		
Mean	0.97 m	2.27 g/t Au
Median	1 0 m	0.88 g/t Au
Maximum Value	1 0 m	25.0 g/t Au
Standard Deviation	0.10	3.52
Coefficient of Variation	0.11	1.55

14.6. BLOCK MODEL AND GRADE INTERPOLATION

The block model was developed with blocks 2 m X 2 m X 1 m with the 1 m dimension across strike to compensate for the relative narrowness of the deposits. Grade interpolation was carried pout using inverse distance squared (ID2) using a 100 m search radius for the Main Zones and for the Hangingwall Zones about -100 m Reference Level (RL). Below -100 m RL, a 50 m search radius was used for the Hangingwall Zones 2 and 3. In reality drill holes spacing above -100 m RL, was significantly closer than 100 m and the margins of the deposit were clipped at shorter distances than 100 m. In the Main Zones, the 100 m search radius was required to join up apparent mineralized shoots. Drilling in the Hangingwall Zones is not close enough to define apparent mineralized shoots and the lesser search radius was selected. Two block model sections, Figures 14-2 and 14-3, are shown depicting the block model.

14.7. CLASSIFICATION OF MINERAL RESOURCES

The drilling used to estimate mineral resources is not uniformly distributed. Drilling is much more closely spaced above -100 m RL and more widely spaced below -100 m RL. The better tested parts of the deposit are judged to meet the CIM requirements for an Indicated Mineral Resource, while below -100 m RL, the mineralization is classified as Inferred Mineral Resources.

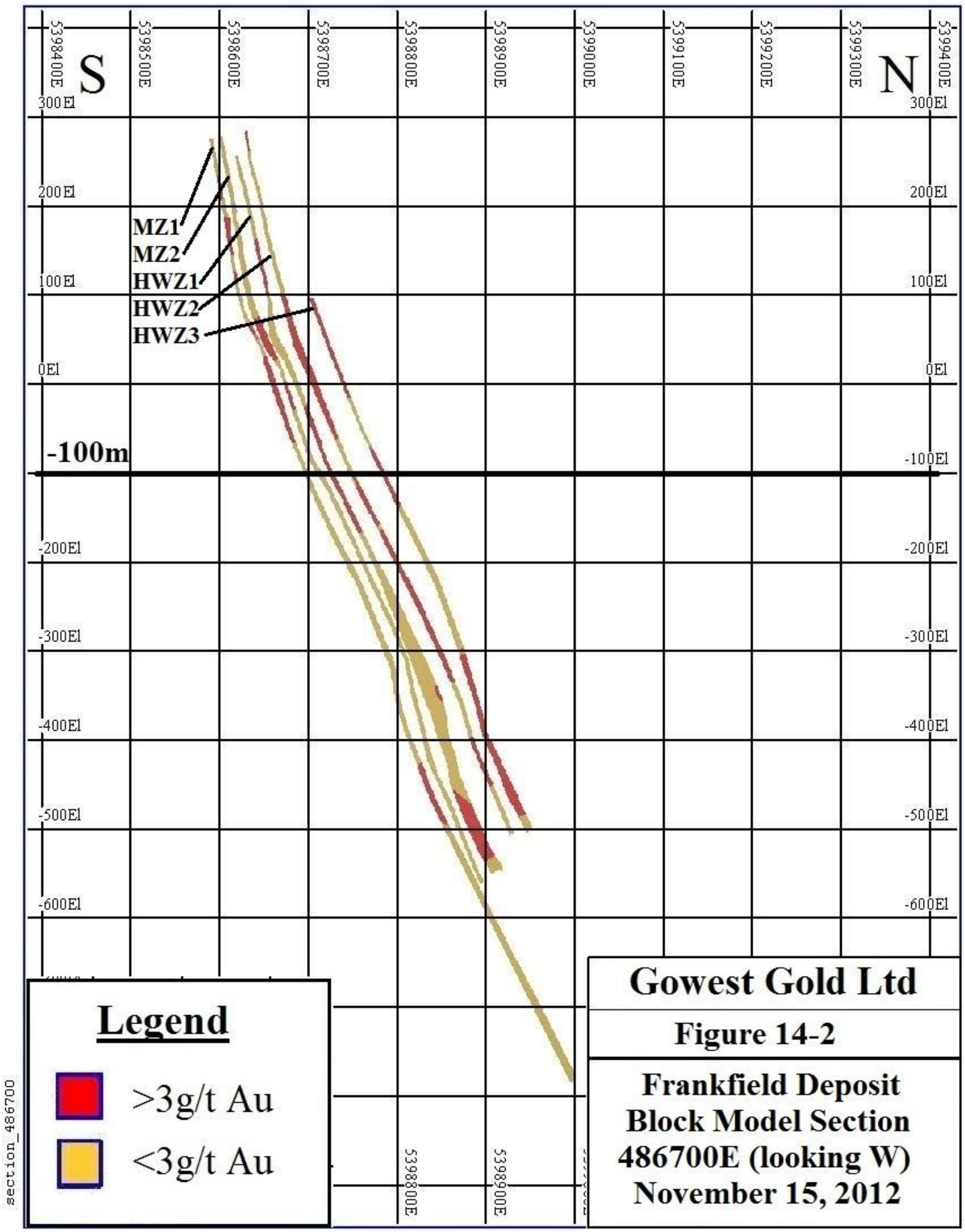

FIGURE 14-2 SECTION 486700, SHOWING MODELING

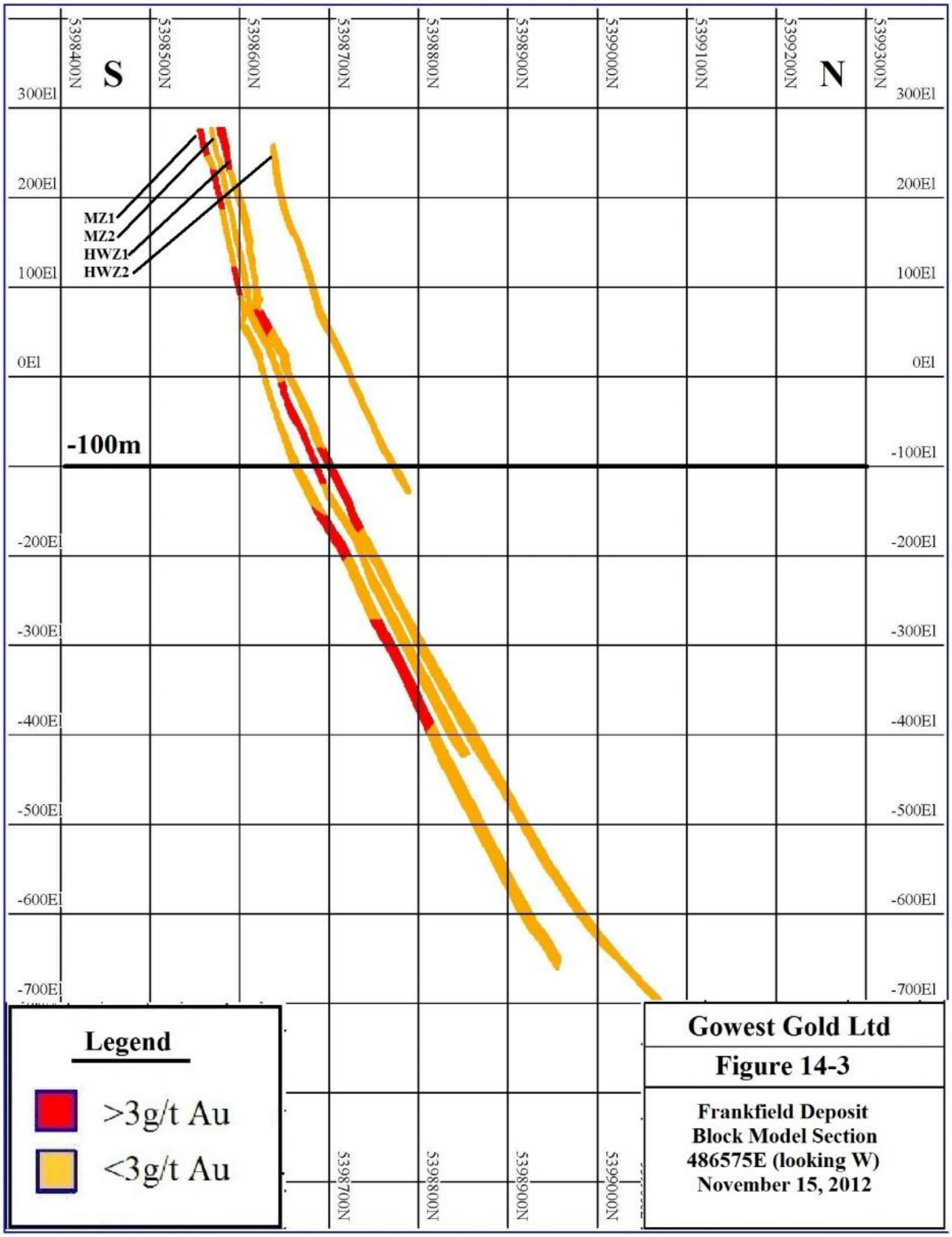

FIGURE 14-3 SECTION 486575, SHOWING MODELING

15. MINERAL RESERVE ESTIMATES

No Mineral Reserve estimates have been prepared for the deposits on the Frankfield claims at this time.

16. MINING METHODS

16.1. GENERAL

This section was taken from "Preliminary Economic Assessment on the Frankfield Gold Project, Tully Township, North-Eastern Ontario" by Ling and Trinder, 2012.

16.2. INTRODUCTION

A conceptual mine development plan was prepared and used as the basic for the capital and operating cost estimates contained in the preliminary economic assessment (PEA). The level of detail is considered sufficient for a PEA but should be considered as preliminary only and subject to changes as more advanced planning activities is completed.

Sections through the deposit were prepared on 25-m spacing showing the exploration drill holes with the mineralized intervals identified on each hole. Intervals were connected vertically based on geological interpretations to estimate the extents of the parallel zones present throughout the deposit. Drill log information related to the lithologies and alteration patterns was utilized to aid in the interpretation process. Following the completion of the sectional interpretations, 3D wireframes were prepared to outline the individual mineralized horizons. A total of six (6) zones were identified with the bulk of the mineralization contained within the "main zone" area and first two "hanging wall zones".

Sections (see Figure 16-1) and elevation plans (see Figure) were prepared on 25-m intervals from the 3D wireframe model. Included in the plans were the outlines of the mineralized zones and the drill hole grade intervals as well as a range of geotechnical information (including RQD) that was obtained by Gowest from its 2010/11 exploration drill program. This information served as the basis for establishing a preliminary mine plan for the deposit. Also shown for reference in Figure is a conceptual site layout and trace of the initial pre-production ramp access.

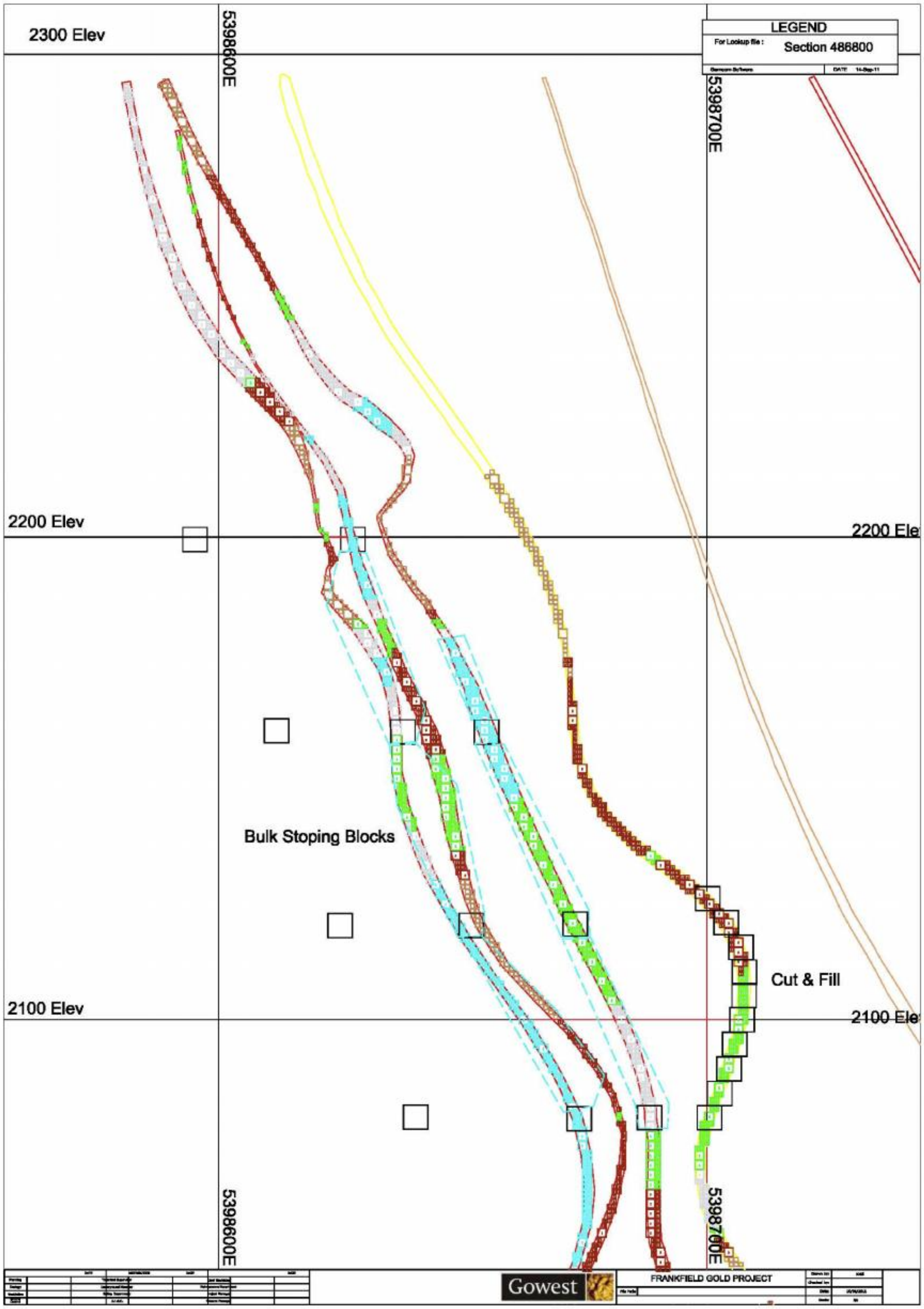

FIGURE 16-1   TYPICAL SECTION SHOWING MINERALIZATION AND CONCEPTUAL MINING BLOCKS

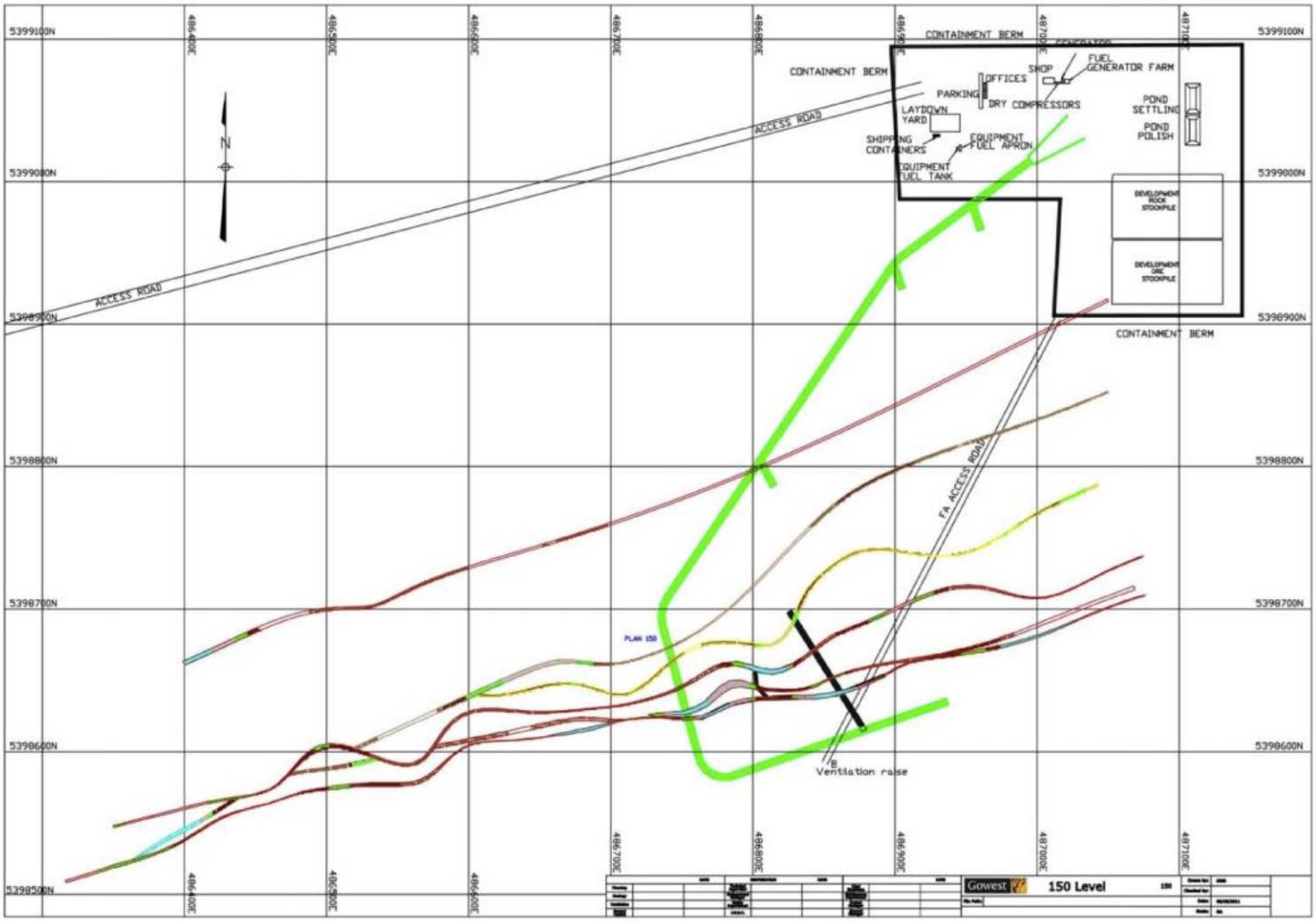

FIGURE 16-2 SURFACE LAYOUT WITH "150 LEVEL" PROJECTIONS

16.3. MINING METHOD

The Frankfield East deposit resource consists of bulk mining areas as well as narrow vein sections. The two main mining methods selected for this phase of the mine evaluation are open stoping and shrinkage. Open stoping was selected where the geometry of the deposit appeared regular between sublevels. Shrinkage was suitable where a more selective technique was required in areas that are more irregular and thinner. Mechanized cut and fill is an alternate technique that might also be considered in the future within narrower portions of the deposit. This combination of open stope and narrow vein mining is common within the Timmins camp.

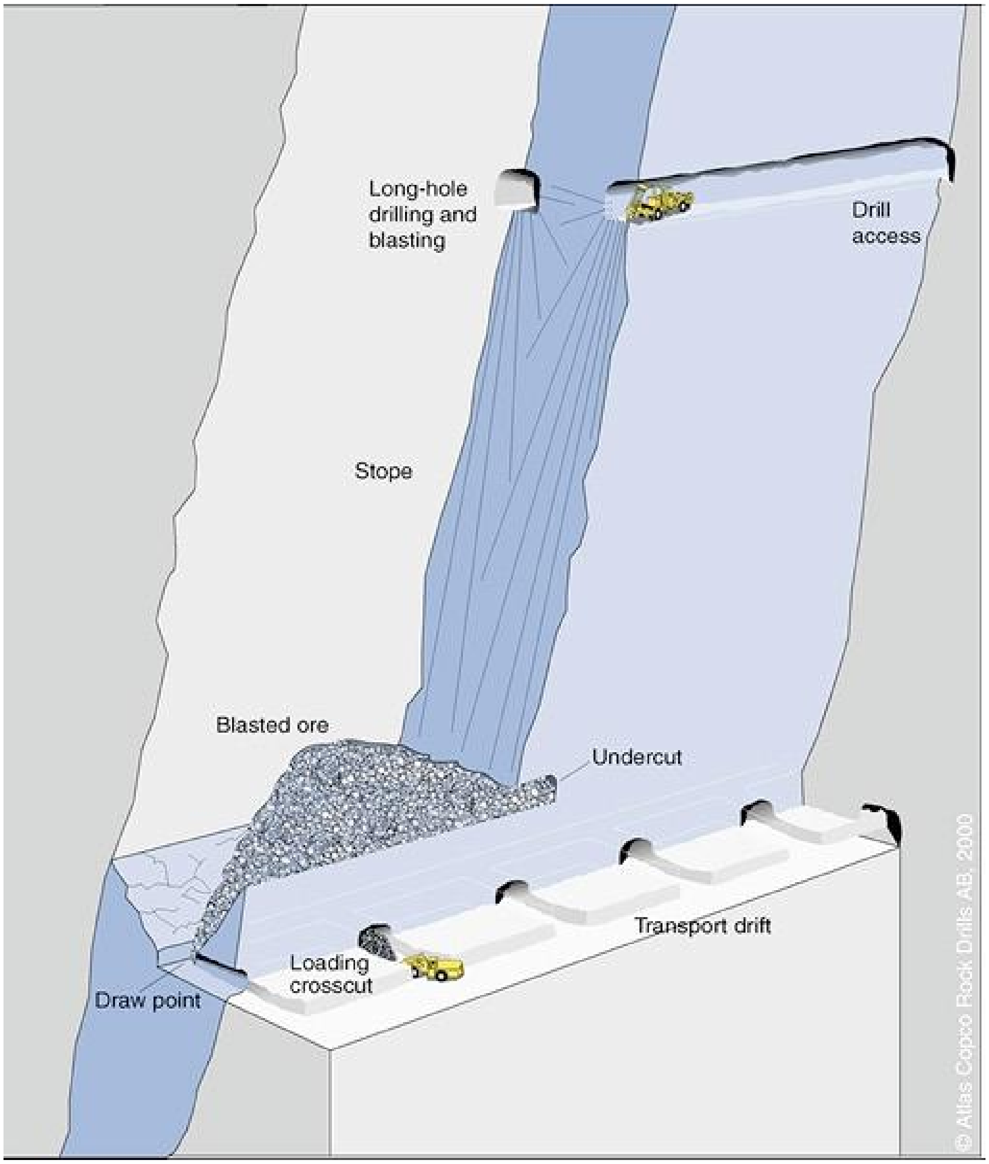

FIGURE 16-3   TYPICAL BULK MINING STOPE

The overall mine plan envisions a predevelopment period where ramp access will be driven from surface down to the 200 m mine level. Following the initiation of commercial mining operations production will be supported exclusively via ramp access down to approximately the 400-450 m level. Following this an auxiliary shaft would be constructed to maintain mine production rates as the mining operations progress to greater depths.

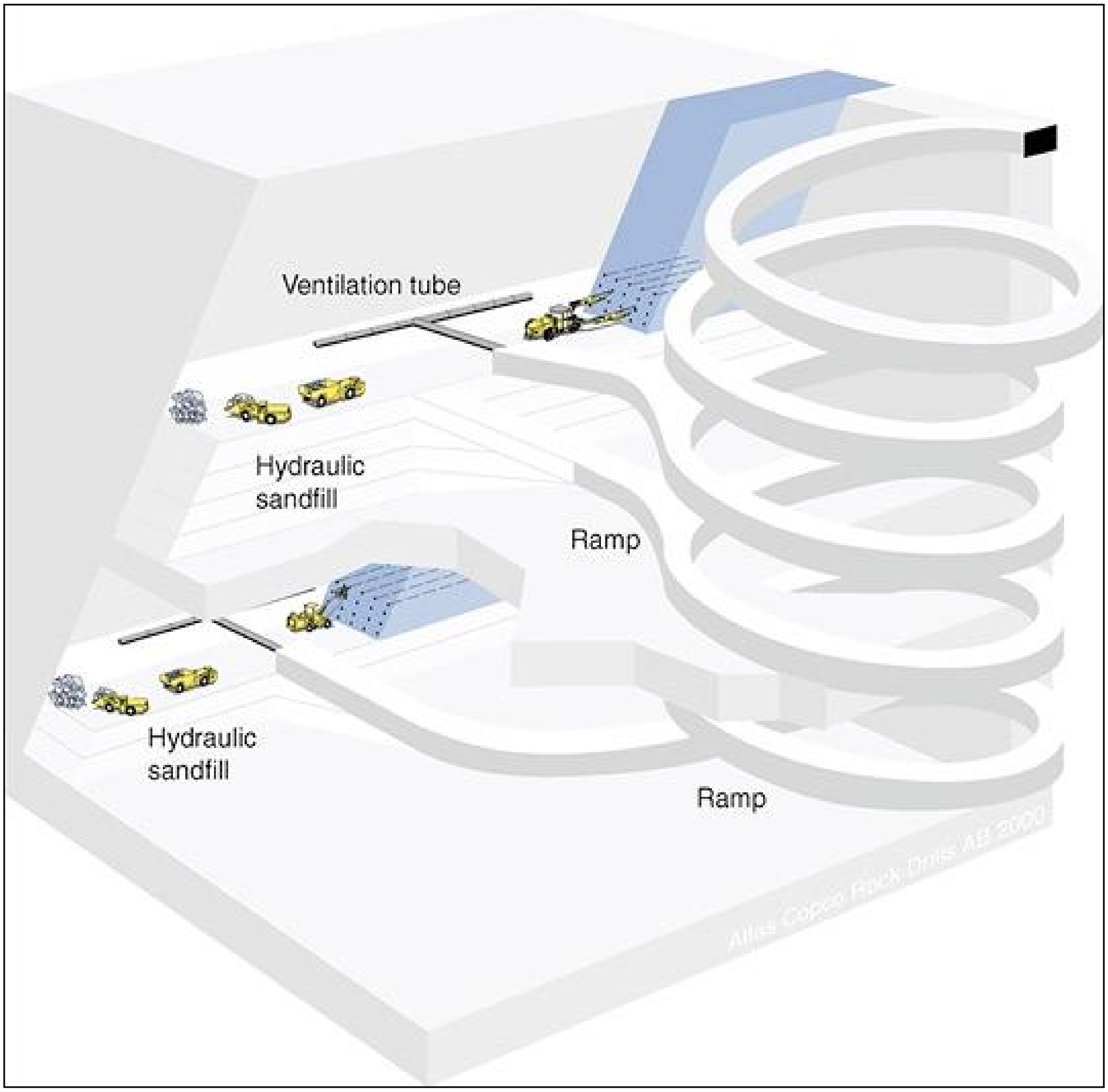

FIGURE 16-4 TYPICAL CUT AND FILL STOPE BLOCK

It is expected that the mine plan as currently conceived would allow for production rates of approximately 1500 tpd. Based on the current models, approximately 2/3 (or greater) of this extraction rate would come from open stopes and the remainder from shrinkage operations. As much as possible waste rock generated by underground mine development will be placed in mined out stopes to avoid hoisting/trucking it to the surface. Waste storage availability (determined by stope filling cycles) will be a critical parameter for future mine planning activities in order to determine the total ratio of waste that can be retained underground.

FIGURE 16-5 TYPICAL ALIMAK MINING METHOD (NARROW ZONES)

Taking into account the fact that areas of the mine don't require backfill and can be left open for periods of time, it is currently estimated that the quantity of backfill required for the operation will be equivalent to approximately 35-40% of the mined ore production rate. The start of filling operations will be deferred for the first 1-2 years as underground operations are ramped up to full production levels. Existing sand and gravel pits are located within close proximity to the Frankfield East deposit and will be utilized for the preparation of mixed fill at the mine site. It is believed that deslimed flotation tailings from the Frankfield East processing plant can also be filtered and backhauled to the mine for use in the backfill mix. Tailings characterization studies will allow for a determination of the optimal backfill mix ratios.

It is assumed that all mining activities will be completed by a capable mining contractor experienced with normal operations in the Timmins camp. Contractor plans are based on a work schedule of two (2), 12- hour shifts per day, seven days per week.

16.4. MINE PREDEVELOPMENT

A conceptual mine predevelopment schedule was prepared and is included as Figure 16-8. Some details related to this plan are presented below.

16.4.1. MOBILIZATION

It is assumed that the existing road infrastructure is sufficient for the contractor to access the Frankfield East site. A one month period has been included to allow for site preparation and set up with portal excavation to follow. Manpower and equipment would be mobilized to (and demobilized from) the site in stages to accommodate the project schedule. These tasks will be completed quickly as the immediate equipment necessary to start the work is assumed to be available in the Timmins area. Estimates for mobilization prices include the supply of major electrical components including generators and substations.

16.4.2. SURFACE SET-UP

A site set-up plan has been developed and is included as Figure . Near the entrance to the property there would be a security gate house with four office trailers, mine dry and cold storage building being set up on the property. A pole line will be installed to provide power to the facilities in this area. The offices and dry in this area will be heated with propane to reduce the electrical loads. Adjacent to the surface breakthrough location of the fresh air raise will be the propane farm and mine air heaters.

Near the portal face will be the main working area for the project and will consist of:

- A new 40 foot wide by 80 foot long workshop that will be constructed on a concrete slab. The slab will add environmental protection against oil leaks, ensure proper cleaning and maintenance of equipment and provide a safer work environment for mechanics.
- A designated parking area will be established here for underground mobile equipment.
- Sea containers will be positioned in this area to provide covered storage/warehousing facilities.
- Generator plant with a dedicated 68,000L fuel tank.
- A fuel station dedicated to the fueling of mobile equipment complete with a 35,000L fuel tank and a concrete apron for the control of potential spills.
- An electric powered compressor plant with associated piping. A stench gas warning system will be located in the compressor plant with a second unit located adjacent to the intake fresh air.

The contractor will supply, install and maintain Type 4 cap and powder magazines which will meet the requirements of the Explosives Regulatory Division and the Ministry of Labour of Ontario. The magazines are sized to hold at least one week's explosives consumption. Once development is sufficiently advanced, magazines will be established underground in accordance with regulatory guidelines.

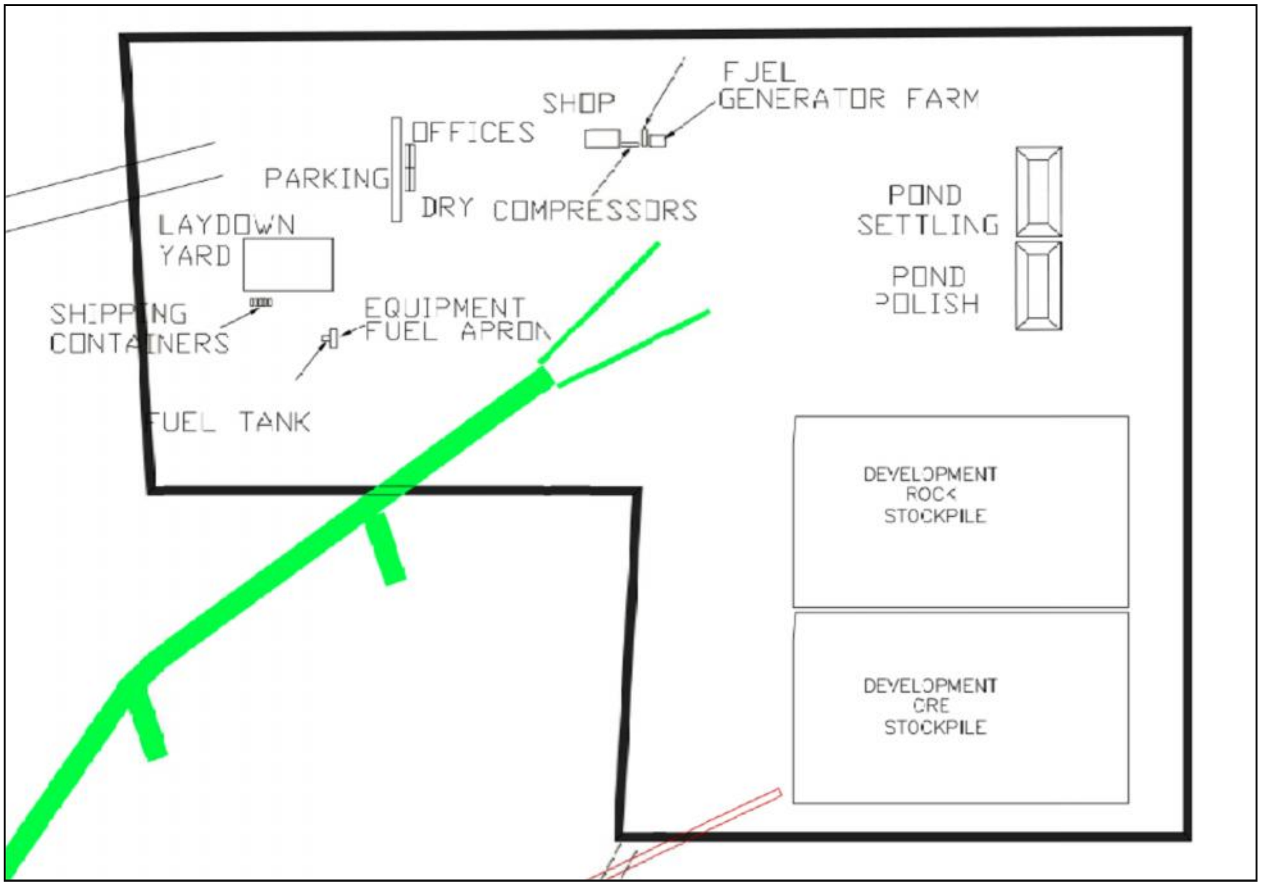

FIGURE 16-6 CONCEPTUAL SURFACE LAYOUT

16.4.3. PORTAL BOX CUT

The drilling and blasting of the portal area will be completed by a local contractor. Contractor will use broken muck to establish a work platform for the bolting equipment. Portal area ground support will consist of pattern bolting with 6 ft. fully grouted rebar on a 4-ft by 4-ft pattern. Shotcrete will be applied on the wall area of the portal and the brow of the portal at 2" thickness.

16.4.4. UNDERGROUND DEVELOPMENT

16.4.4.1. GENERAL

The 5 meter by 5 meter arched profile headings will be advanced using conventional drill and blast methods. Standard service lines will be installed for air, water and dewatering. Dewatering will be achieved utilizing submersible pumps, staged as the ramp progresses with all pump water reporting to the settling pond. A blasting line and leaky feeder communications line will be advanced as the ramp face advances. ANFO will be the main explosive with stick powder as necessary.

Ground support included in the current estimate includes an allowance for galvanized screening of the drift from shoulder to the shoulder. Shotcrete and additional support would be installed as required or necessitated by ground conditions but has not been included in the estimate. An allowance has been included for spot bolting for the majority of the development work.

16.4.4.2. MAIN RAMP DECLINE

The main decline will be driven at a maximum grade of 15% to permit suitable trucking performance. The main ramp services will comprise of compressed air, water and dewatering. An average advance rate of 4.5 meters per day has been assumed in the estimate. It would be expected that the advance rate will be slower for the first 100-200 meters and then will increase as the learning curve is completed. All re-mucks, magazines, safety bays, sumps, backslashes for truck loading will be excavated and supported as they are encountered.

The main ramp will be developed to sump and once the upper level access drifts have been developed 15 meters, a double face situation will be available. For scheduling purposes the decline has been maintained as the priority heading at 4.5 meters per day and the upper level has been scheduled at 1.0 meters per day for a combined double face development rate of 5.5 meters per day.

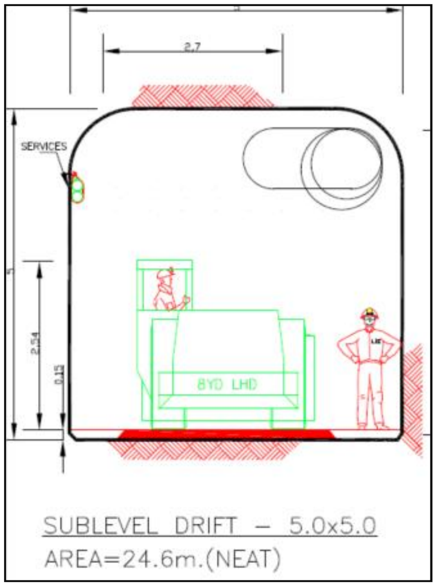

FIGURE 16-7 TYPICAL DRIFT

16.4.4.3. LEVEL DRIVE

The upper level drive will be driven at a rate of 1.0 meters per day. The upper level drift will include air, water for the extent of the full drift and a dewatering line will be carried to the grade change point located at the main sump level. The upper level drive and ramp will progress simultaneously.

16.4.4.4. ORE DEVELOPMENT/BULK SAMPLES

The ore will be broken and transported to surface using contractor's development equipment. Ore will be stockpiled on a separate ore pad located near the portal entrance. Gowest has not yet made a decision on whether to proceed with an initial bulk sample campaign and the size of this campaign should it be performed.

16.4.5. VENTILATION RAISES

16.4.5.1. EXCAVATIONS

The ventilation raise will be excavated, supported and the manway installed utilizing a double drive air raise climber. It is assumed that the raise will be advanced at a rate 2.0 meters per day in the current estimate. Ground support while the raise is being driven will consist of 6 ft grouted rebar in the walls of the raise with screen pinned to the face of the raise with 5 ft rock bolts prior to the drilling of each round. The final rounds coming through to surface and near the previously excavated raises/fan installations at the upper and mid-level accesses will be systematically broken into the access drifts utilizing controlled blasting techniques.

16.4.5.2. MANWAY INSTALLATIONS

An allowance has been included for fabrication and installation of the three legs of manway. Upon completion of the manway installation, the raise climber will be torn down, stored and the crew demobilized until the next raise access is ready. Contractor will install air line, water and dewatering lines along with electrical services and leaky feeder system in the manway.

Allowance has also been made at the surface breakthrough area for:

- A small rock cut with ground support.
- Leveling and filling of an area with non-acid generating mine muck sufficient for the heater installation and propane tank set up.
- Concrete slab as a base for heater installation.
- Fabrication and installation and concreting in place an insert to support and seal the collar area as well as transition ventilation pieces.
- Power services to be run to the collar area to service the heaters.

16.4.6. VENTILATION

16.4.6.1. GENERAL

The following ventilation requirements were estimated for the Frankfield East project. The estimates are calculated to comply with regulatory requirements based on diesel equipment dilution and required minimum air flows. In additional to the minimum requirements the ventilation system was assessed for clearing of explosive gases and optimized for costs associated with winter heating requirements. On completion of the development phases, primary flow and auxiliary ventilation will remain to ventilate the underground accesses for the diamond drills remaining in operation underground.

16.4.6.2. AIRFLOW REQUIREMENTS

The flow requirements were estimated for each phase of the project to determine installed fan requirements. The ventilation estimates used 54” ducting to calculate the pressure and flow requirements and determined that two (2) 54” twin 200 Hp fans for ventilating the main development were required. Selection of these fans will provide coverage for each phase of the work however variable vane inlets will be used to optimize the flows and power draw across the life of the project. Ventilation consumables have been included in the cost per meter of development including ventilation bag, messenger cable, clips, tensioning tools and repair kits.

The initial set of fans will be setup in the Box-cut portal area to provide airflow until the completion of the first raise to surface. On completion on the first raise, booster wallswill be constructed at the bottom of the raise and then twin 200Hp fans will be installed in the booster walls. One set will ventilate the continuation of the decline and the second, the development of the upper level. The fans will draw fresh air from surface and exhaust up the ramp. On completion of each additional fresh air leg the booster fans for the ramp will be moved into each new booster wall to provide airflow to the development face.

Additional fans will be required to provide ventilation to exploration drift development and the diamond drills once completed. In addition to exploration drives, allowances for booster fans have been made for the lowest level development.

16.4.6.3. MINE HEATING REQUIREMENTS

Mine air heating requirements were estimated based on the average monthly air temperatures for the Timmins region over the past 30 years. Based on the average temperatures and the mining schedule, air heaters will be required during the box-cut ventilated phase and once the fresh air source is from the surface vent raise collar. For each phase of the project the airflows were optimized to save on the costs of heating requirements.

16.4.7. ELECTRICAL

The contractor will supply a suitable generator plant consisting of 600V generators (including backup). The generators will feed a synchronization panel with 600V for several surface loads and a 600-4160V transformer for underground. Final power load requirements will need to be determined during subsequent mine planning activities.

As the mine portable substations (or substations) are moved further down the drifts the mine power feeder cable will be advanced. The mine portable substations will be moved in approximately 350 meter intervals and will be installed in substation cross-cuts.

16.4.8. MINE VENTILATION AIR DISCHARGE

For information purposes only, the estimated peak mine ventilation requirement is approximately 150,000 cfm or 70.8 m^3/second.

16.4.9. UNDERGROUND COMPRESSED AIR

An electric compressor "plant" will be established on surface near the shop/portal area. A receiver will be part of the set up and the air supplied underground from this location. One of the stench gas warning systems will be tied into the compressed air system. Since there is a road between the ramp portal and compressed air plant location, it will be necessary to run the compressed air pipes through a culvert located under the road. All surface lines will be heat traced and insulated.

16.4.10. MINE WATER SUPPLY

Mine service water would be taken initially from diamond drill holes with make water on the site. The water would be pumped to a mine water supply holding tank at the portal shop area and fed from there underground as required via steel piping. As with the compressed air services there is a road between the ramp portal and this area and it will be necessary to run the pipes through a buried culvert. All surface lines will be heat traced and insulated.

16.4.11. DEWATERING

Dewatering of the mine will be achieved utilizing submersible pumps. These pumps will be staged as the ramp progresses. Pumping will progress from ramp bottom through 4 inch piping with pumps located in pump boxes and sumps along the ramp length. The water will be pumped to the surface Settling Pond. As with the compressed air and water services, it will be necessary to run the dewatering pipes through a culvert buried under the road to reach the Settling Pond. All surface lines will be heat traced and insulated.

To reduce fresh water demand for underground water requirements, Contractor proposes to pull water from the polishing pond and re-use it for mine supply water.

16.4.12. WATER TREATMENT

Settling and polishing pond area contains a minimum 20,000m^3 capacity. This volume is required to allow adequate settling and to deal with any ammonia and associated sediment. All treatment and eventual discharge of the water from underground as well as permitting has been included in the Gowest owner's costs.

16.4.13. TEAR DOWN AND DEMOBILIZATION

Initial plans are for Contractor to demobilize its equipment, infrastructure and personnel as soon as practically possible to reduce costs to the project. During the final phase of the project, unnecessary personnel will be demobilized. Contractor will also demobilize any equipment not required for this diamond drill support phase. Gowest has not currently included any costs related to the purchase of equipment to remain on site. Infrastructure to be tore down and demobilized during this phase would be the site facilities unless Gowest wishes to take over and operate the site facility. The site would be cleaned up and graded to approximate pre set-up conditions. Contractor personnel required to maintain the mine surface plant and support the diamond drills would be accommodated in alternate facilities. The explosive and cap magazines will be demobilized once underground magazines are established; the site will be cleaned up and graded. Where feasible other components such as containers, diesel tanks, spare office facilities, etc will be demobilized.

Final teardown and demobilization would entail the disassembly of all facilities, shipping off site, sealing of the portal and vent raise and any required site cleanup. If required the portal and fresh air raise breakthrough would be sealed. No allowance has been made for the stripping and recovery of underground services.

16.5. MINE DEVELOPMENT SCHEDULE

A preliminary schedule was prepared for the pre-production mine development activities down to the 200 meter access level. This is included as **Error! Reference source not found.**8.

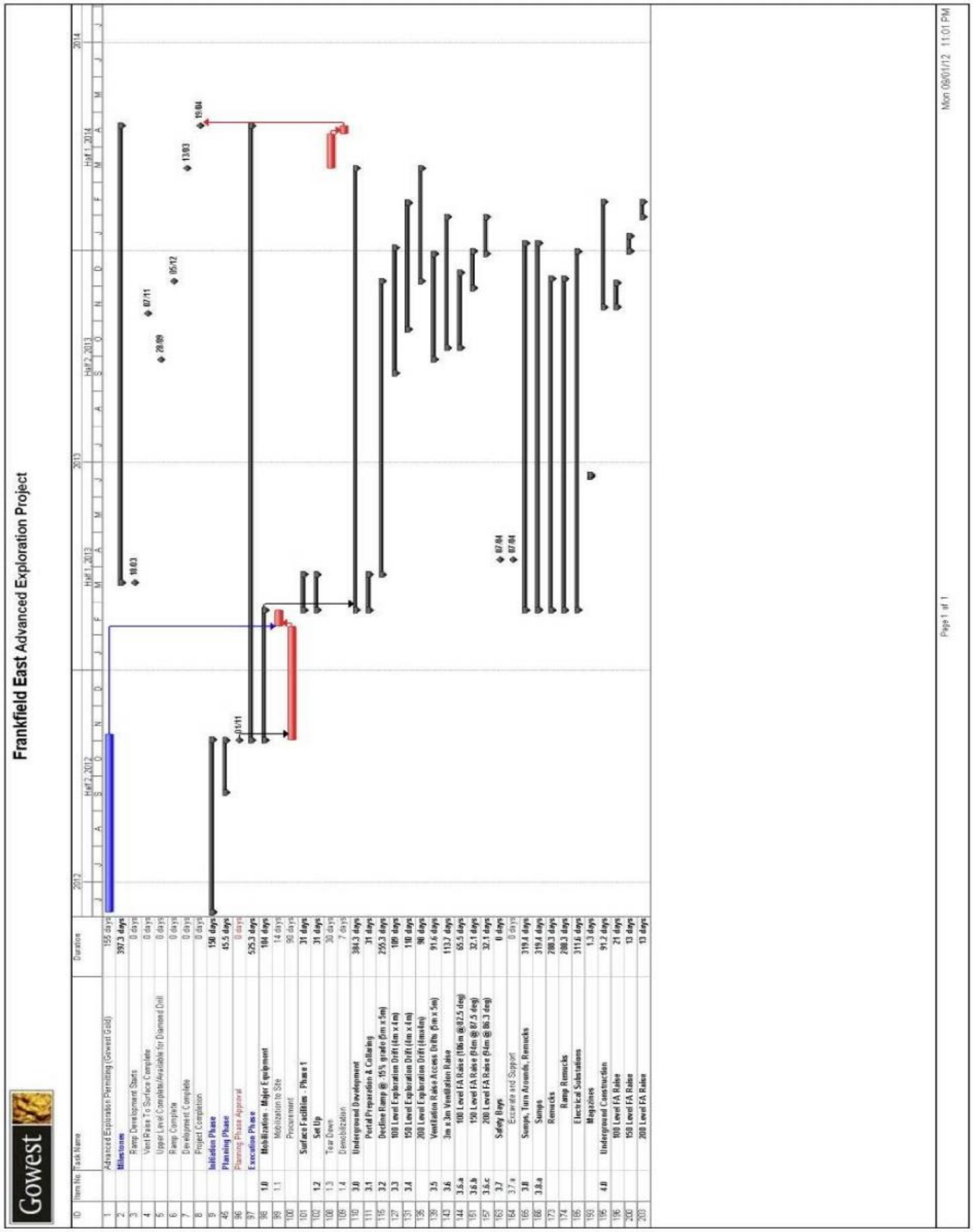

FIGURE 16-8 PRELIMINARY PRE-PRODUCTION MINE DEVELOPMENT SCHEDULE

16.6. MINE AUXILARY SHAFT

As mining depths increase towards the 400-450m level the preliminary mine plan envisions the construction of an auxiliary shaft which would allow for production rates to be maintained as the mine depth increases. Following the construction of the shaft, mined material will be transported to surface both via the ramp and shaft.

16.6.1. SHAFT

The shaft will be 4 metres in diameter and concrete-lined (300mm). It will have a conventional back leg headframe equipped with a production hoist for skipping. The maximum depth for the shaft based on the current resource is 800 metres which includes a collar, sub-collar, and a ventilation plenum entering the shaft below the sub-collar. The house includes hoist house building, electrical room and a compressor room. It is connected to shaft sub collar via a services tunnel.

The shaft diameter was selected to allow production rate of 800 to 3000 tpd from finished depth of 800 metres. The shaft will consist of two skip compartments --skip size of 1,500 mm x 1,500 mm

16.6.2. SHAFT SERVICES

The following shaft services will be installed to support ongoing production activities in the ore body.

Piping

- Compressed air line
- Dewatering lines
- Process water line
- Electrical, communications &process control
- Power cables
- Shaft communications - leaky feeder cable, shaft signals, fibre optics line, telephone

16.6.3. HEADFRAME

The headframe will be a structural steel construction with a clad/insulated exterior. Stairs inside the headframe will provide access to the various levels of the headframe. The headframe will include one sheave decks in order to facilitate the two skips sets of hoist ropes, as well as support for the shaft sinking phase.

The sub-collar will be constructed to support skip changing and ventilation air routing, and will transfer loads from the headframe to the shaft collar. The shaft collar will be equipped with full-height access doors and gates to allow for conveyance removal. In addition, jack-knife monorails will be provided for each shaft compartment to support conveyance removal operations.

The skips dump system will utilize a cylinder actuation system, with a hydraulic power pack located on the dump floor adjacent to the shaft. The dump chutes will be lined with heavy wear plates to reduce the size of the structure for rock boxes and provide sufficient space for inspection of the chutes and gates.

16.6.4. SHAFT SINKING METHODOLOGY

1) Mobilization to Site

On award of the contract, the shaft sinker will expedite the mobilization of equipment to site. The shaft sinker will provide for an office trailer and a meeting room trailer along with storage sea containers and a shop area suitable for sinking equipment repairs. A suitable lay down area will be outlined to allow delivery and storage of shaft sinking supplies and equipment.

2) Pre Sink Excavation

Shaft pilot raise will be excavated from surface to 400 m level -- this pilot hole will be used for shaft sinker to slash into. The broken material will be removed on the 400 m level -- this pilot slash methodology allows for rapid shaft sinking and reduces final cost of shaft.

After each blast, the remaining blasted collar pre-sink muck will be blown from the bench down the pilot hole. If this becomes an issue, a Cryderman Clam will be mounted on the wall. The muck going down the pilot hole will be mucked on the 400 m level as required. During this time, all blasts will be carefully timed with electronic detonators. Five metre high shaft concrete forms will be installed to form the first shaft lining pour. Once the pour is complete, the process of benching, bolting, screening and lowering the lining will continue to a depth of 40 metres allowing for Galloway and equipping deck installation.

3) Galloway Installation

The Galloway will be fabricated using modular systems. These modules will be assembled in the lay-down area prior to being installed in the pre-sink collar area. Initially, beams and cribbing will be lowered to the pre-sink bench to form a floor. The entire Galloway structure will be assembled bottom up.

When the top deck of the Galloway is completed, a second beam structure will provide a work area to assemble the equipping deck. The Galloway and equipping deck will be roped up and suspended. Remaining equipment will be installed into the Galloway. The Galloway will then be commissioned and sinking will begin. As the shaft is advanced, the remaining items to be installed on the equipping deck will be completed.

4) Slashing to 800 Level

With the Galloway roped up and suspended, the raise cover will be placed over the 2.4 metre raise bore hole. The raise cover will be outfitted with holes to allow the jumbo steel to drill through where required. During blasting and mucking, the raise cover is pulled up under the Galloway. Drilling the bench will be performed by the two nested hydraulic jumbos and will be carried out in 5 metre benches. Finished concrete lining of 600 mm will be poured using a concrete form 5 m in height. A temporary fan and mine air heater will be installed to provide fresh air from surface to the working face.

A second pilot raise bore will be excavated from the 400 level to 800 m level. This will allow the shaft sinking to continue to 800 level utilizing the pilot and slash method. The concrete lining will continue to be advanced in 5 metre lengths as described in Phase 1 with the average expected liner thickness of 0.6 metre. The steel furnishings will continue to follow the sinking as the shaft is advanced. Once shaft sinking is completed, shaft contractor would install loading pocket, surface dump and final shaft bin on surface.

The shaft will be used for fresh air ventilation and to hoist ore and waste material from depth.

16.7. MINE DILUTION

Additional detailed mine planning studies are required to fully evaluate the effects of the selected mining methods on overall mine dilution rates at the Frankfield East Deposit. For the purposes of the current study the following dilution rates have been assumed:

Narrow Structures (Shrinkage/Cut and Fill)	-	10% dilution
Bulk Mining (Long-hole)	-	20-25% dilution

Based on preliminary mine plans the total tonnes of mined material attributed to bulk mining areas is estimated at 50-65% leaving the remaining 35-50% coming from narrow structure areas. Overall this results in an expected LOM dilution rate of approximately 15% for the mined resource material from the Frankfield East deposit. It is expected based on the distribution of the gold within the deposit that this dilution material would contain between 0.5 and 1 g/t of gold.

16.8. MINE SITE SERVICES (LIFE-OF-MINE)

It has been assumed that all of the mine predevelopment work will be completed by a suitable mine contractor. During this predevelopment period services such as power/water/sewage will be provided by the contractor in the form of generators, portable offices and dry, etc.

Following the completion of the predevelopment activities it is assumed that power for normal mine production activities will be provided from the nearby grid via the installation of new power lines, transformers, substations, etc. Allowances have been made in the current capital costs estimates for the installation of other long term infrastructure/services including:

- Fuel storage and dispensing;
- Backup emergency power generators;
- Permanent water/sewage services;
- Permanent truck shop facilities;

17. RECOVERY METHODS

17.1. GENERAL

This chapter is taken from the report of Ling and Trinder, (2012).

17.2. UNDERGROUND MINE

The underground mine at Frankfield East will be accessed initially using a ramp with a combination of bulk mining (open stope) and narrow vein (shrinkage/cut and fill) techniques. Underground development plans have not been finalized but a conceptual mine development/production scenario for the project was detailed previously in Section 16. The mined rock from the Frankfield East underground operations will be brought to the surface and delivered to a ROM stockpile for further handling at the mine site.

17.3. CRUSHING AND SCREENING

A portable crushing and screening plant with daily production of approximately 1500 tonnes is considered to be operated at the mine site via an independent contractor. Crushing operations are currently envisioned as a two stage circuit (primary jaw and secondary cone). The portable equipment (including transfer belt conveyors) is independently powered via diesel powered drives.

ROM ore is loaded from the mine site stockpile and processed to produce a final crushed product of minus 25 mm material. The crushed material is then transported by truck to the crushed ore processing facility for gold recovery operations. The ROM ore stockpile at the mine site is sufficient to allow for normal crushing operation shutdown periods and short term production interruptions.

17.4. PROCESSING PLANT

The current study for the Frankfield East deposit includes the construction of a new mill and processing plant. A flowsheet for the processing plant utilized in the study base case is depicted in Figure 17-1. It is assumed that the process plant will operate on a 24 hour per day basis with an overall availability of 95%.

The plant design incorporates the following general stages:

- Comminution (grinding and regrinding)
- Flotation for gold concentrate production
- Pressure oxidation
- Cyanidation for gold recovery
- Gold refinery
- Tailings and cyanide destruction

It is important to note that the pressure oxidation and cyanidation stages will process only the flotation concentrate which represents approximately 12% of the initial mill feed rate.

17.4.1. COMMINUTION

The plant receives crushed ore which will be stored at the plant site in crushed ore storage bins. The grinding circuit consists of a primary rod mill and ball mill circuit. Ore is ground to a size of approximately 80% passing 75 microns prior to being sent to the flotation circuit.

A regrind mill circuit has been included to reduce the rougher flotation concentrate particle size to approximately 25 microns (d_{80}) in order to improve the sulphide cleaning efficiency.

17.4.2. FLOTATION

The flotation circuit consists of rougher and cleaner stages for separating the arsenopyrite and pyrite concentrates. The flotation circuit shown in Figure 17-1 represents the bench scale Locked Cycle Test (LCT) flowsheet used in the metallurgical program (see Section 13). The rougher flotation is completed with a feed particle size of 75 microns (d_{80}). The arsenopyrite rougher concentrate is then reground to 25 microns (d_{80}) for final cleaning operations. The rougher tailings are fed to pyrite flotation stage for pyrite recovery.

The sequential flotation circuit generates two concentrate products:

- arsenopyrite concentrate (7% mass recovery / 93% gold recovery)
- pyrite concentrate (5% mass recovery / 3% gold recovery)

Tailings from both arsenopyrite and pyrite cleaning circuits are combined and fed to the last stage of flotation, sulphide scavenger to recover residue sulphides prior to disposal.

The use of a sequential flotation circuit provides the most flexibility with respect to potential changes in the mineralogy within the Frankfield East deposit as well future opportunities to custom treat materials from other deposits. In the current study the two flotation concentrates are combined to produce a single sulphide concentrate feed for pressure oxidation. This combined concentrate represents an overall mass recovery of approximately 12% of the mill production rate (180 tonnes per day) and along with a gold recovery of 96-97%.

17.4.3. PRESSURE OXIDATION

The gold-bearing sulphide concentrate is transferred to a pressure oxidation (POX) facility adjacent to the milling circuit. The slurry is pumped into a continuously operating autoclave. Once in the autoclave, the slurry is subjected to high temperature (+200^oC) and injected with high pressure oxygen from an oxygen plant. After approximately 60 minutes, approximate 98-99% of the original arsenopyrite and pyrite components in the concentrate is dissolved to free the contained gold. The majority of the iron and arsenic is solubilized first and then precipitates under pressure forming scorodite($FeAsO_4 \cdot 2H_2O$), a chemically stable form of arsenic.

The oxidized slurry from the autoclave is discharged, cooled and thickened separating solids from the acidic solution. A portion of the acidic filtrate from the thickener is recycled to the autoclave feed tank to help condition the new concentrate and remove carbonates. The balance of the thickener overflow is neutralized with limestone and lime prior to being pumped to tailings area. The thickened gold bearing

POX residue is neutralised to a desired pH level suitable for cyanidation and then pumped to a cyanidation circuit for gold recovery. Options to filter the thickened slurry prior to neutralisation and cyanidation are being investigated.

17.4.4. CYANIDATION

Neutralized POX residue is pumped to a conventional CIL (Carbon-in-Leach) circuit where leaching and adsorption of gold are carried out simultaneously. Cyanide required for leaching gold is added to the circuit, while milk of lime is added to maintain slurry at the desired pH level. Activated carbon is added to the last tank and advances via carbon advance pumps counter-currently to the slurry. As the gold is leached, it is adsorbed by the carbon. Air is sparged from the bottom of each tank into slurry to maintain adequate dissolved oxygen levels in the pulp.

Carbon pregnant with gold from the first CIL tank is pumped to a loaded carbon screen where the loaded carbon is separated from the slurry. The slurry falls by gravity back to the 1st CIL tank. The loaded carbon is transferred to a bin from where the loaded carbon is transferred to a stripping stage.

Tailings from the last CIL tank overflows to a carbon safety screen which prevents the loaded carbon from lost. The screen undersize flows by gravity to a pump box, and is then pumped to the tailings dewatering area.

Cyanidation of the POX residue results in high gold extractions over 98%. Loaded carbon is processed via a pressure stripping and gold refining plant. The expected overall recovery of gold from the ore is approximately 95%.

17.4.5. TAILINGS AND CYANIDE DESTRUCTION

Following cyanidation, residual cyanide contained in the leached slurry is destroyed via a SO_2/air cyanide destruction circuit. Cyanide destruction discharge is then thickened along with the flotation tailings. The combined tailings are sent to a conventional tailings containment area for impoundment. Water is recycled from the tailings impoundment area for reuse in the process plant.

Options for impoundment of the neutralized autoclave discharge filtrate are currently being evaluated. Alternatives included disposal in the general flotation/cyanidation tailings area or in a separate designated area.

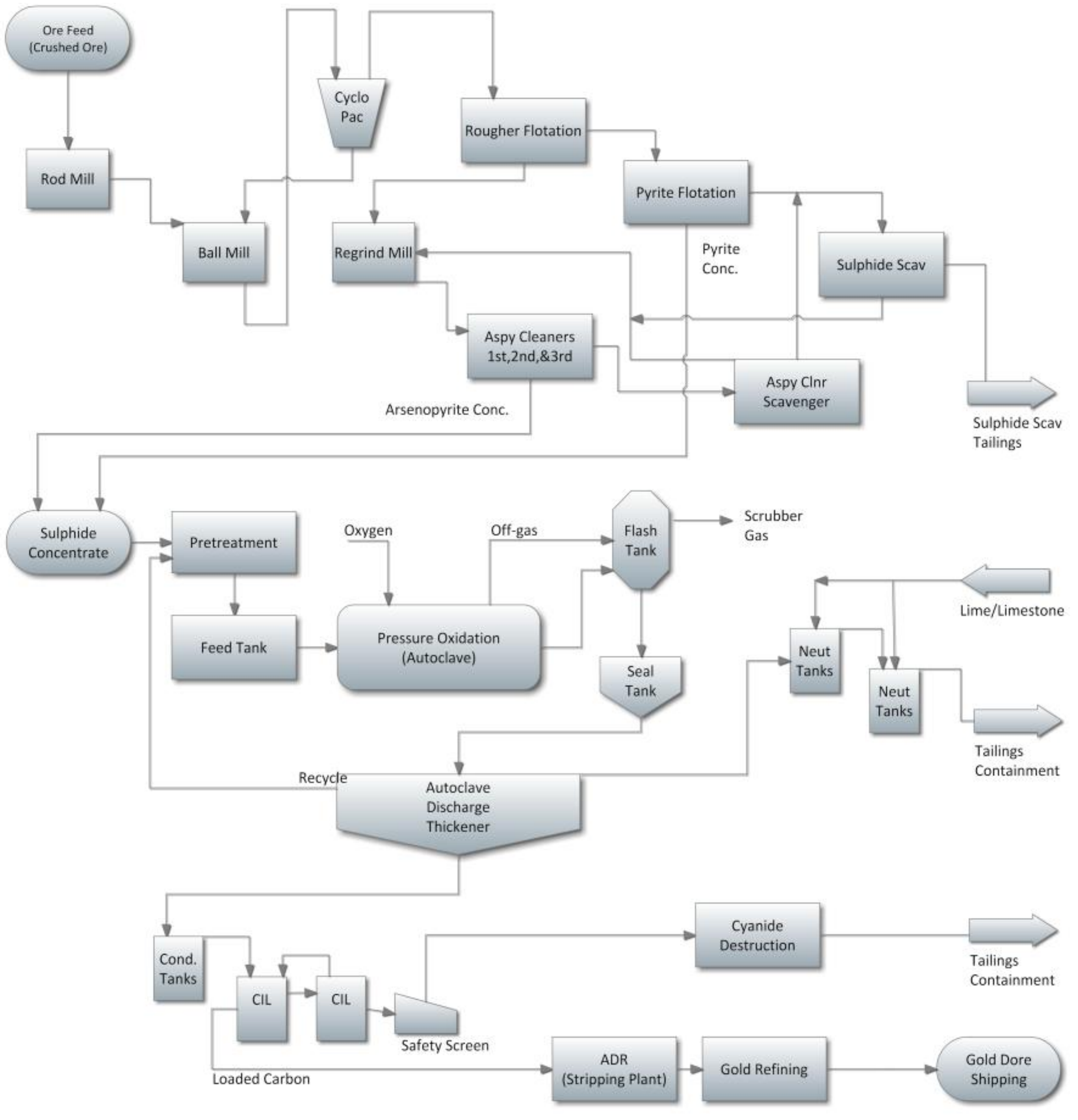

FIGURE 17-1 MILL FLOWSHEET

18. PROJECT INFRASTRUCTURE

Given its exploration stage of development there is very limited infrastructure currently available at the Project site.

All-weather gravel road access is currently available to the Texmont deposit in the northwestern part of the Project. The final 500 metres of this road is currently inaccessible to road vehicles due to a wash-out. Access to the Frankfield East deposit could be achieved by constructing approximately 1.0-1.5 km of new gravel road to connect with the existing gravel road.

115 kV and 500 kV electric transmission lines paralleling Highway 655 are located approximately 10 km and 13.5 km west of the property respectively. The West Buskegau River, located 1.6km east of the Frankfield East deposit offers an abundant source of process water. Large quantities of aggregate resources are located adjacent to Highway 655, approximately 15 km west of the property.

Gowest maintains a secure and well equipped, combined field office / core logging-sampling facility at 115 Jubilee Avenue East, Timmins.

The City of Timmins is the nearest source of mining related commercial services and an abundant pool of managerial and skilled labour. Timmins is serviced by modern telecommunications, commercial airlines, rail service and truck transportation.

Gowest holds sufficient surface rights necessary for potential future mining operations including tailings storage areas, waste disposal areas and a processing plant.

19. MARKET STUDIES AND CONTRACTS

19.1. MARKETS

Gold prices have steadily increased over the last number of years to in excess of USD 1500/oz at the present time and gold market forecasts in the industry have generally remained bullish. Traditionally two year historical price averages were often taken as the basis for economic analyses. This average value is currently at approximately USD 1350/oz. As part of a more conservative approach, a long term gold price of USD 1200/oz was used in the current analysis. This level is consistent with the current industry long term predictions.

An exchange rate of USD1.00 / CAD was utilized where currency conversions were required.

19.2. CONTRACTS

Gowest currently has no contracts in place for the development of the Frankfield East deposit.

While preparing the economic analysis, non-binding "budget" quotations were received for a number of key cost items including:

- Transportation of ore from the mine and sand for backfill
- Supply of limestone and lime
- Contract crushing
- Oxygen production
- "Typical" mine contractor rates

The remainder of the operations related to concentrating, oxidation, gold recovery and refining would be done directly by Gowest personnel.

20. ENVIRONMENTAL STUDIES, PERMITTING AND SOCIAL OR COMMUNITY IMPACT

Gowest retained Golder Associates in 2010 to conduct environmental baseline studies on the Frankfield Gold Project. Data acquisition is ongoing; results will be presented at the completion of the baseline study period. A summary of environmental baseline activities completed to date and planned future activities follows are presented in this section.

20.1. GEOCHEMISTRY

Regulation 240/00 of the Ontario Mining Act requires that materials that will be encountered at proposed mining projects undergo geochemical characterization. A staged approach to geochemical characterization was adopted, with Phase I including screening level geochemical characterization of waste rock, ore and tailings, and Phase II including kinetic tests.

The screening level analytical program included only static (i.e., one-time) tests. Static tests are typically used to quantify the solid phase chemical composition of samples, and evaluate metal leachability in specific test conditions. The screening level evaluation included the following tests:

- Acid-Base Accounting (ABA);
- Major and trace element analysis on rock samples;
- Net Acid Generation (NAG) testing and comprehensive analysis of NAG leachates and;
- Short-term leach testing

After the evaluation of the results of static testing, samples are selected for longer-term leach tests (i.e., kinetic tests) which are repetitive leach tests designed to evaluate mineral reactivity over an extended period of time. The test methodology is designed to enhance sulphide oxidation and/or weathering reactions relative to field conditions. Kinetic tests can be used to develop meaningful information with respect to leachate water quality in a relatively short period of time, as compared to actual field conditions, where it may take years to centuries for long-term weathering rates to develop.

20.1.1. COMPLETED ACTIVITIES

- Tailings characterization - Static and kinetic analyses of tailings sample were completed in June 2011.
- Waste rock characterization - Sample collection took place in February 2011. Static testing of a sub-set of 40 samples has been completed. Kinetic testing on seven waste rock samples commenced in August 2011.

20.1.2. PLANNED ACTIVITIES

- Tailings characterization - No further tailings characterization work has been proposed as of the time of this report.
- Waste rock characterization - Two of the seven waste rock samples reached a steady state after 20 weeks of kinetic testing, and were terminated. The remaining five samples were maintained for an additional 10 weeks of kinetic testing, or until a steady state is reached. Further static testing will be conducted upon finalization of the mine plan.

20.2. WATER QUALITY

Baseline surface and groundwater quality samples are being collected in order to establish the background water quality conditions of the Project site prior to development. Generally, surface water quality samples are collected from stations established upstream and downstream of the proposed Project footprint. Groundwater quality samples are collected from monitoring wells installed in boreholes located in overburden and shallow bedrock within the project footprint. Due to seasonal variability, baseline water quality monitoring is being completed throughout the year (i.e. spring freshet, low flow summer, ice-covered low flow in winter) and over a period of several years in order to determine annual trends. The sampling program is currently in its second year.

The water quality field campaigns were conducted in concert with the hydrology component in order to maximize the utility of the data collected at each station. Surface water quality samples were collected from six stations. Groundwater quality samples were collected from monitoring wells at five borehole locations drilled as part of the hydrogeology program in 2010, three of which were installed with nested monitoring wells.

During each field campaign, samples were submitted for the following analyses:

- Physical parameters - pH, alkalinity, conductivity, dissolved oxygen, total dissolved solids and total suspended solids;
- Major ions – calcium, magnesium, potassium, sodium, sulphate, chloride, fluoride and cyanide (free);
- Nutrients – nitrate, nitrite, ammonia;
- Organics – oil and grease, phenols;
- Microorganisms – E coli and total coliform; and
- Metals – total and dissolved.

20.2.1. COMPLETED ACTIVITIES

Surface water quality sampling was conducted in:

- September 2010: low flow conditions;
- February 2011: low flow conditions, minimum temperature;
- May 2011: spring freshet;
- August 2011: low flow conditions, maximum temperature; and
- September 2011:low flow conditions.

20.2.2. PLANNED ACTIVITIES

Water quality monitoring is expected to continue in February, May and August, 2012.

20.3. HYDROLOGY

Four stream flow monitoring stations were established on the main water courses potentially affected by the Project. These locations are collocated with surface water quality monitoring locations. Level loggers were installed with discrete flow measurements used to establish elevation-flow relationships over subsequent field visits. Stream flow measurements were collected at all monitoring stations during each field visit to provide at least three points on the level-flow rating curve. The rating curves establish a relationship between water level and flow in the river, which can then be used to translate the recorded water levels into flows.

20.3.1. COMPLETED ACTIVITIES

September 2010, and February, May and September 2011 field campaigns have been completed. Data from September 2010 to May 2011 at two stations could not be downloaded in May 2011 because the data loggers were damaged and rendered inoperable during the winter. New loggers were installed at these two locations in May 2011, and data was downloaded during the September 2011 field event.

20.3.2. PLANNED ACTIVITIES

No further hydrology field campaigns have been proposed as of the time of this report.

20.4. HYDROGEOLOGY

The baseline hydrogeological investigation was designed to establish a monitoring well network for the purpose of obtaining baseline groundwater quality, groundwater elevation and hydraulic conductivity data at the site.

The hydrogeological investigation consisted of the following components:

- borehole drilling and installation of groundwater monitoring wells;
- development of groundwater monitoring wells; and
- hydraulic conductivity testing.

Five boreholes with groundwater monitoring well nests were installed to characterize the overburden (when present) and shallow bedrock groundwater quality in the vicinity of potential groundwater contaminant sources.

20.4.1. COMPLETED ACTIVITIES

Borehole drilling, and installation and development of baseline monitoring wells was completed in June 2010.

20.4.2. PLANNED ACTIVITIES

Packer testing will be completed in conjunction with exploration drilling to determine the hydraulic conductivity of bedrock adjacent to the deposit. These hydraulic properties will be used to develop a hydrogeological model for the site and estimates of groundwater inflow.

20.5. TERRESTRIAL ECOLOGY

20.5.1. TERRESTRIAL PLANT COMMUNITY SURVEY

Plant community mapping was conducted in the summer of 2010 (late July to early August) when both late summer and fall flowering plants are visible.

20.5.2. BREEDING BIRD POINT COUNTS

Breeding bird surveys were conducted in late May to early June 2011 to inventory breeding birds in the area defined by the mineral concession boundary.

20.6. AQUATIC ECOLOGY

A cursory fish community and fish habitat survey was conducted in late June 2011, focused on selected portions of the Buskegau River and the West Buskegau River. Survey locations in each system were targeted to collect representative information upstream, within and downstream of the Project area.

21. CAPITAL AND OPERATING COSTS

21.1. BASE CASE ASSUMPTIONS

Capital and operating cost estimates were prepared for the PEA Base Case scenario assuming a greenfields installation of mining and processing facilities. Costs are considered to be accurate within a range of ±30%. Key assumptions utilized during the estimating process were as follows:

- 1500 tonnes per day mining and milling operations
- Approx. 95% mill availability for a total annual capacity of 525,000 tonnes of mill feed
- Overall gold recovery of 95% resulting in annual production rate of 95,000 oz.
- Life-of-mine (LOM) average estimated grade of the resource is used for all production years (prior to dilution).
- Overall mineable recovery of 85% of the current resource (indicated+inferred) during LOM operations (10 year mine life).
- Milling facilities to be constructed at a suitable site within close proximity of the mine site

21.2. COST ESTIMATE METHODOLOGY

The general methodology utilized for the development of the PEA study operating and capital costs estimates was as follows:

- A complete metallurgical processing model was completed using Metsim® software with testwork data obtained primarily from SGS Canada and experience from similar previous projects.
- Mass and energy flows were taken directly from the process model and then utilized to identify and size all major process equipment items.
- Capital costs were estimated for individual equipment then factors applied to account for additional requirements such as foundations, piping, electrical, buildings and engineering (EPCM).
- A conservative 30% contingency was added to all process plant capital cost estimates to account for items that were not specifically identified at this stage of the study.
- Conceptual capital costs were prepared in conjunction with Golder Associates for tailings containment facilities.
- Infrastructure and owner's costs were developed based on a conceptual plant site location within 15-20 km of the mine site. Infrastructure requirements included road upgrades, power lines, site preparations and facilities such as a truck shop, drying area, laboratory and administration building. Owner's costs include permitting requirements, insurance, first fill of consumables, temporary construction requirements, land acquisition and a pre-production drilling program. Excluded from owner's costs are corporate overheads and working capital requirements.
- Operating costs were developed based on estimated staffing levels, consumables (from testwork and modeling) and expenditures required to support the mine and its associated processing, maintenance and administrative activities. Power requirements were calculated based on estimated equipment motor sizes and assuming a conservative delivered charge of $0.07 /kWh

which is at the conservative end of the range for current costs at similar operations in Northern Ontario.

- Additional operating cost allowances were included for outside contractors, laboratory consumables, vehicle fuel requirements, etc.
- Included in the mine operating costs were the estimated average contractor rates, costs for the Company mine services group and an allowance for backfilling and annual ongoing development drilling. Contractor rates were assumed to include ongoing production development.
- Utilizing 3D models of the interpreted parallel mineralized zones, a conceptual mine plan was prepared. The mining plan envisions a combination of long-hole bulk mining techniques for wider zones of mineralization and shrinkage mining for narrower zones. Initial estimates for the ratio of bulk mined material to shrinkage material range from 1/1 to 2/1. A pre-development schedule and cost estimate was created down to the 200m level using ramp access. Ramp access would be utilized exclusively down to approximately the 400m level after which a small shaft would be developed to allow for the maintaining of LOM production levels as the mine development continued to greater depths. The construction of this shaft is assumed to take place starting in year four of production and would consist of a combination of raise boring to surface and slashing down to depth.

21.3. CAPITAL COSTS– BASE CASE

The capital cost estimate was divided into “Pre-production” capital and production “Sustaining” capital.

Pre-production capital includes all mine and process costs up to the initiation of commercial mining operations (75% of steady state production). Total pre-production costs at Frankfield East are estimated at $167M. Sustaining capital costs over the life of mine are estimated at $86M for a total project capital cost of $253M. A breakdown of the project capital costs is summarized in Table 21-1.

TABLE 21-1 BASE CASE CAPITAL COSTS (GREENFIELDS PLANT) - $M

Area	Pre-Production Capital Costs	Sustaining Capital Costs	Total Capital Costs
Mine			
Mine predevelopment	21		21
Mine site	12[*1]		12
Mine expansion (shaft)		50 (year 4-5)	50
Process Plant/ Infrastructure			
Processing Plant	96		96
NSR Purchase	3.5[*2]		3.5
Infrastucture	12		12
Tailings	10	5 (year 4)	15

Mine Closure (less $4 million salvage value)		11	11
Owner cost	12		12
Sustaining Capital (LOM)		20	20
Total Capital	**167**	**86**	**253**

Notes:

1. Cost includes predevelopment mine costs plus installation of mine site permanent substation and truck shop.
2. Buyout of NSR royalty related to Texmont land acquisition.

The pre-production capital cost estimate of $167 million includes the construction of a new stand-alone process facility, mine development down to the 200m level, Phase 1 of the tailings storage facilities and all necessary site infrastructure to bring the mine into production. A conservative 30% contingency has been included in the process facility estimate to account for requirements that are not detailed in the current study.

The largest single component of the sustaining capital estimate of $86 million is the construction of a mine shaft starting in year four (4) of production. Other items included in this figure are the Phase 2 expansion of the tailings impoundment facilities and ongoing annual sustaining capital requirements. To reduce capital requirements, the company will utilize contractors for both mining and mine-site crushing activities. Subsequent to the initial mine pre-development activities, all additional mine development is treated as operational development and included in the contractor mining rates (with the exception of the mine shaft installation).

21.3.1. MINE PREDEVELOPMENT

A preliminary mine predevelopment plan was prepared to access available mine stopes down to the 200 meter level via a ramp. Details of this plan are presented in Section 16 of this report. A breakdown of the $21 M in capital costs associated with this predevelopment work is included in Table 21-2.

TABLE 21-2 MINE PREDEVELOPMENT COSTS TO 200M LEVEL

Schedule of Prices - Revision 1					
Item No.	Description	QTY	UNIT	UNIT PRICE ($)	TOTAL PRICE ($)
1.0	**MOBILIZATION MAJOR EQUIPMENT**				
1.1	Mobilization to Site	1	LS	$1,634,190.60	$1,634,190.60
1.2	Contractors Set-Up	1	LS	$1,574,371.72	$1,574,371.72
1.3	Teardown	1	LS	$122,269.80	$122,269.80
1.4	Demobilization	1	LS	$292,637.84	$292,637.84
	Total Item 1.0 MOBILIZATION				**$3,623,469.96**
2.0	**SITE SET UP AND OPERATION**				
2.1a	Cost per month surface facilities - Phase 1	1.0	Month	$30,416.36	$30,999.69
2.1b	Cost per month surface facilities - Phase 2	3.7	Month	$22,997.13	$85,435.91
2.1c	Cost per month surface facilities - Phase 3	4.6	Month	$42,816.93	$195,667.52
2.1d	Cost per month surface facilities - Phase 4	3.3	Month	$54,273.37	$180,217.33
2.2	Cost per month surface equipment	13	Month	$28,721.24	$362,595.84
	Total Item 2.0 SITE SET UP AND OPERATION				**$854,916.29**
3.0	**UNDERGROUND DEVELOPMENT**				
3.1	Portal preparation and collaring	2,500	m3	$87.69	$219,228.49
3.2	Decline ramp @ -15% grade (5m x 5m)	1,264	m	$4,020.00	$5,081,280.00
3.3	100 Level (4m x 4m)	246	m	$3,440.00	$846,240.00
3.4	150 Level (4m x 4m)	250	m	$3,440.00	$860,000.00
3.5	200 Level (4m x 4m)	250	m	$3,440.00	$860,000.00
3.6a	3m x 3m Ventilation Raise @ 70 degrees - Setup/Teardown	1	Ea	$30,369.18	$30,369.18
3.6b	3m x 3m Ventilation Raise @ 70 degrees - Excavate & Support	200	m	$3,092.51	$618,502.78
3.7	Safety bays	42	Ea	$1,120.00	$47,040.00
3.8	Sumps, turn arounds, substations	125	m	$3,440.00	$430,000.00
3.9	Miscellaneous slashing	3,540	m3	$86.98	$307,907.70
	Total Item 3.0 UNDERGROUND DEVELOPMENT	**2,010**			**$9,300,568.16**
4.0	**INDIRECTS**				
4.1	Cost per day for indirects - Phase 1	31	Day	$12,892.20	$399,658.20
4.2	Cost per day for indirects - Phase 2	113	Day	$16,379.71	$1,850,907.23
4.3	Cost per day for indirects - Phase 3	139	Day	$20,145.37	$2,800,206.43
4.4	Cost per day for indirects - Phase 4	101	Day	$20,145.37	$2,034,682.37
	Total Item 4.0 INDIRECTS				**$7,085,454.23**
	TOTAL	384			$20,864,408.64

21.3.2. MINE SITE

An estimate of $8M was included to cover pre-production mine site development activities. Included in this cost are the following:

- 15km of power line installation from main line to mine site
- Power controls
- Water/sewage utilities
- Waste rock and site run-off ponds
- 2km of new mine roads
- ROM ore stockpile pad
- Diesel storage
- Emergency power backup generators

An estimate of $4M was included to cover additional mine site costs following the completion of the mine access ramp (via contractor). This covered the installation of a permanent power substation and construction of site truck shop/dry.

21.3.3. MINE EXPANSION

An estimate of $50M was included to cover the construction of an auxiliary shaft to maintain the production levels of material from the mine as the mine depth increases beyond the 400-450 meter level. Details of the preliminary shaft design are contained in Section 16.5. It has been assumed that the shaft will be constructed in Years 4/5 of the mine operation with the capital costs spread over those two years.

21.3.4. PROCESS PLANT

A breakdown of the overall process plant costs is shown in Table 21-3. The capital cost estimates were prepared based on the construction of a new greenfields facility within reasonable proximity to the Frankfield East mine site. It has been assumed that the site consists of relatively flat terrain with minimal site excavations required prior to the initiation of construction operations.

TABLE 21-3 FRANKFIELD EAST PROCESS PLANT CAPITAL COSTS

Description	Mechanical Cost (equipment only)	Cost Factors	Factored Cost
Grinding and Flotation	$ 8,100,000	3.59	$ 29,100,000
Pressure Oxidation (Autoclave) Plant	$ 11,900,000	2.96	$ 35,200,000
Gold Recovery Plant	$ 3,900,000	2.45	$ 9,600,000
Contingency (30%)			$ 22,100,000
Total Process Plant (includes EPCM)	**$ 23,900,000**		**$ 96,000,000**

As was described previously capital cost estimates for the processing facilities are derived from the cost of major equipment items which were sized based on a mass balance generated from a complete metallurgical process simulation model for the Frankfield East deposit. Individual cost estimating factors were then applied to each individual equipment item to accounts for related capital requirements (see description below). An overall contingency of 30% was applied to the total factored equipment costs to account for other capital items that will be required but have not yet been detailed at the level of this current study. It is believed that a contingency level of this magnitude represents a conservative approach based on the level of engineering detail completed to date.

The total cost factors which were calculated for each individual process plant area are shown in Table 21-3. These factors are applied to the mechanical equipment costs to account for capital requirements including the following:

- Installation
- Foundations and structural steel
- Piping and insulation
- Electrical and instrumentation
- Electrical distribution
- Buildings (plant only)
- EPCM

21.3.5. INFRASTRUCTURE

An estimate of $12M is included to cover pre-production infrastructure activities. Included in this cost are the following:

- 20km of power line installation from main line to plant site
- Plant site transformers/substation
- 10km of new roads to access plant site
- Construction of administrative and lab buildings
- Misc. site preparations

21.3.6. TAILINGS DISPOSAL

Golder Associates conducted a conceptual design and costs estimate for a tailings facility suitable for the Frankfield East deposit. A total capital cost of $15M is estimated for the life-of-mine. In the current study it is assumed that $10M of this total will be spent as part of the pre-production activities followed by an additional $5M tailings expansion in the fourth production year. The current estimate is not site specific and will need to be re-evaluated once a site selection has been completed.

Basic parameters utilized for the design include:

- 5 million tonnes of solids in tailings
- Site with level grade
- “Typical” flotation tailings final void ratio
- Deposition method – upstream raising from starter dike and berms constructed with imported fill on previously deposited tailings (segregated coarse fraction)

Included in the estimate are the following:

- Basic site clearing (assumed 2m of peat over glacial till)
- Dam construction
- Tailings transport (pipe/pump)
- Water reclaim (includes polishing pond)
- Closure (regarding/vegetation)
- Indirect costs and contingency

21.3.7. MINE CLOSURE

An allowance of $15M has been included for final closure costs related to the mine and processing plant. This cost was estimated based on published data from similar recent project studies in the Abitibi region. A deduction of $4M has been assigned as the final salvage value for the constructed mine facilities at the end of the mine life.

21.3.8. OWNER COSTS

Owner's cost is estimated at $12M. Included in this figure are:

- EIA activities related to plant site and tailings
- Initial fill of warehouse supplies and reagents
- Insurance
- Temporary building power and misc. supplies
- Construction communications and security
- Land acquisition costs
- Predevelopment definition drilling

21.3.9. ONGOING SUSTAINING CAPITAL

An annual allowance of 1% of the LOM project capital costs has been made to account for ongoing sustaining capital requirements. It is assumed that this capital requirement will not be required until the start of Year 2 of operations.

21.3.10. EXCLUSIONS

No allowances have been made in the current capital cost estimates for the following:

- Working capital
- Gowest corporate costs
- Additional preconstruction civil works beyond basic requirements assuming relatively level terrain with soils suitable for the proposed construction activities.
- Taxes
- Bonding
- Inflation

21.4. OPERATING COSTS– BASE CASE

The total unit operating costs for the project are estimated at $119 /tonne of ore resulting in a net cash production cost of $660 /oz of gold (including corporate G&A). It should be noted that the decision to utilize contractors for mining and crushing has added somewhat to this cost. Should the deposit resource continue to grow it may make sense in future evaluations to perform these activities in-house. Of the total $39 /tonne in processing costs, approximately $17 /tonne are related to the additional sulphide oxidation stage, which is required to effectively process the Frankfield East mineralization. This equals to a processing cost of $90-100 /oz of recovered gold beyond that which would be expected from more "conventional" non-refractory gold deposits.

The life-of-mine operating costs are summarized in Table . Details of these costs are discussed later in this section.

TABLE 21-4 OPERATING COST SUMMARY

Description	$/tonne ore
Total Underground Mining Costs	68.80
Crushing and Haulage	7.00
Processing/Refining	38.82
G&A	4.28
Total	**118.90**

21.4.1. MINING COSTS

Operating costs assume contract mining at site. A detailed breakdown of the total LOM average mining costs is summarized in Table 21-5.

TABLE 21-5 MINE OPERATING COSTS

Description	
Ore production	525,000 tonnes/ year
Average Contractor Mining Cost (incl. production development)	$60.00/t
Backfill / Misc. Mine Services	$3.00/t
Ongoing Definition Drilling	$2.50/t
Gowest Mine Services Personnel	$3.30/t
Total Underground Mining Costs	$68.80/t

Conceptual mining plans have indicated approximately 2/3 of the total mine production tonnes will come via long hole methods with the remainder utilizing shrinkage (and/or cut and fill) techniques. Based on preliminary plans and discussions with local contractors an average LOM contractor rate of $60 per tonne of ore has been utilized in the estimate. Included in this average rate are ongoing production development costs beyond the initial mine predevelopment capital costs.

There are a number of gravel/sand pits within close proximity to the Frankfield East site, which are suitable for providing backfill material. Preliminary "all-in" cost estimates for the production of backfill based on a simple conventional backfill mix plant are $6 to $8 per tonne of fill (including labour and materials). Assuming a 35%-40% fill factor for the overall mined voids this is equivalent to a LOM backfill cost of approximately $2.50 per tonne of mined ore. Additional testwork is recommended to determine what quantity of deslimed and filtered flotation tailings would be available from the Frankfield

East processing operations to serve as suitable fill material. The backhauling of this tailings material offers the opportunity to replace a portion of the sand/gravel used in the backfill mix in order to reduce overall backfill costs.

During mining operations, there will be an ongoing development exploration drilling program aimed at better defining resource blocks prior to their extraction. An allowance of $2.50 per tonne of mined ore has been included in the current figures for these ongoing activities.

A breakdown of the Gowest mine service requirements is summarized in Table 21-6. This group would be responsible for the preparation of overall mine plans and the monitoring of mine contractor activities.

TABLE 21-6 MINE SITE LABOUR COSTS

	Qty.	Base Rate	w/Benefits	Total Cost
Hourly Personnel Requirements				
- Surveyors/Geotechnicians	4	$ 25.00	$ 37.50	$ 327.600.00
- Labourers –General	4	$ 25.00	$ 27.00	$ 224,640.00
- Labourers - Security	6	$ 20.00	$ 27.00	$ 336.960.00
Salaried Personnel (Mgmt/Admin)				
- Mine Manager	1	$ 210,000.00	$ 73,500.00	$ 283,500.00
- Mine Engineers	1	$ 150,000.00	$ 52,500.00	$ 202,500.00
- Geological Engineer	1	$ 140,000.00	$ 49,000.00	$ 189,000.00
- Geologists	1	$ 130,000.00	$ 45,500.00	$ 175,500.00
Total Work Force	18			**$ 1,739,700.00**
Cost per Mined Tonne	**$3.30**			

21.4.2. SURFACE ORE CRUSHING/HAULAGE

It has been assumed that mined ore will be stockpiled and crushed at the mine site utilizing portable crushing equipment and a crushing contractor. ROM ore will be crushed to minus 18 mm in a two stage crushing circuit. Discussions with crushing equipment suppliers as well as local contractors have indicated that an overall cost of $7 per tonne of ore is a reasonable estimate for these activities. Included in this rate are:

- Supply and maintenance of all crushing equipment
- Loading of crushed ore from ROM stockpile into crushing circuit
- Loading and haulage of crushed ore to processing facility located within 15-20km of mine site.

The advantages of using portable equipment and a contractor for crushing/hauling operations include a reduction in upfront capital requirements and greater flexibility with respect to the crushing circuit design and integration between the mine and processing facilities. Should the project resources continue to grow a re-evaluation of the contractor option may be warranted by Gowest.

21.4.3. PROCESSING/REFINING COSTS

A breakdown of the overall process/refining costs is shown in Table 21-7.

TABLE 21-7 PROCESSING OPERATING COSTS

Description	Costs
Labour	
Salaried	$2.47/t
Hourly	$8.54/t
Consumables	
Reagents	$14.29/t
Steel	$2.60/t
Spares	$2.95/t
Misc.	$1.25/t
Power	$4.72/t
Misc. (contingency)	$2.00/t
Total	**$38.82/t**

Labour costs were developed by preparing a complete manpower schedule for the processing operations and then applying typical base rates and burdens for current operations in the Timmins area. This is summarized in Table .

Power and consumables consumption quantities were estimated based on the mass balance and equipment list generated for the project. Current consumable costs were applied as well as an overall supplied power rate of $0.07/kWh. Other operating cost components were estimated as follows:

- Annual operating spares calculated as 5% of installed mechanical equipment costs.
- Allowance of $1.25/t for misc. consumables which may be required for laboratory, safety equipment and vehicle fuel/maintenance
- A $2/t contingency to account for outside consultants and contract services.

TABLE 21-8 PROCESS PLANT LABOUR COSTS

	Qty.	Rate	w/Benefits	Total Cost
Hourly Personnel				
Mill lead	4	$35.00	$52.50	$458,640.00
Mill op 1	4	$30.00	$45.00	$393,120.00
Mill op 2	4	$28.00	$42.00	$366,912.00
Plant op 1	4	$30.00	$45.00	$393,120.00
Plant op 2	4	$28.00	$42.00	$366,912.00
Control room	8	$35.00	$52.50	$917,280.00
Assayers	2	$25.00	$37.50	$156,000.00
Samplers	2	$20.00	$30.00	$124,800.00
Mechanics	2	$32.00	$48.00	$199,680.00
Electricians	2	$32.00	$48.00	$199,680.00
Warehouse manager	1	$28.00	$42.00	$87,360.00
Warehouse helper	4	$23.00	$37.50	$258,336.00
Labour - general	4	$20.00	$27.00	$224,640.00

Labour - security	6	$20.00	$27.00	$336,960.00
Salaried Personnel (Mgmt/Admin)				
Mill superintendent	1	$190,000.00	$66,500.00	$256,500.00
General foreman	1	$140,000.00	$49,000.00	$189,000.00
MTC foreman	1	$120,000.00	$42,000.00	$162,000.00
Senior metallurgist	1	$130,000.00	$45,500.00	$175,500.00
Process technician	2	$100,000.00	$35,000.00	$270,000.00
Inst. technician	2	$90,000.00	$31,500.00	$243,000.00
Total Work Force	**59**			**$5,779,440.00**
Cost per Mined Tonne				**$11.01**

21.4.4. G&A COSTS

The general and administrative (G&A) costs for the plant is estimated at $2.25M per year or $4.20 per tonne (see Table 21-9).

TABLE 21-9 G&A COSTS

Area: New Plant	**Total per annum**
President	$250,000
CFO	$180,000
COO	$180,000
Controller	$130,000
Accountant	$90,000
Purchasing Agent	$60,000
Payable/receivable Clerk	$90,000
Secretary	$60,000
Sub-total	$1,040,000
Burden (@ 35%)	$364,000
Materials & Services (@60%) Includes Audit Services, Consultants, Office	$842,400
G&A Cost	**$2,246,400**
Cost per Mined Tonne	**$4.28**

22. ECONOMIC ANALYSIS

<u>Note:</u> The PEA is preliminary in nature. It includes indicated and inferred mineral resources, which are considered too speculative geologically to have the economic consideration applied to them that would enable them to be categorized as mineral reserves and there is no certainty that the preliminary economic assessment will be realized.

22.1. LOM PLAN AND ECONOMICS

The base case economic analysis for the Frankfield East gold deposit is based on the current resource estimate filed by ACA Howe on August 3, 2011 -- 348,000 indicated ounces (1,621,000 tonnes at 6.68 g/t Au) and 838,900 inferred ounces (4,342,000 tonnes at 6.01 g/t Au). The study envisions the construction of a new mine and processing facility with an average annual production of 95,000 ounces of gold at a cash cost of $660 per ounce over a 10-year mine life. Under this scenario and at a gold price of $1,200 /oz, the Frankfield East gold deposit would be expected to generate $265 million in pre-tax net cash flow, a pre-tax NPV (5% discount) of $159 million and a pre-tax IRR of 23% (USD/CAD = 1). Additional details of the parameters utilized in the model are described in the table below.

TABLE 22-1 BASE CASE ECONOMIC MODEL PARAMETERS

<u>Item</u>	**<u>Value</u>**
Mining / Processing Throughput	1,500 tpd
Mineable Resource (based on total indicated+inferred resources)	85%
Mine Life	10 years
Total Mining Costs	$69 per tonne
Crushing /Truck Haulage	$7 per tonne
Total Processing Costs	$39 per tonne
G & A Costs	$4.30 per tonne
Gold Price (USD)	$1,200 per oz.
Exchange rate	1 USD/CAD
Overall Gold Recovery	95%
<u>Initial Capital Costs</u> ($167 million)	
Process Plant / Infrastructure / Owner's Costs	$130 million
Mine Development	$21 million
Mine Site	$12 million
<u>Sustaining Capital Costs</u> (LOM - $86 million)	
Phase 2 Tailings Expansion	$5 million
Mine Shaft Construction	$50 million
Sustaining Capital (LOM)	$20 million
Mine Closure Costs (less $4 million salvage value)	$11 million

For reference, the Frankfield East deposit operating costs can be compared with the average global gold mining cost of $620 /oz as published in June 2011 by ABN AMRO Bank and VM Haliburton

Mineral Services. At the gold prices of $1,200 /oz selected for the current PEA study the operating costs estimated for the Frankfield East deposit would appear to support the use of a 3 g/t cut-off grade as is utilized in the current resource estimate.

22.2. CASH FLOW FORECASTS

An annual LOM cash flow forecast is presented in Table . The economic model used in the current PEA study is simplified as follows:

- Average diluted LOM mined material grades are used for all production years;
- All preproduction capital costs are assumed to take place in Year 0
- Mining unit costs, processing unit costs and gold recoveries are assumed to be equal to their LOM averages for all production years
- Gold prices are constant at $1,200 /oz
- No inflation is incorporated into the model parameters
- No allowances are made for depreciation or taxes.

22.3. PAYBACK

The preliminary economic assessment (PEA) cash flow model confirms a pre-tax net cash flow ("PNCF") of $265 million and a 3.3 year payback period based on the current resources with annual production averaging 95,000 ounces over a 10 year mine life.

TABLE 22-2 FRANKFIELD EAST DEPOSIT BASE CASE CASH FLOW MODEL

			Year 0	1	2	3	4	5	6	7	8	9	10	11	12	Total
Resource																
Beginning of Year																
Tonnes (M)			5321978	5321978	4796378	4270778	3745178	3219578	2693978	2168378	1642778	1117178	591578	65978	0	
Grade (g/t)			5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	0.00	
Contained Ounces			1,008,942	1,008,942	909,298	809,655	710,011	610,368	510,725	411,081	311,438	211,795	112,151	12,508	0	
End of Year																
Tonnes (M)			5321978	4796378	4270778	3745178	3219578	2693978	2168378	1642778	1117178	591578	65978	0	0	
Grade (g/t)			5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	0.00	0.00	
Contained Ounces			1,008,942	909,298	809,655	710,011	610,368	510,725	411,081	311,438	211,795	112,151	12,508	0	0	
Production and Sales																
Ore Mined and Milling		525600		525600	525600	525600	525600	525600	525600	525600	525600	525600	525600	65978	0	5321978
Mined Grade (g/t)		5.90		5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	5.90	0.00	0.00
Gold Mined (ounces)		99,643		99,643	99,643	99,643	99,643	99,643	99,643	99,643	99,643	99,643	99,643	12,508	0	1,008,942
Gold Recovery (%)		95.0%		95.0%	95.0%	95.0%	95.0%	95.0%	95.0%	95.0%	95.0%	95.0%	95.0%	95.0%	0.0%	95.0%
Gold Recovered (ounces)		94,661		94,661	94,661	94,661	94,661	94,661	94,661	94,661	94,661	94,661	94,661	11,883	0	958,494
Royalty (NSR %)		0.0%		0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Gold Royalty (ounces)		0		0	0	0	0	0	0	0	0	0	0	0	0	0
Gold Sales (ounces)		94,661		94,661	94,661	94,661	94,661	94,661	94,661	94,661	94,661	94,661	94,661	11,883	0	958,494
Gold Price (US$/ounce)		1200.00		1200.00	1200.00	1200.00	1200.00	1200.00	1200.00	1200.00	1200.00	1200.00	1200.00	1200.00	0.00	1200.00
Net Revenue (US$ millions)		113.6		113.6	113.6	113.6	113.6	113.6	113.6	113.6	113.6	113.6	113.6	14.3	0.0	1150.2
Net Ore Value (US$/tonne)		216.12		216.12	216.12	216.12	216.12	216.12	216.12	216.12	216.12	216.12	216.12	216.12	0.00	216.12
Operating Costs																
Mining																
	US$/tonne milled	68.81		66.81	66.81	68.81	68.81	68.81	68.81	68.81	68.81	68.81	68.81	68.81	0.00	68.41
	US$ millions	36.2		35.1	35.1	36.2	36.2	36.2	36.2	36.2	36.2	36.2	36.2	4.5	0.0	364.1
Crushing and Haulage																
	US$/tonne milled	7.00		7.00	7.00	7.00	7.00	7.00	7.00	7.00	7.00	7.00	7.00	7.00	0.00	7.00
	US$ millions	3.7		3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	0.5	0.0	37.3
Process Cost																
	US$/tonne conc.	38.82		38.82	38.82	38.82	38.82	38.82	38.82	38.82	38.82	38.82	38.82	38.82	0.00	38.82
	US$ millions	20.4		20.4	20.4	20.4	20.4	20.4	20.4	20.4	20.4	20.4	20.4	2.6	0.0	206.6
Administration and Environmental																
	US$/tonne milled	4.16		4.16	4.16	4.16	4.16	4.16	4.16	4.16	4.16	4.16	4.16	4.16	0.00	0.00
	US$ millions	2.2		2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	0.3	0.0	22.1
Transportation, Refining and Insurance																
	US$/oz	3.0		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	0.0	3.0
	US$ millions	0.3		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.0	0.0	2.9
Total																
	US$/tonne milled	119.33		117.33	117.33	119.33	119.33	119.33	119.33	119.33	119.33	119.33	119.33	119.33	0.00	118.94
	US$ millions	62.7		61.7	61.7	62.7	62.7	62.7	62.7	62.7	62.7	62.7	62.7	7.9	0.0	633.0
	US$/oz	662.6		651.5	651.5	662.6	662.6	662.6	662.6	662.6	662.6	662.6	662.6	662.6	0.0	660.4
Capital Costs																
Capital (US$ millions)		221.5	159.0	7.5	0.0	0.0	25.0	30.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	221.5
Sustaining Capital (US$ millions)		2.2	0.0	0.0	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	0.0	0.0	19.9
Closure (US$ millions)		15.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	15.0	0.0	15.0
Salvage Value (US$ millions)		4.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	4.0
Cash Flow			-159.0	44.4	49.7	48.7	23.7	18.7	48.7	48.7	48.7	48.7	48.7	-4.6	0.0	264.8
Cummulative Cash Flow			-159.0	-114.6	-64.9	-16.2	7.5	26.1	74.8	123.4	172.1	220.7	269.4	264.8	264.8	

22.4. SENSITIVITY

The results of a sensitivity analysis performed on the Frankfield East gold deposit base case economic model are shown in Table 22-3.

TABLE 22-3 PEA BASE CASE SENSITIVITY ANALYSIS

			Cash Cost	**Project NPV: ($millions)**		
Sensitivity	Variances	Value	USD/ oz	0%	5%	IRR
Gold Price	-15%	$1,020	$660	$92	$32	10%
($ / oz gold)	Base Case	$1,200	$660	$265	$159	23%
	+15%	$1,380	$660	$437	$285	36%
Mined Gold Grade	-15%	5.0 g/t	$779	$92	$32	10%
(g/t gold)	Base Case	5.9 g/t	$660	$265	$159	23%
	+15%	6.8 g/t	$577	$437	$285	36%
Total LOM Capital	-15%	$215	$660	$301	$191	30%
($ millions)	Base Case	$252	$660	$265	$159	23%
	+15%	$290	$660	$229	$127	18%
Mining Cost	-15%	$58/ tonne	$603	$320	$200	27%
(per tonne of ore)	Base Case	$69/ tonne	$660	$265	$159	23%
	+15%	$79/ tonne	$718	$210	$120	19%
Process Cost	-15%	$33/ tonne	$628	$296	$182	26%
(per tonne of ore)	Base Case	$39/ tonne	$660	$265	$159	23%
	+15%	$45/ tonne	$693	$243	$136	21%

The sensitivity modeling demonstrates that the project economics are most impacted by variations in gold prices and mined gold grades and least impacted by capital requirements and operating costs.

Gowest is continuing to drill at the Frankfield East deposit with an intention of expanding the resource base. A sensitivity analysis was completed in Table to demonstrate the impact of potential increases in gold resources on the base case PEA results. Parameters used to calculate the NPV and IRR remain the same with the following exceptions for the +50% resource case:

- Mine production and processing rate increased by 50% to 2,250 tpd
- Capital costs are factored from the base case values based on the increased throughput (initial capital requirement of $258 million)
- Unit operating costs unchanged with the exception of the labour, which was assumed to be reduced based on the change in throughput (total labour costs unchanged but unit costs reduced)

TABLE 22-4 INCREASE IN GOLD RESOURCE RESULTS (@ $1,200 PER OZ GOLD PRICE.)

			Cash Operating Cost	Project NPV ($millions)		
Sensitivity	**Total LOM Capital**	**Mine Life**	**USD/ oz**	**0%**	**5%**	**IRR**
Gold Resources +20% 1500 tpd	$257	12	$660	$367	$214	25%
Gold Resources +50% 2250 tpd	$307	10	$626	$518	$327	28%

22.5. OTHER ANALYSIS: SHORT-TERM CONTRACT PROCESSING

Early on in the current Gowest metallurgical testwork program it was determined that an opportunity existed to effectively separate the arsenopyrite and the pyrite components in the ore. In doing so a high grade (+80 g/t Au) flotation concentrate could be produced with a 3-4% reduction in overall gold recoveries (versus PEA Base Case scenario). Although this opportunity was not selected as the basis for the current PEA study a preliminary evaluation was completed as part of the current sensitivity analyses to examine its potential for a short-term production scenario.

A cash flow model was developed to examine a scenario in which existing processing facilities near the Frankfield East deposit could be used to custom treat the Frankfield East ore producing a high grade gold flotation concentrate that could then be shipped to a third party for final processing (existing pressure oxidation facilities). The intention of this evaluation was to determine if an alternative might exist to bring the Frankfield East deposit into production on a fast-track schedule while final design/permitting was completed on the longer term greenfield processing facilities as were evaluated in the current PEA.

The basic framework of this alternate development scenario is as follows:

- Mine development would be as per the base case development.
- Ore from the mine would be transported to a nearby existing processing facility where a high grade (80-90 g/t) gold bearing sulphide concentrate would be produced.
- The sulphide concentrate would then be transported to rail cars and shipped for final processing at a third-party location.

Discussions are ongoing between Gowest and a number of existing processing facilities that would be suitable for this development scenario. Although no contract terms have been finalized, some reasonable values were incorporated into a financial model for the Frankfield East deposit. Details of these model assumptions are presented in Table . A conservative allowance of $12 million in capital upgrades at the existing processing facilities has been included at this time in order to handle the receiving and processing of the Frankfield East materials. Should this option be pursued further, this amount can be reevaluated based on the final site selections.

Highlights from this alternative development opportunity include:

- Initial capital requirement of $60 million

- Total cash costs (including G&A) estimated at $891 per ounce at $1,200 / oz gold price
- Pre-tax positive cash flows of $28 million annually at $1,200 /oz gold price, which rises to approximately $52 million annually at a short term gold price of $1,500 / oz
- Payback of mine development costs in 1-2 years, depending on gold price.

The results from the preliminary evaluation of a short-term contract processing scenario are sufficiently positive that this opportunity should be investigated further. If successful, the Company would be able to fast-track mine development activities at Frankfield East thereby enabling positive cash flows to be generated in a period of less than 2 years from start of construction. Concurrently with this development work, the Company would continue the design and permitting of a long-term processing facility. Should discussions indicate that favorable terms can be negotiated with contract treatment facilities, an updated PEA can be prepared to examine the combination of the short-term contract and long-term standalone scenarios.

TABLE 22-5 MODEL PARAMETERS FOR SHORT-TERM CONTRACT PROCESSING SCENARIO

Item	**Value**			
Mining / Processing Throughput	1,500			tpd
Mine Life	10			years
Total Mining Costs	$69			per tonne
Crushing /Truck Haulage	$12			per tonne
Custom Processing Costs (concentrate production only)			$30	per tonne
Custom Concentrate Treatment Charges (including transportation)			$42	per tonne
G & A Costs			$3.00	per tonne
Exchange rate		1		USD / CAD
Overall Gold Recovery		93		%
<u>Initial Capital Costs</u>				
Process Plant Upgrades / Infrastructure / Owner's Costs		$21		million
Mine Development		$21		million
Mine Site		$14		million
Royalty Purchase (2% NSR)		$4		million

It should be noted that the short-term contract processing scenario is presented for information purposes only and is not considered as a viable development scenario under the current PEA study. Should Gowest wish to pursue this alternative further an additional PEA study should be completed to better evaluate its economic potential.

23. ADJACENT PROPERTIES

The reader is cautioned that the information in this section is not necessarily indicative of the mineralization on the property that is the subject of this report.

23.1. SGX RESOURCES INC. AND SAN GOLD CORPORATION'S NORTH TIMMINS PROPERTY

SGX Resources Inc. and San Gold Corporation's North Timmins Property lies immediately south of and is contiguous to Gowest's Frankfield Gold Project.

The Nickel Offsets deposit lies within the North Timmins Property and was discovered in 1968 by McIntyre Mines Limited while testing conductive horizons for base metal mineralization potential. The Nickel Offsets deposit has been renamed through successive property holders and has been alternately known as the Tully, Black Pearland most recently the North Timmins deposit. The deposit is located approximately 2 km to the south of the Frankfield East Deposit and is associated with conductive mineralization, mainly graphite and disseminated sulphides within a shear zone adjacent to ultramafic volcanic rocks. The shear zone trends at N080°E, dips steeply north, and is interpreted to be have a strike length of 1.6 km on the property.

This mineralized structure appears to be localized in tuffaceous mafic volcanic rocks (shear zone) adjacent to the contact between Porcupine Assemblage sedimentary rocks to the north and Kidd-Munro Assemblage mafic / ultramafic volcanic rocks to the south. Gold occurs in the native form along with subordinate amounts of disseminated pyrite and arsenopyrite within, and marginal to, the quartz carbonate veins. Diamond drilling indicates that three vein systems occur over a 25-50 m true width for a strike length of more than 450 m, and to a depth of more than 335 m. Both hanging wall and footwall vein systems are parallel to shearing foliation and a middle vein system is approximately perpendicular to these bounding vein systems.

24. OTHER RELEVANT DATA AND INFORMATION

No additional information or explanation is necessary to make this Technical Report understandable and not misleading.

25. INTERPRETATION AND CONCLUSIONS

The objectives of this report are to update the mineral resource estimate for the Frankfield East deposit. Since the previous report with an effective date of November 2011, Gowest has completed 46 diamond drill holes with an aggregate depth of 14,835 m. The database and the geological and structural models have all been updated. Whereas, the previous NI 43-101 report relied on a polygonal estimate, a block model has been developed. Gowest considers that the block model will be more useful for ongoing mine planning and other work that the company wishes to undertake.

TABLE 25-1 MINERAL RESOURCE ESTIMATE				
Frankfield East deposit –Gowest Gold Ltd.				
Indicated Resources				
Lens ID	**Volume**	**Tonnes**	**Oz Au**	**Grade g/t Au**
MZ1	521,908	1,487,438	241,497	**5.05**
MZ2	469,064	1,336,832	200,283	**4.66**
HWZ1	484,036	1,379,503	214,659	**4.84**
HWZ2	451,000	1,285,350	207,033	**5.01**
HWZ3	185,060	527,421	82,070	**4.84**
Totals	**2,111,068**	**6,016,544**	**945,542**	**4.88**
Inferred Resources				
Lens ID	**Volume**	**Tonnes**	**Oz Au**	**Grade g/t Au**
MZ1	995,816	2,838,076	425,198	4.66
MZ2	33,232	94,711	9,987	3.28
HWZ1	189,852	541,078	69,409	3.99
HWZ2 (50m)	41,856	119,290	16,951	4.42
HWZ3 (50m)	34,988	99,716	15,228	4.75
Totals	**1,295,744**	**3,692,871**	**536,773**	**4.22**

Notes:
1. (CIMM) Canadian Institute of Mining, Metallurgy and Petroleum definitions were followed for Mineral resources.
2. Mineral Resources are estimated at a cut-off grade of 3 g/t Au.
3. Mineral Resources are estimated at a long-term gold price of US$1,200/oz, and a US$/C$ exchange rate of 1:1.
4. A minimum width of 2 m was used.
5. The mineral Resource estimate is based on drilling up to April 2012

26. RECOMMENDATIONS

The major part of the recommendations in this report is taken from Ling and Trinder (2012). The recommendation deal with the preparation of a final feasibility study and initial detailed mine planning. Further drilling in the upper part of the deposit is considered necessary. All of this work will be carried out to, or for the advancement of the Frankfield Block.

Some drilling is required as part of the agreement with Transition Metals. This work will be carried out outside the Frankfield Block.

TABLE 26-1 RECOMMENDED PROGRAM COSTS	
Frankfield Project – Gowest Gold Ltd.	
Item	**C$**
Milling	
Final Engineering Agreement and Feasibility Study	800,000
Mining	
Block model development	150,000
Mine development plans	300,000
Further diamond drilling (20,000 m @$125/m)	2,500,000
Mining permits	350,000
General and Administration	
G&A	2,200,000
Subtotal	**6,300,000**
10% contingency	630,000
Outside Exploration	
Transition Metals Option	500,000
Grand Total	**7,430,000**

Any further work will follow the completion of the Feasibility Study.

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28. SIGNATURE PAGE

This report titled "Updated Mineral Resource Estimate, North Timmins Project, Timmins, ON" and dated November 15, 2012 was prepared by and signed by the following authors:

Date
November 15, 2012

Neil N. Gow, B.Sc. (Hons.), P. Geo.
Consulting Geologist

Date
November 15, 2012

Kevin Montgomery, M.Sc. (App.),P.Geo
Consulting Geologist

Date
November 15, 2012

Ms Peimeng Ling,, M.Sc., P.Eng.
Consulting Engineer

29. CERTIFICATE OF QUALIFICATIONS

29.1. NEIL N. GOW

As an author of this report entitled "Updated Mineral Resource Estimate, North Timmins Project, Timmins, ON" prepared for Gowest Gold Ltd., and November 15, 2012, I hereby make the following statements:

A. My name is Neil Neville Gow and I am a Consulting Geologist. My office address is Suite 1400, 80 Richmond Street West, Toronto, Ontario.

B. I have received the following degrees in Geological Sciences:
   - BSc.(Hons) 1965 University of New England, Armidale, NSW Australia

C. I am a registered Professional Geologist in the Province of Ontario. I am also a member of:
   a. The Canadian Institute of Mining, Metallurgy, and Petroleum (CIM)
   b. The Prospectors and Developers Association of Canada (PDAC)
   c. Society of Economic Geologists (SEG).

D. I have read the definition of "Qualified Person" set out in National Instrument 43-101 ("NI-43-101") and certify by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience I fulfill the requirements to be a "Qualified Person" for the purposes of NI 43-101. My relevant experience for the purpose of this report is:
   - Mineral resource and mineral reserve audit Homestake Mine, SD
   - Mineral Resource Estimate, Dome Mine, Timmins, ON.

E. This report is based on my personal review of technical reports and other data supplied by the Issuer, on discussions with the Issuer and its representatives, discussions with the geologists working for Geological Team on the property. I have visited the property twice. The most recent time was on March 11, 2011.

F. I have been practicing as a professional geologist for more than thirty years.

G. I have not had prior involvement with the properties that are the subject of this technical report.

H. I am responsible for all sections of the report.

I. I am not aware of any material fact with respect to the subject matter of this report which is not reflected in "the Report" the omission to disclose which makes this report misleading.

J. I am independent of the issuer applying the tests set out in section 1.5 of National Instrument 43-101. I have read National Instrument 43-101 and Form 43-101F1 and this report has been prepared in compliance with National Instrument 43-101 and Form 43-101F1.

K. I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them for regulatory purposes including electronic publication in the public company files on their websites accessible by the public of the Technical Report.

PROFESSIONAL GEOSCIENTISTS
NEIL NEVILLE GOW
PRACTISING MEMBER
0433
ONTARIO

Dated at Toronto, Ontario
November 15, 2012

Neil N. Gow, B.Sc. (Hons.), P. Geo.
Consulting Geologist

29.2. KEVIN MONTGOMERY

I, Kevin Montgomery, residing at 1190 Lozanne Crescent, Timmins, Ontario do hereby certify that:

1) I am an independent Professional Consulting Geoscientist with an office at 1190 Lozanne Crescent, Timmins, Ontario, Canada P4P 1E8.

2) I hold a B.Sc. Honours degree in Geological Sciences (1984) from Queen's University, Kingston, Ontario and a M.Sc. (App.) degree in Mineral Exploration (1987) from McGill University, Montreal, Quebec. I have practiced my profession continuously from 1993 as a consulting geologist for a number of major and junior mining companies and from 1984 to 1992 as a geologist with Gold Fields Canadian Mining Limited. I have worked in mining exploration continuously over the last twenty eight years, predominantly in the Abitibi area. My gold exploration experience in the Abitibi ranges from conceptual grassroots exploration through to underground drilling on advanced projects.

3) I am a member in good standing of the Association of Professional Geoscientists of Ontario, Membership # 0659;

4) I have personally visited the North Timmins Project on various occasions and supervised the Frankfield East Gold Deposit exploration work for Gowest Gold since July 2010;

5) I have read the definition of "qualified person" set out in National Instrument 43-101 and certify that by virtue of my education, affiliation to a professional association and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of National Instrument 43-101 and this technical report has been prepared in compliance with National Instrument 43-101 and Form 43-101F1;

6) I, as a qualified person, I am independent of the issuer as defined in Section 1.5 of National Instrument 43-101;

7) I contributed to the compilation of this report and co-authored Sections 1 to 12 and 23 to 27 of this technical report;

8) That, as of the date of this certificate, to the best of my knowledge, information and belief, this technical report contains all scientific and technical information that is required to be disclosed to make the technical report not misleading;

9) I consent to the filing of the technical report with any stock exchange and other regulatory authority and any publication for regulatory purposes, including electronic publication in the public company files on their websites accessible to the public of extracts from the technical report.

Dated at Timmins, Ontario
November 15, 2012

Kevin Montgomery, M.Sc. (App.), P.Geo.
Consulting Geologist

29.3. PEIMENG LING

I, Peimeng Ling, M.Sc., P.Eng. (Ontario), do hereby certify that:

1. I reside at 39 Clovercrest Road, Toronto, Ontario, Canada, M2J 1Z5,
2. I am President of Peimeng Ling & Associates Limited located at 39 Clovercrest Road, Toronto, Ontario, Canada, M2J 1Z5
3. I hold the following academic qualifications:

   B.Eng. (Chemical Engineering) Zhejiang University, PRC 1982

   M.Sc. (Chemical Engineering) University of Toronto, Canada 1994
4. I am a registered Professional Engineer with Professional Engineers Ontario (Registration Number 90444985). I am a member of The Canadian Institute of Mining, Metallurgy and Petroleum (CIM).
5. I have over 15 years of direct experience with precious and base metals mineral and hydrometallurgical processing in Canada, USA, Brazil, and Russia including test work, project feasibility study, process design, plant design, environmental compliance, and financial evaluation with a variety of deposit types including gold, silver, copper, zinc, nickel, cobalt, vanadium, platinum-group metals and industrial minerals. Additional experience includes the completion of various NI 43-101 technical reports for vanadium, talc-magnesite deposit projects.
6. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
7. I am author of the technical report titled: "Updated Mineral Resource Estimate, North Timmins Project, Timmins, ON**"** for Gowest Gold Ltd. dated November 15, 2012, (the "Technical Report"). I am responsible for Sections 13 and 16 to 22. I visited the Frankfield Gold Project between December 7th and 9th, 2011.
8. I have previously prepared a National Instrument Report entitled "Preliminary Economic Assessment on the Frankfield Gold project, Tully Township, North-eastern Ontario"
9. As of the effective date of the technical report, to the best of my knowledge, information, and belief, the technical report contains all scientific and technical information that is required to be disclosed to make the technical report not misleading.
10. I am independent of the issuer applying all of the tests in section 1.5 of National Instrument 43-101.
11. I have read National Instrument 43-101 and Form 43-101F1, and the Technical Report has been prepared in compliance with that instrument and form.
12. I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public, of the Technical Report.

EFFECTIVE DATE: November 15, 2012
AMENDED: April 17, 2012
DATED this 15th Day of November, 2012.

LICENSED PROFESSIONAL ENGINEER
P. LING
PROVINCE OF ONTARIO

Peimeng Ling, M.Sc., P.Eng.
Consulting Engineer

30. APPENDIX 1

TABLE 30-1 MINERALIZED INTERSECTIONS, FRANKFIELD EAST DEPOSIT				
n/a= no sample taken in this area of the drill hole.				
Hole ID	**From**	**To**	**Grade**	**Zone**
74-03	65.53	74.95	4.13	MZ1
75-04	72.15	75.01	1.31	MZ1
75-05	56.98	60.93	n/a	MZ1
75-06	74.49	76.78	3.25	MZ1
75-07	64.59	66.6	1.92	MZ1
75-08	59.44	67.36	0.88	MZ1
75-09	73.15	88.88	3.53	MZ1
75-10	68.31	72.39	1.49	MZ1
75-11	103.23	105.81	0.73	MZ1
75-12	122.56	125.47	n/a	MZ1
75-13	56.28	59.96	0.28	MZ1
75-14	76.86	79.89	0.69	MZ1
76-15	90.61	93.88	n/a	MZ1
76-16	101.13	111.86	2.74	MZ1
76-17	56.2	59.74	2.41	MZ1
76-18	120.83	122.83	2.03	MZ1
76-19	109.1	111.1	1.09	MZ1
76-20	46.97	50.19	0.07	MZ1
76-21	29.15	33.13	n/a	MZ1
76-24	157.79	160.69	n/a	MZ1
80-1	90.03	94.12	0.60	MZ1
80-2	84.8	89.18	3.26	MZ1
80-3	212.54	213.36	n/a	MZ1
80-4	110.55	113.23	n/a	MZ1
81H-11	14.1	20.39	n/a	MZ1
82-2	185.66	189.05	0.17	MZ1
88-1	177.29	184.13	0.13	MZ1
88-10	135.46	137.46	2.09	MZ1
88-11	351.19	355.2	n/a	MZ1
88-12	253.62	295.67	1.02	MZ1
88-13	331.93	334.06	4.13	MZ1

88-14	263.48	265.48	8.60	MZ1
88-15	284.18	287.34	0.00	MZ1
88-16	341.16	344.7	n/a	MZ1
88-2	146.01	149.85	0.09	MZ1
88-21	543.74	555.01	0.79	MZ1
88-3	119.58	121.58	8.14	MZ1
88-4	167.27	170.78	0.00	MZ1
88-5	146.81	150.18	0.00	MZ1
88-6	111.6	114.77	n/a	MZ1
88-7	91.23	94.03	5.90	MZ1
88-8	91.51	93.51	1.37	MZ1
88-9	154.08	161.85	3.34	MZ1
89-GO-1	556.76	558.76	7.99	MZ1
89-GO-3	603.3	625.94	5.32	MZ1
90-GO-5	632.7	644.38	1.35	MZ1
GW04-01	192.5	197.5	4.24	MZ1
GW04-02	208.23	214.5	5.27	MZ1
GW04-03A	194	196	17.30	MZ1
GW04-04	197	199	1.84	MZ1
GW04-05	210	213	14.29	MZ1
GW04-06	217	228	3.66	MZ1
GW04-07	242.31	245.47	0.06	MZ1
GW04-08	248.9	251.9	8.27	MZ1
GW04-09	251.43	255.16	n/a	MZ1
GW04-10	272.88	277.54	0.03	MZ1
GW04-11	207.78	210.22	0.00	MZ1
GW04-12	243	247	1.92	MZ1
GW04-13	268	270	5.83	MZ1
GW04-14	299.9	303.54	0.01	MZ1
GW04-15	294	299	2.01	MZ1
GW04-16	301.26	306.28	n/a	MZ1
GW04-17	309	311	9.80	MZ1
GW04-18	312.25	314.25	1.25	MZ1
GW04-19	191	194	4.78	MZ1
GW04-20	299	301.85	2.70	MZ1
GW04-21	303.5	306.8	3.12	MZ1
GW04-22	449.3	453.25	13.24	MZ1
GW05-23	422.5	425.5	1.41	MZ1
GW05-24	372.05	374.92	0.00	MZ1
GW04-25	361.82	367.71	n/a	MZ1
GW05-26	350.3	354.8	0.92	MZ1

GW05-27	350	355.5	6.10	MZ1
GW05-28	379.2	381.2	2.53	MZ1
GW05-29	390.5	399.5	1.99	MZ1
GW05-30	408.5	412.6	2.03	MZ1
GW05-31	315.1	317.1	1.86	MZ1
GW06-32	132	137	2.87	MZ1
GW06-33	116	124	6.06	MZ1
GW06-34	106.51	109.5	0.13	MZ1
GW06-35	160.44	165.03	0.29	MZ1
GW06-36	128.21	131.16	0.15	MZ1
GW06-37	121.52	125.11	0.02	MZ1
GW06-38	125	132	5.50	MZ1
GW08-39	219.64	222	11.49	MZ1
GW08-40	184.29	187.19	0.45	MZ1
GW08-41	159.6	161.6	1.32	MZ1
GW08-42	226.53	230.87	0.11	MZ1
GW08-43	198.1	206.75	7.07	MZ1
GW08-44	171.19	177.49	0.02	MZ1
GW10-100	293.41	298.08	0.00	MZ1
GW10-101	209.26	213.66	0.00	MZ1
GW10-102	55	58.32	5.37	MZ1
GW10-103	302	304	1.77	MZ1
GW10-104	194.62	201.98	0.00	MZ1
GW10-105	126.63	130.82	0.45	MZ1
GW10-106	73.3	75.3	1.62	MZ1
GW10-107	282.85	292.47	0.01	MZ1
GW10-108	190.09	192.99	n/a	MZ1
GW10-109	292.9	294.9	2.55	MZ1
GW10-110	335.09	338.13	0.00	MZ1
GW10-112	305.5	307.8	3.14	MZ1
GW10-113	59.4	62	6.53	MZ1
GW10-114	69.4	71.4	0.54	MZ1
GW10-119	148.03	150.81	0.00	MZ1
GW10-122	352.19	355.73	n/a	MZ1
GW10-125	67.76	69.23	0.00	MZ1
GW10-126	260.4	264.4	7.92	MZ1
GW10-128	67.92	70.07	0.00	MZ1
GW10-130	58.59	61.46	0.04	MZ1
GW10-131	194.58	197.78	0.00	MZ1
GW10-133	305	307.2	1.68	MZ1
GW10-134	702	706.8	1.49	MZ1

GW10-135	43	45	3.38	MZ1
GW10-136	63.38	65.62	0.19	MZ1
GW10-137	161	163	1.90	MZ1
GW10-138	212	215	1.53	MZ1
GW10-140	110.7	112.9	5.48	MZ1
GW10-141	229.8	231.8	4.42	MZ1
GW10-142	163.48	173	0.19	MZ1
GW10-143	244.92	256.51	0.21	MZ1
GW10-144	43.3	46.4	4.75	MZ1
GW10-145	121.66	124.79	0.17	MZ1
GW10-146	42.23	46.8	n/a	MZ1
GW10-45	196.2	209	1.15	MZ1
GW10-46	691	701	6.41	MZ1
GW10-47	447.7	464.8	0.74	MZ1
GW10-49	335.66	344.48	n/a	MZ1
GW10-51	315.26	319.98	0.10	MZ1
GW10-52	476.8	480.95	0.20	MZ1
GW10-55	841.7	843.7	1.25	MZ1
GW10-56	834.15	843.18	n/a	MZ1
GW10-57	507.3	509.3	2.84	MZ1
GW10-58	758	765	2.97	MZ1
GW10-59	570.5	572.5	2.80	MZ1
GW10-60	841	843	1.52	MZ1
GW10-60WA	828	832	5.24	MZ1
GW10-60WB	825	827	3.01	MZ1
GW10-61	123.35	126	10.64	MZ1
GW10-62	473.4	475.4	3.08	MZ1
GW10-76	480.6	482.6	1.50	MZ1
GW10-78	739	746	5.02	MZ1
GW10-82B	533	535	2.59	MZ1
GW10-85	73	75	1.30	MZ1
GW10-86	180.4	182.4	1.12	MZ1
GW10-87B	315.92	321.78	0.00	MZ1
GW10-88	331.7	340.26	0.00	MZ1
GW10-89	100.2	102.2	2.71	MZ1
GW10-90	0	0.1	n/a	MZ1
GW10-91	170	173.1	3.35	MZ1
GW10-92	103.74	106.35	0.28	MZ1
GW10-93	254.16	258.35	0.00	MZ1
GW10-94	250.6	252.6	1.47	MZ1
GW10-95	125.66	128.79	n/a	MZ1

GW10-96	993.3	998.4	4.15	MZ1
GW10-97	99.14	102.63	0.00	MZ1
GW10-98	145	147	3.50	MZ1
GW10-99	217	219	2.41	MZ1
GW11-121	934.8	936.8	6.12	MZ1
GW11-139	927.36	931.77	n/a	MZ1
GW11-147	113	115	5.71	MZ1
GW11-148	167.9	172.97	0.29	MZ1
GW11-149	250	256	5.99	MZ1
GW11-150	222.35	233.4	3.84	MZ1
GW11-151	300.6	303.82	0.00	MZ1
GW11-152	665.4	667.9	8.39	MZ1
GW11-153	204	210	1.59	MZ1
GW11-154	374.77	383.25	0.01	MZ1
GW11-155	1109	1110.99	3.01	MZ1
GW11-157	391	396.5	3.03	MZ1
GW11-159	500.6	513.8	3.14	MZ1
GW11-161	1032	1038	2.35	MZ1
GW11-162	382.15	391.34	0.01	MZ1
GW11-164	207	211	3.06	MZ1
GW11-165	102	104	1.92	MZ1
GW11-166	207.53	211.71	n/a	MZ1
GW11-167	88.36	91.4	0.49	MZ1
GW11-168	73.31	80.42	0.01	MZ1
GW11-169	157.11	163.87	0.03	MZ1
GW11-170	365.62	368.89	0.00	MZ1
GW11-171	91.92	94.43	0.00	MZ1
GW11-172	79.35	81.8	0.48	MZ1
GW11-173	121.72	124.76	0.52	MZ1
GW11-174	162.66	165.58	n/a	MZ1
GW11-175	157.5	159.5	1.33	MZ1
GW11-176	114	116	12.83	MZ1
GW11-177	56.25	60.13	0.03	MZ1
GW11-178	74	76	4.65	MZ1
GW11-179	197.19	200.09	0.00	MZ1
GW11-180	212.81	216	0.01	MZ1
GW11-184	568.39	576.78	0.00	MZ1
GW11-185B	467.39	471.92	0.00	MZ1
GW11-186	419.48	426.74	0.10	MZ1
GW11-187	463	469	1.61	MZ1
GW11-188	172	174	1.47	MZ1

GW11-198	81.79	118.74	2.16	MZ1
GW11-199	0	256.06	1.02	MZ1
GW12-203	573.2	579	3.39	MZ1
T-91-1	452.96	461.97	0.11	MZ1
T-91-2	285.85	288.55	0.61	MZ1
T-91-3	342.75	351.75	1.12	MZ1
T-91-4	456.78	460.88	0.00	MZ1
T-91-5	437.5	439.5	1.90	MZ1
T-91-6	675.7	689.2	0.95	MZ1
T-91-9	546.42	550.61	n/a	MZ1
74-03	55.1	57.82	n/a	MZ2
75-04	62.52	64.08	2.06	MZ2
75-05	53.37	56	0.42	MZ2
75-06	60.69	63.34	1.01	MZ2
75-07	50.6	53.64	1.37	MZ2
75-08	50.17	53.64	11.75	MZ2
75-09	62.56	64.56	4.11	MZ2
75-10	45.55	52.58	n/a	MZ2
75-11	93.86	95.86	2.74	MZ2
75-12	110.02	112.87	n/a	MZ2
75-13	45.25	48.76	0.34	MZ2
75-14	59.32	62.99	n/a	MZ2
76-15	72.5	77.31	n/a	MZ2
76-16	90.71	92.96	10.60	MZ2
76-17	44.87	47.85	1.20	MZ2
76-18	105.81	108.41	0.43	MZ2
76-19	79.61	85.06	0.02	MZ2
76-20	29.73	31.73	1.32	MZ2
76-21	23.3	25.3	1.84	MZ2
80-1	76.57	79.49	3.77	MZ2
80-2	73.32	75.96	n/a	MZ2
80-3	193.63	197.4	n/a	MZ2
80-4	95.85	98.17	n/a	MZ2
82-2	172.52	178.43	0.87	MZ2
88-1	155.65	159.96	0.28	MZ2
88-10	112.06	116.53	2.88	MZ2
88-11	330.5	334.71	n/a	MZ2
88-12	236.92	240.49	2.67	MZ2
88-13	311.64	312.69	n/a	MZ2
88-14	250.08	253.8	0.03	MZ2
88-2	132.06	135.21	n/a	MZ2

88-21	528.99	530.99	3.78	MZ2
88-3	107.34	109.45	0.24	MZ2
88-4	155.85	158.04	0.03	MZ2
88-5	133.78	136.37	n/a	MZ2
88-6	103.26	106.02	n/a	MZ2
88-7	73.02	78.18	n/a	MZ2
88-8	67.02	70.85	n/a	MZ2
88-9	145.64	150.14	0.14	MZ2
89-GO-1	542.63	545.07	1.92	MZ2
89-GO-3	577.55	581.4	n/a	MZ2
90-GO-4	616.88	633.07	2.81	MZ2
90-GO-5	616.47	618.47	2.39	MZ2
GW04-01	173.5	181.5	3.68	MZ2
GW04-02	188.9	191.44	n/a	MZ2
GW04-03A	179.08	183.97	0.01	MZ2
GW04-04	191	193	2.80	MZ2
GW04-05	190	192	3.85	MZ2
GW04-06	209	211	3.00	MZ2
GW04-07	225.42	230.62	0.00	MZ2
GW04-08	230.4	232.6	12.07	MZ2
GW04-09	240.24	244.36	n/a	MZ2
GW04-10	260.49	266.58	n/a	MZ2
GW04-11	189.25	192.03	n/a	MZ2
GW04-12	235.22	238.73	0.05	MZ2
GW04-13	258	265	4.32	MZ2
GW04-14	282.35	285.44	n/a	MZ2
GW04-15	282.56	286.3	n/a	MZ2
GW04-16	285.1	288.14	n/a	MZ2
GW04-17	293	299	2.23	MZ2
GW04-18	280.7	282.7	2.83	MZ2
GW04-19	179.73	183.82	n/a	MZ2
GW04-20	289.5	294.5	1.56	MZ2
GW04-21	296.5	298.5	3.87	MZ2
GW04-22	435.3	441	5.38	MZ2
GW04-25	344.93	349.2	n/a	MZ2
GW05-23	397	399	1.70	MZ2
GW05-24	351.28	354.8	n/a	MZ2
GW05-26	330.1	334.25	n/a	MZ2
GW05-27	336	338	1.11	MZ2
GW05-28	354	357	1.49	MZ2
GW05-29	381.5	388	2.16	MZ2

GW05-30	396.5	399.5	2.32	MZ2
GW05-31	298.28	300.45	n/a	MZ2
GW06-32	126	129	2.42	MZ2
GW06-33	109.25	113.5	1.11	MZ2
GW06-34	89.45	93.24	n/a	MZ2
GW06-35	149.54	152.61	n/a	MZ2
GW06-36	117.49	120.48	n/a	MZ2
GW06-37	109.71	113.65	0.39	MZ2
GW06-38	112	118	1.08	MZ2
GW08-39	208.5	210.5	3.51	MZ2
GW08-40	169.6	178.05	7.46	MZ2
GW08-41	148.77	154.3	n/a	MZ2
GW08-42	201.4	204.1	2.24	MZ2
GW08-43	179.37	181.72	n/a	MZ2
GW08-44	159.6	161.6	2.53	MZ2
GW10-101	179.07	182.21	0.07	MZ2
GW10-102	43.09	46.29	0.01	MZ2
GW10-103	294.33	296.55	0.00	MZ2
GW10-104	169.09	174.71	0.02	MZ2
GW10-105	101.61	110.31	0.00	MZ2
GW10-106	52	61.1	5.61	MZ2
GW10-108	169.74	172.79	0.15	MZ2
GW10-109	277.61	280.2	0.01	MZ2
GW10-110	311.4	313.4	1.15	MZ2
GW10-112	289.76	292.34	0.00	MZ2
GW10-113	37.7	39.7	1.82	MZ2
GW10-114	60.8	62.09	3.23	MZ2
GW10-119	132.37	136.36	0.00	MZ2
GW10-125	36.4	42.2	6.54	MZ2
GW10-126	247.3	254	1.56	MZ2
GW10-128	45.49	49.69	0.56	MZ2
GW10-130	43.44	47.59	0.25	MZ2
GW10-131	178.84	183.71	0.02	MZ2
GW10-133	294.7	301.7	7.06	MZ2
GW10-134	649.58	654.93	n/a	MZ2
GW10-135	30.88	34.26	0.24	MZ2
GW10-136	52.69	55.12	0.00	MZ2
GW10-137	152.5	156	2.09	MZ2
GW10-138	201	208	1.42	MZ2
GW10-140	102.84	104.76	0.00	MZ2
GW10-141	217	223	2.40	MZ2

GW10-142	150.3	152.3	2.11	MZ2
GW10-143	226.41	234.3	0.02	MZ2
GW10-144	34.49	36.65	1.05	MZ2
GW10-145	107.03	109.38	0.00	MZ2
GW10-146	24.14	28.31	0.06	MZ2
GW10-45	183.65	192	6.06	MZ2
GW10-47	418	430.1	2.16	MZ2
GW10-49	283.7	285.7	2.43	MZ2
GW10-55	814.54	817.86	0.00	MZ2
GW10-57	492.84	496.37	0.00	MZ2
GW10-58	752	754	1.51	MZ2
GW10-59	558.1	560.1	4.56	MZ2
GW10-60	819.5	821.5	3.18	MZ2
GW10-60WA	799.63	802.4	0.09	MZ2
GW10-60WB	806.86	807.72	0.02	MZ2
GW10-61	91.27	95.39	n/a	MZ2
GW10-76	438.81	442.68	n/a	MZ2
GW10-78	721	723	1.66	MZ2
GW10-85	45.07	50.92	n/a	MZ2
GW10-86	164.17	174	1.34	MZ2
GW10-87B	279.99	285.86	0.00	MZ2
GW10-88	308.53	318.63	0.11	MZ2
GW10-89	90.7	94.5	4.13	MZ2
GW10-91	157.93	160.95	0.27	MZ2
GW10-92	90.4	92.4	2.25	MZ2
GW10-93	245.45	247.75	0.00	MZ2
GW10-94	238.05	240.71	n/a	MZ2
GW10-95	88.9	90.9	9.69	MZ2
GW10-97	89.4	91.4	2.05	MZ2
GW10-98	139.5	141.5	2.93	MZ2
GW10-99	213	215	2.11	MZ2
GW11-121	912	916	1.86	MZ2
GW11-147	84	94	2.04	MZ2
GW11-148	157.43	159.23	0.18	MZ2
GW11-149	219.13	224.16	0.02	MZ2
GW11-150	215	217	1.23	MZ2
GW11-151	284.73	288.3	0.00	MZ2
GW11-152	622.53	627.75	n/a	MZ2
GW11-153	195.95	198.75	0.18	MZ2
GW11-154	324.93	332.36	0.09	MZ2
GW11-157	371.9	373.9	1.92	MZ2

GW11-159	493.2	497.8	1.52	MZ2
GW11-162	351.78	357.25	0.02	MZ2
GW11-165	85.8	92	6.35	MZ2
GW11-171	80	83	5.24	MZ2
GW11-172	48.5	52	5.67	MZ2
GW11-173	111.18	114.45	0.04	MZ2
GW11-174	150.37	152.82	0.29	MZ2
GW11-175	139.79	143.42	0.00	MZ2
GW11-176	101.51	104.2	0.06	MZ2
GW11-177	52.74	55.3	0.00	MZ2
GW11-178	56.23	59.63	0.02	MZ2
GW11-179	180	182.8	1.77	MZ2
GW11-180	194.12	196.88	0.04	MZ2
GW11-185B	446.45	453.24	n/a	MZ2
GW11-187	442.29	445.08	0.00	MZ2
GW12-203	509	511	1.32	MZ2
T-91-1	430.7	435.7	2.68	MZ2
T-91-2	267.72	272.11	0.01	MZ2
T-91-3	332.75	336.75	0.73	MZ2
T-91-5	408.05	424	1.73	MZ2
T-91-6	617.58	622.51	0.01	MZ2
74-01	91.29	93.6	1.63	HWZ1
74-03	35.81	44.17	3.25	HWZ1
75-04	48.1	56.21	6.47	HWZ1
75-05	27.45	29.62	2.40	HWZ1
75-06	32.69	34.69	5.39	HWZ1
75-07	41.45	49.07	n/a	HWZ1
75-11	76.28	81.98	n/a	HWZ1
75-12	96.96	99.69	n/a	HWZ1
76-17	20.07	22.86	n/a	HWZ1
76-21	5.9	10.57	n/a	HWZ1
76-24	83.23	89.35	0.00	HWZ1
80-1	65.07	69.85	5.49	HWZ1
80-2	44.57	46.57	n/a	HWZ1
80-4	68.58	70.93	1.15	HWZ1
81H-11	100.13	107.6	n/a	HWZ1
82-2	138.17	149.08	1.43	HWZ1
88-10	108.84	111	n/a	HWZ1
88-11	310.83	313.72	n/a	HWZ1
88-13	274.02	277.65	n/a	HWZ1
88-14	220.69	223.49	n/a	HWZ1

88-21	506.36	508.65	7.89	HWZ1
88-3	97.91	102.28	n/a	HWZ1
88-4	139.82	144.27	n/a	HWZ1
88-5	103.92	108.16	n/a	HWZ1
88-6	80.93	82.64	n/a	HWZ1
88-7	55.75	58.87	n/a	HWZ1
88-8	44.1	47.23	n/a	HWZ1
88-9	130.73	133.94	0.00	HWZ1
89-GO-1	531.55	535.87	0.00	HWZ1
89-GO-3	558.72	566.84	4.72	HWZ1
90-GO-5	585.54	601.07	0.37	HWZ1
GW04-01	158	160	1.14	HWZ1
GW04-02	157.79	161.44	n/a	HWZ1
GW04-03A	160.8	165.42	n/a	HWZ1
GW04-04	163.23	165.94	n/a	HWZ1
GW04-05	171	173	4.79	HWZ1
GW04-06	176.27	179.8	n/a	HWZ1
GW04-07	200	202	4.04	HWZ1
GW04-08	200.1	202.1	4.03	HWZ1
GW04-09	224.5	226.5	6.57	HWZ1
GW04-10	243.09	251.17	n/a	HWZ1
GW04-11	154.3	161.87	0.59	HWZ1
GW04-12	229.83	234.38	0.10	HWZ1
GW04-14	268.49	273.92	n/a	HWZ1
GW04-15	260	267.5	1.31	HWZ1
GW04-16	267.5	272.17	0.07	HWZ1
GW04-17	275	277	2.06	HWZ1
GW04-18	256.5	260.99	n/a	HWZ1
GW04-19	147.5	149.5	2.00	HWZ1
GW04-20	257.6	261.9	2.07	HWZ1
GW04-21	266.75	268.75	4.25	HWZ1
GW04-25	326.86	331.49	0.01	HWZ1
GW05-23	348.79	354.96	n/a	HWZ1
GW05-24	336.51	341.37	n/a	HWZ1
GW05-26	311.06	313.98	n/a	HWZ1
GW05-27	322.35	326.97	n/a	HWZ1
GW05-28	342.5	346.5	1.31	HWZ1
GW05-29	372.5	377	1.60	HWZ1
GW05-30	368	369	0.60	HWZ1
GW05-31	285.5	287.5	4.00	HWZ1
GW06-32	98.58	101.37	n/a	HWZ1

GW06-33	89.27	93.36	n/a	HWZ1
GW06-34	65	67	3.24	HWZ1
GW06-35	119.71	122.15	n/a	HWZ1
GW06-36	105	112	2.46	HWZ1
GW06-37	89.46	92.26	0.55	HWZ1
GW06-38	97.86	101.52	n/a	HWZ1
GW08-39	186.63	189.12	n/a	HWZ1
GW08-40	155.55	160.34	n/a	HWZ1
GW08-41	134.39	137.89	n/a	HWZ1
GW08-42	193.57	195.71	n/a	HWZ1
GW08-43	147.81	150.39	n/a	HWZ1
GW08-44	124.8	128.19	n/a	HWZ1
GW10-102	30.8	36	2.36	HWZ1
GW10-104	164.29	166.88	0.36	HWZ1
GW10-105	91.94	95.25	0.01	HWZ1
GW10-106	40	42	2.92	HWZ1
GW10-107	253	258.6	0.07	HWZ1
GW10-108	128.5	130.45	6.05	HWZ1
GW10-109	260.3	267.6	0.81	HWZ1
GW10-110	302.6	305.6	3.74	HWZ1
GW10-112	279.1	281.3	2.20	HWZ1
GW10-113	2.69	8.28	n/a	HWZ1
GW10-114	28.6	31	10.17	HWZ1
GW10-119	111.79	114.25	n/a	HWZ1
GW10-125	3.44	7.34	n/a	HWZ1
GW10-126	237	239	5.09	HWZ1
GW10-131	153.37	156.63	0.00	HWZ1
GW10-133	282.4	290	1.37	HWZ1
GW10-134	612.7	615	1.20	HWZ1
GW10-136	30.9	32.9	1.20	HWZ1
GW10-137	130.06	132.62	0.00	HWZ1
GW10-138	190	192	1.50	HWZ1
GW10-140	85.85	91.25	n/a	HWZ1
GW10-141	204.9	206.9	3.11	HWZ1
GW10-142	125.34	129.85	0.49	HWZ1
GW10-143	203.68	205.78	n/a	HWZ1
GW10-144	20.79	26.46	0.40	HWZ1
GW10-145	91.94	97.51	0.00	HWZ1
GW10-45	164.4	166.7	5.71	HWZ1
GW10-47	398	400	1.76	HWZ1
GW10-55	785	808.4	1.40	HWZ1

GW10-57	483.4	485.4	5.37	HWZ1
GW10-58	712	714	3.50	HWZ1
GW10-60	804	807	2.04	HWZ1
GW10-60WA	790.3	793.3	7.55	HWZ1
GW10-60WB	804	806	1.78	HWZ1
GW10-61	73.92	78.46	n/a	HWZ1
GW10-76	422.88	428.17	n/a	HWZ1
GW10-78	682.67	688.08	0.01	HWZ1
GW10-88	290.34	292.91	1.14	HWZ1
GW10-91	138.25	140.84	n/a	HWZ1
GW10-92	61.3	64.28	0.12	HWZ1
GW10-93	228.45	231	3.55	HWZ1
GW10-94	213	215	2.95	HWZ1
GW10-95	66.69	73.87	0.05	HWZ1
GW10-97	44.5	46.5	2.38	HWZ1
GW10-98	92.9	94.9	8.19	HWZ1
GW10-99	156	158	1.76	HWZ1
GW11-121	889	908	2.68	HWZ1
GW11-148	153	155	1.96	HWZ1
GW11-150	200	205	1.20	HWZ1
GW11-151	265.26	270.17	n/a	HWZ1
GW11-152	586.6	589.8	1.99	HWZ1
GW11-155	1032	1034.5	2.59	HWZ1
GW11-159	481.3	489.3	2.99	HWZ1
GW11-161	977	979.6	1.99	HWZ1
GW11-162	336.73	338.82	0.08	HWZ1
GW11-164	123.31	124.38	n/a	HWZ1
GW11-165	33.49	35.46	n/a	HWZ1
GW11-166	120.47	122.6	n/a	HWZ1
GW11-167	20.59	22.6	n/a	HWZ1
GW11-171	67	71.1	3.45	HWZ1
GW11-172	40.8	44.65	0.53	HWZ1
GW11-173	92	94	1.72	HWZ1
GW11-174	119.5	123.5	0.58	HWZ1
GW11-176	92.1	94.1	1.96	HWZ1
GW11-177	29	31	3.30	HWZ1
GW11-179	137	152.5	0.72	HWZ1
GW11-180	165	167	2.94	HWZ1
GW11-182	102	113.11	0.67	HWZ1
GW11-183	19.63	30.76	0.03	HWZ1
GW11-185B	420	422	2.22	HWZ1

GW11-186	372	374	3.83	HWZ1
GW11-187	435	437	5.12	HWZ1
GW11-188	95	111	3.63	HWZ1
T-91-2	259.7	265.75	2.51	HWZ1
T-91-3	311	313.5	0.38	HWZ1
T-91-5	388.05	391.81	n/a	HWZ1
T-91-6	581.7	584.7	0.68	HWZ1
75-13	2.99	7	n/a	HWZ2
75-14	19.99	22.34	1.37	HWZ2
80-1	39.76	43.3	n/a	HWZ2
80-2	22.86	24.99	1.28	HWZ2
80-4	56.05	58.51	n/a	HWZ2
88-10	85.33	87.96	n/a	HWZ2
88-11	280.25	283.79	n/a	HWZ2
88-13	258.82	260.82	2.69	HWZ2
88-21	474.63	477.47	5.80	HWZ2
88-7	34.96	38.01	n/a	HWZ2
88-8	28.18	30.18	12.72	HWZ2
88-9	110.89	114.24	n/a	HWZ2
89-GO-1	519.55	521.55	2.19	HWZ2
GW04-01	137	141.17	0.12	HWZ2
GW04-02	141.46	145.32	n/a	HWZ2
GW04-03A	141.75	143.75	1.64	HWZ2
GW04-04	134.5	137.5	4.17	HWZ2
GW04-05	155.1	157.48	n/a	HWZ2
GW04-06	156.98	161.08	n/a	HWZ2
GW04-07	176.94	180.13	0.46	HWZ2
GW04-08	168.2	177.2	1.80	HWZ2
GW04-09	211.5	214.5	1.20	HWZ2
GW04-11	126.43	139.45	0.29	HWZ2
GW04-15	250.5	252.5	1.38	HWZ2
GW04-16	238.79	243.45	n/a	HWZ2
GW04-17	246	248	2.03	HWZ2
GW04-18	236.24	239.25	0.39	HWZ2
GW04-20	237.5	241.5	3.32	HWZ2
GW04-21	227.85	229.85	1.82	HWZ2
GW04-25	309.1	318.5	8.44	HWZ2
GW05-26	278.69	282.27	0.03	HWZ2
GW05-27	302.5	311	8.51	HWZ2
GW05-28	312.5	319.2	n/a	HWZ2
GW05-29	358.37	362.83	n/a	HWZ2

GW05-30	340.03	343.83	n/a	HWZ2
GW05-31	269	271	1.86	HWZ2
GW06-32	83.39	86.37	n/a	HWZ2
GW06-33	68.89	71.83	n/a	HWZ2
GW06-34	49.23	51.8	n/a	HWZ2
GW06-35	104.96	108.32	n/a	HWZ2
GW06-36	83.77	86.73	n/a	HWZ2
GW06-37	73.32	76.13	n/a	HWZ2
GW06-38	77.78	80.41	0.05	HWZ2
GW08-39	169.35	171.4	1.56	HWZ2
GW08-40	137.97	141.12	n/a	HWZ2
GW08-41	118.4	121	2.75	HWZ2
GW08-42	171.76	175.07	n/a	HWZ2
GW08-43	130.97	134.77	0.20	HWZ2
GW08-44	107.96	111.37	n/a	HWZ2
GW10-101	131.5	133.5	1.67	HWZ2
GW10-103	194.18	197.42	n/a	HWZ2
GW10-108	108.1	110.1	1.99	HWZ2
GW10-109	221.5	223.5	1.73	HWZ2
GW10-110	268.67	270.61	n/a	HWZ2
GW10-112	233.1	235.1	1.84	HWZ2
GW10-114	3.51	6.35	n/a	HWZ2
GW10-119	90.2	92.2	6.37	HWZ2
GW10-126	201.9	204.4	2.93	HWZ2
GW10-128	8.36	10.42	n/a	HWZ2
GW10-130	6.95	9.23	n/a	HWZ2
GW10-131	135.24	138.52	0.00	HWZ2
GW10-133	252.27	258.15	n/a	HWZ2
GW10-134	598.3	604.7	4.88	HWZ2
GW10-141	167.5	169.5	1.37	HWZ2
GW10-55	763.62	767.49	n/a	HWZ2
GW10-57	460.3	462.6	1.92	HWZ2
GW10-58	672.26	679.71	0.01	HWZ2
GW10-60	792	794	1.51	HWZ2
GW10-60WA	775	777	3.17	HWZ2
GW10-60WB	774.87	777.68	0.04	HWZ2
GW10-92	53	55	1.13	HWZ2
GW10-93	191.67	194.13	n/a	HWZ2
GW10-94	180	182	1.32	HWZ2
GW10-95	44	50	5.13	HWZ2
GW10-97	9.5	11.5	10.12	HWZ2

GW10-98	64	66	0.38	HWZ2
GW10-99	119	120	0.55	HWZ2
GW11-121	851	854	6.90	HWZ2
GW11-159	474.6	476.7	4.65	HWZ2
GW11-161	963	965	1.57	HWZ2
GW11-171	57	59	2.77	HWZ2
GW11-178	19.78	21.97	n/a	HWZ2
GW11-179	120.34	129.66	0.40	HWZ2
GW11-180	129	144.7	1.46	HWZ2
GW11-183	76	81	2.03	HWZ2
GW11-185B	384.26	386.47	n/a	HWZ2
GW11-187	420.16	424.56	4.17	HWZ2
T-91-3	302.13	306.64	n/a	HWZ2
T-91-5	361.78	368.29	0.02	HWZ2
75-12	26.49	31.92	n/a	HWZ3
88-17	239.1	241.1	1.51	HWZ3
88-21	453.4	455.4	7.20	HWZ3
88-4	75.78	81.13	n/a	HWZ3
89-GO-1	485.35	488.94	0.00	HWZ3
90-GO-5	537.45	541.74	1.34	HWZ3
GW04-09	188	190	5.45	HWZ3
GW04-10	167.2	169.2	3.58	HWZ3
GW04-11	113.5	117.5	6.77	HWZ3
GW04-15	207.73	212.77	n/a	HWZ3
GW04-21	213.94	218.55	n/a	HWZ3
GW04-25	294.8	296.8	1.69	HWZ3
GW05-24	266.46	270.41	n/a	HWZ3
GW05-27	266	268	6.35	HWZ3
GW05-28	292.35	302.22	1.80	HWZ3
GW05-29	332.5	348.5	n/a	HWZ3
GW05-30	296.54	300.91	n/a	HWZ3
GW05-31	209	211	1.28	HWZ3
GW10-101	110.4	118.1	3.62	HWZ3
GW10-110	234.94	239.15	n/a	HWZ3
GW10-112	219.64	224	0.01	HWZ3
GW10-134	564.42	569.85	0.01	HWZ3
GW10-145	37.67	41.8	n/a	HWZ3
GW10-55	740.84	747.35	n/a	HWZ3
GW10-57	424.7	426.2	2.79	HWZ3
GW10-58	627.71	632.11	0.01	HWZ3
GW10-59	493	495	1.62	HWZ3

GW10-60	746	770	1.00	HWZ3
GW10-60WA	755.5	757.5	8.76	HWZ3
GW10-60WB	771	773	1.61	HWZ3
GW10-78	612	614	2.91	HWZ3
GW10-94	165.6	169.86	n/a	HWZ3
GW11-121	831.26	842	2.73	HWZ3
GW11-150	141.96	145.88	n/a	HWZ3
GW11-159	447.9	452.5	9.53	HWZ3
GW11-176	26.03	30.65	0.03	HWZ3
GW11-180	123	125	1.66	HWZ3
GW11-185B	316	318	2.41	HWZ3
GW11-187	399	406	2.38	HWZ3
T-91-2	175.53	178.66	0.00	HWZ3
T-91-3	270.49	275.95	0.01	HWZ3
T-91-5	338.17	342.66	0.31	HWZ3