TECHNICAL REPORT
Magnetite Mineral Resource Estimate – Bronson Slope Deposit

For

SKYLINE GOLD CORPORATION
Vancouver, BC

On
THE BRONSON SLOPE PROPERTY

NORTHWESTERN BRITISH COLUMBIA
CANADA

NTS Map Sheets 104B 11E, Trim 104B 065, NAD 27
Latitude 56 ° 40 ′ 00” North,
Longitude 131° 05’ 33” West

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January 28, 2010

TABLE OF CONTENTS

TABLES **Page**

FIGURES

SECTIONS **Following Page 35**

APPENDICES **Following Page**

1.0 Summary

The Bronson Slope Property, hosting a porphyry gold-copper-silver-molybdenum deposit, is located in Northwestern British Columbia 110 km northwest of Stewart, B.C., 280 km northwest of Terrace, B.C., and 80 km east of Wrangell, Alaska. Skyline Gold Corporation ("Skyline") completed extensive exploration and drilling on Bronson Slope during the period 1988 through 1997. During that period, they carried out prospecting, geochemical soil surveys, geological mapping, induced polarization surveys, property grids and surveying, and surface core drilling, followed by metallurgical, engineering scoping, pre-feasibility, and economic evaluation studies. In 2006 and 2007 Skyline completed further drilling, resource estimates and mine development

During 2009 and early 2010 core sampling of historical and 2006/2007 core, analyses for magnetite, and a magnetite resource estimate was completed. The quality of the Skyline exploration work is considered to be of good quality and meets industry standards.

The property consists of 12 Mineral Claim Tenures and 6 Crown Granted Mineral Claims as illustrated in **Figure 4-3** and is located in the Liard Mining Division. Four of the mineral tenures are under option and 17 mineral tenures and 6 crown granted claims are owned 100% by Skyline.

The Bronson Slope Property is underlain by the Early Jurassic Red Bluff porphyry gold-copper-silver-molybdenum hydrothermal system that is dominated by an intense quartz-magnetite-hematite stock work that trends northwest along the south side of Bronson Creek valley. The Red Bluff porphyry is intrusive into Upper Triassic age feldspathic greywacke. The stock work overprints and is intimately associated with the Red Bluff porphyry intrusion. The stock work is composed of an intense network of veins. Drill intersections of 20 to +100 metres long are composed entirely of intersecting to sheeted sets of quartz-magnetite-hematite veins. Individual veins range from 0.5 to 10 cm in thickness. The quartz-magnetite-hematite stock work is overprinted by quartz + pyrite + chalcopyrite +/- carbonate veins and by carbonate and pyrite veins. The total sulphide content in the quartz-pyrite assemblage is around 5%. The quartz-pyrite assemblage comprises less than 10% of the older quartz-magnetite-hematite veins. The quartz-pyrite veins/alteration are locally brecciated.

The Bronson Slope Property has been mostly explored by surface core drilling where a total of 92 drill holes totalling 19,320 metres have been drilled in 1965, 1986, 1988, 1993 to 1997, 2006, and 2007. Most of the drilling occurred between 1993 and 1997. This drilling has defined a mineralized porphyry gold-silver-copper-molybdenum system in the order of 1.5 km long and 0.4 to 0.6 km wide.

During October 2009 Skyline, using a 7 person sampling team, sampled 5923 meters of historical and 2006/2007 drill core for parts of the Bronson Slope deposit and sent the respective samples to Met-Solve Laboratories in Burnaby, BC for magnetite analyses. On the basis of these analyses a magnetite resource has been determined for the Bronson Slope deposit. The magnetite portion within the larger gold-silver-copper-molybdenum deposit is about 700 meters long and up to 400 meters wide.

During 2008, Burgoyne and Giroux (2008) completed a resource estimate of the Bronson Slope deposit, based on block modeling and kriging and this can be found on www.sedar.com. The Case 2 resource estimate is presented below and is based on metal prices of $2.00/lb Cu, $650/oz Au, $10/oz Ag, and $12/lb Mo.

The metal prices were used along with block based metallurgical recoveries to determine individual block values. The mineral resources presented in the tables below were then determined based on a cut off of US $9.00 per tonne net recoverable value.

Case 2 - 2008 Bronson Slope Resource Estimate

Category	Metric Tonnes	Au g/t	Ag g/t	Cu %	Mo %
Measured	74,800,000	0.45	2.45	0.17	0.0059
Indicated	150,300,000	0.31	2.38	0.13	0.0087
Total Measured & Indicated	225,100,000	0.36	2.22	0.14	0.0077
Inferred	91,600,000	0.27	1.76	0.13	0.0080

Subsequent to this above resource estimate Skyline Gold had Leighton Asia (Lawrence and Seen, 2009) complete a Preliminary Economic Assessment on the deposit that yielded a potential economic rate of return, which is discussed in detail in **Item 18**. This study gave several recommendations to enhance the economics of the property, one of which was, the estimation of a magnetite resource.

The current mineral resource for magnetite mineralization has been estimated for the Bronson Slope deposit that meets CIMM resource standards and classifications. Blocks were classified during the resource estimation for Au and Cu completed in Burgoyne and Giroux (2008). The tonnage was established for each block during this estimation. For the magnetite estimation the block classifications and tonnages were taken from the 2008 block model. The resource estimate, based on block modelling and kriging is considered reliable and relevant. The current magnetite mineral resource is given below. The resource was estimated for contained magnetite at a series of magnetite cut-offs varying from 1% to 10% which are detailed inn **Tables 17-5** through **17-8**. A summary of the measured plus indicated and inferred resource for different cut-offs is given below. No metallurgical recoveries have been applied to the resource.

TABLE 1-1
2010 MEASURED PLUS INDICATED MAGNETITE GLOBAL RESOURCE

Magnetite Cut-Off Weight %	Tonnes > Cut-off (tonnes)	Grade > Cut-off Magnetite (%)	Contained Tonnes Magnetite
1.00	179,960,000	6.74	12,130,000
2.00	163,160,000	7.28	11,880,000
3.00	151,400,000	7.66	11,600,000
4.00	143,170,000	7.90	11,310,000
5.00	131,840,000	8.19	10,800,000
6.00	118,220,000	8.50	10,050,000
7.00	100,640,000	8.84	8,900,000
8.00	72,680,000	9.34	6,790,000
9.00	42,880,000	9.92	4,250,000
10.00	15,960,000	10.73	1,710,000

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TABLE 1-2
2010 INFERRED MAGNETITE GLOBAL RESOURCE

Magnetite Cut-off Weight %	Tonnes > Cut-off (tonnes)	Grade > Cut-off Magnetite (%)	Contained Tonnes Magnetite
1.00	13,040,000	4.01	520,000
2.00	6,300,000	6.92	440,000
3.00	5,710,000	7.38	420,000
4.00	5,320,000	7.66	410,000
5.00	4,980,000	7.88	390,000
6.00	4,390,000	8.21	360,000
7.00	3,500,000	8.60	300,000
8.00	2,510,000	9.00	230,000
9.00	1,110,000	9.58	110,000
10.00	240,000	10.40	20,000

The 2% magnetite cut off highlighted in the above tables and used as a base case for resource estimation is based on by-product milling and truck transportation cost information supplied by Skyline Gold. This is balanced against what is believed to be projected conservative sale price of $130 per tonne after milling and transportation charges. This price is based upon western Canada magnetite market analysis (Appendix D), as well as discussions with Craigmont Mines that produces magnetite powder for dense media separation coal cleaning. The estimated beak-even cut –off grade is less than 2% on a by-product basis. The actual breakeven percent cut off is in the order of 1.5%. It must be stressed that the economics are also dependent on the ability to market and sell magnetite.

It should be noted that when this global magnetite resource is compared to the preliminary open pit designed for the Preliminary Economic Assessment completed by Leighton Asia (Lawrence and Seen, 2009) in March 2009 that 44% of the measured and indicated magnetite tonnage, above a 2% cut-off, is within the pit. The remainder sits below and to the west. As a result it is our recommendation that a new PEA be completed using the magnetite results to demonstrate the changes in project economics along with magnetite marketing considerations.

Skyline Gold's internal studies (Jensen, 2010b) indicate that a 7% weight magnetite cut-off based on the 2009 Bronson slope PEA (Lawrence and Seen 2009) and the 2008 magnetite study (Klein 2008) is potentially viable on a stand-alone production basis and assuming that magnetite is the only mineral produced at Bronson Slope. At this cut-off Bronson Slope Measured and Indicated magnetite resource is 100,640,000 tonnes grading 8.8% magnetite for a total Measured and Indicated estimate of 8,900,000 tonnes of contained magnetite. It is reasonably expected that, on a by-product production basis, the magnetite economic cut-off grade would be lower and the magnetite resource estimate at lower cut-off grades is shown in the above tables.

Klein (2008) completed metallurgical testing from bulk magnetite samples obtained from drill core from the Quartz Magnetite Unit of the Bronson Slope deposit. The testing confirmed the metallurgical process, determined the grinding work index for regrinding and characterize the magnetite product with respect to the specifications. The testing involved grinding and flotation to recover copper sulphides. The flotation tailings were for magnetic separation testing.

Skyline also performed a series of metallurgical test studies on Bronson Slope drill core samples between 1994 -1997 and in 2007-2008 as part of engineering and development pre feasibility studies. These metallurgical studies gave average recoveries of 84% for gold, 86.8% for copper, 67.4 % for silver and 46.5 % for molybdenum.

Skyline completed a significant amount of engineering scoping, environmental, cash flow, capital and operating costs, geotechnical, infrastructure and access, and other pre-feasibility studies on the Bronson slope deposit from 1995 through 1997 and in 2007 through 2009.

Future work on Bronson Slope deposit, should focus on project and mine development. The following recommendations are warranted and include:

- A revised preliminary economic assessment report, as noted above, including a review and revision of the open pit design model, that includes the evaluation of the magnetite resource, should be completed; this will determine what amount of magnetite can be included in a revised preliminary open pit design along with magnetite marketing considerations.
- Further metallurgical work should be completed on the magnetite mineralization to define metallurgical recoveries in the different rock units.
- Continuation of mine development studies recommended by the gap study currently being undertaken by SRK.
- Depending on the gap analysis study results by SRK, initiate a Pre-Feasibility or Feasibility Study. Such study to include magnetite and molybdenum recovery;
- Implement project changes requested on Environmental Assessment (EA) permitting process by BC EAO on previously submitted project description and advance EA process with BC EAO and CEAA.
- Negotiate a Participation Agreement with the Tahltan Band and Iskut First Nation;
- Prepare a Feasibility Study for Skyline Gold's local hydro license applications for self-generation hydropower for the Bronson Slope project.

2.0 Introduction & Terms of Reference

Burgoyne Geological Inc., Arnd Burgert Consulting Ltd. and Giroux Consultants Ltd. were commissioned by Skyline Gold Corporation ("Skyline") to complete a Technical Evaluation Report, including a Mineral Resource Estimate on the magnetite mineral content of the Bronson Slope copper-gold-silver-molybdenum property in northwestern British Columbia.

Cominco initially explored this project in 1965 and later, in 1988 and 1993 through 1997 by Skyline Gold Corporation who, in turn, spent approximately $3.5 million in 2006 dollars (with an equivalent amount also spent on development studies) and defined an historical mineral resource. Approximately $1.5 million was spent in 2006 and $3.7 million in 2007 on core drilling. A current gold-silver-copper-molybdenum mineral resource is defined. A Preliminary Economic Assessment report was completed in March 2009, by Leighton Asia.

During October 2009 Skyline, using a 7 person sampling team, sampled 5923 meters of historical and 2006/2007 drill core for parts of the Bronson slope deposit and sent the respective samples to Met-Solve Laboratories in Burnaby, BC for magnetite analyses. On the basis of these analyses a magnetite resource has been determined for the Bronson Slope deposit. Approximately $235,000 was spent on this program. Also, separate from the core-sampling program, Skyline completed during October 2009 a two hole, 729 meter drilling program on the Snip-1 Mineral Tenure some 900 meters east of the Bronson Slope deposit, costing in the order of $250,000.

This Technical report is the result of the review and evaluation of a large library and database of technical information on exploration, drilling resource estimates, metallurgy, historical mine development including pre feasibility studies, and the Leighton Asia 2009 report. This Technical Report will be used by Skyline in satisfying reporting requirements for the appropriate regulatory authorities including the British Columbia Securities Commission. Skyline owns a 100% interest in the Bronson Slope Property consisting of 6 crown granted mineral claims and 17 mineral tenures; Skyline also has a further 4 mineral tenures under option.

To accomplish this assignment, the writers had discussions with Mr. David Jensen, P.Eng. President of Skyline and Dr. Bern Klein of BC Mining Research Ltd. and Mr. Ish Grewal P.Eng. of Met-Solve Laboratories Inc. with respect to metallurgical studies, recoveries and analytical methods to determine magnetite. Burgoyne conducted a property site visit during the period of October 1 and 3, 2009. Mr. Arnd Burgert was on-site Project Geologist and was at the Bronson Camp for the full duration of fieldwork from October 1 to 21, 2009. Office and site work included review of technical reports and maps, resource models of cross sections, tonnage and grade block models and spreadsheet compilation and checking. Map and figure preparations and report writing was undertaken during October 2009 through January 2010. Drill core from the 1986 and 1994 through 1997 and 2006, and 2007 programs is located at the Bronson Airstrip. Drill core from the 1988 and 1993 campaigns is no longer available having been lost on collapse of drill core sheds due to snow load in the winter of 2000-2001. Also 5 holes from the 1996 drill program are missing.

The detailed technical review of the large exploration and drilling database by the writers form the basis for this Technical Report. **Note Item 21**. The more important technical references are Burgoyne and Giroux (2008 and 2007), Lawrence and Seen (2009), Rhys (1995a), Rhys (1995b), Yeager (1997b). All currency values are expressed in Canadian dollars unless otherwise indicated. Magnetite analyses (% magnetite) were determined by the Davis Tube method.

Mr. Burgoyne prepared **Items 2** through **10, 15, 16, 18 and 21.** Mr. Burgert prepared **Items 11** through **14**. Mr. Giroux prepared **Item 17**. **Items 1, 19** and **20** were jointly prepared.

3.0 Reliance On Other Experts

An informal review of mineral title and ownership of the Bronson Slope property was completed; however, there has been no formal legal mineral title and ownership review as this is outside the expertise of the writers. The **Item 4.0 Property Description** information was obtained from Skyline and through checking the records of the Mineral Title Branch, Ministry of Mines and Energy for British Columbia. The writers disclaim responsibility for such information in this **Item 4.0.** The information on environmental liability in **Item 4.0** was determined from discussions with Skyline personnel and the site visits.

This report is based on an extensive technical review and discussion of information that was available. This report is believed to be correct at the time of preparation. It is believed that the information contained herein will be reliable under the conditions and subject to the limitations herein.

4.0 Property Description & Location

4.1 Bronson Slope Mineral Claims & Crown Grants

The Property is located in northwestern British Columbia. It is centred on 131°05' West Longitude and 56°40' North Latitude on National Topographic Series map sheet 104B 11/E (also BC Trim Map104B 065). The Property is 110 km northwest of Stewart, B.C., 280 km northwest of Terrace, B.C., 80 km east of Wrangell, Alaska and 70 km west of Bob Quinn airstrip on the Stewart-Cassiar Highway. A mine access road leads from Bob Quinn 40 km down the south side of Iskut River to within 30 km of Bronson Slope where it turns south to the Eskay Creek gold-silver mine of Barrick Gold. **Note Figures 4-1** and **4-2**.

The property consists of 17 Mineral Claim Tenures and 6 Crown Granted Mineral Claims as illustrated in **Figure 4-3** and located in the Liard Mining Division. Four of the mineral tenures are under option and 8 mineral tenures and 6 crown granted claims are owned 100% by Skyline. The claims are located in NTS 104B 11/E. The Crown Granted claims portion of the Property has been legally surveyed. The known Bronson Slope Au-Cu-Ag-Mo deposit with respect to property boundaries is presented in **Figures 4-3.** The Bronson Slope Property is located on the north side of the large Iskut Property (Richards 2005) also owned by Skyline. Skyline in April 2006 (Skyline 2006) closed a "farm-out" of their Iskut River Property to Spirit Bear Minerals Ltd. but this agreement has apparently lapsed.

The Bronson Slope property mineral claim tenure and Crown Granted Mineral Claims names along with claim numbers; expiry date are set out in **Table 4-1**. All of the mineral tenures are have been staked and registered with MTO (Mineral Titles Online) for the province of BC. These are electronic claims based on coordinates for the cells in UTM NAD 83 format**. Mineral tenure areas provided in Table 4-1, as noted below, are those obtained from the British Columbia Government, Minerals Online Title Viewer and remain to be confirmed through a detailed mineral title review. The actual areas of the tenures, where they are staked over underlying claims, are less than those reported and the exact area(s) must be confirmed through a title review. The solid colours on Figure 4-3 are actual claim areas owned/controlled by Skyline. The Bronson Slope tenures/areas and property outline in Figure 4-3 was provided by Skyline.**

In 1996 Skyline entered into an agreement with Prime Resources Group Inc. to acquire Prime's claims immediately between the Skyline Crown Grants Red Bird, Red Bluff, and Homestake on the north and El Oro on the south. This transaction was achieved in two stages – a claim swap for the Kathleen Fraction between Red Bird and Red Bluff Crown Grants and a purchase agreement for the Highwall claims located south of the Red Bird, Red bluff and Homestake Crown Grants. In return Skyline (Yeager 2006) granted a 3.5% Net Smelter Return payable to Cominco/Prime from any production obtained on the Highwall claims only. This NSR interest is purchasable by Skyline for $500,000 (Yeager 2006). Mineral Tenure 517754 now covers the Highwall and Kathleen claims.

In December 2008 the Snip 1 and Bronson Slope Fraction mineral tenures (Skyline Gold Press Release December 4, 2008) were acquired as to a 100% ownership from St. Andrews Goldfields by cash payment. In February 2009 the Snipped mineral tenure was acquired through Mineral Title online staking.

In November 2009 the Chopin I, II and Handel and Ravel mineral tenures (Skyline Gold Press Release of November 19, 2009) were acquired through the following acquisition terms:

TABLE 4-1
BRONSON SLOPE PROPERTY MINERAL TENURE

Claim Name	Tenure Number	Expiry Date	Area Hc		Claim Name	Tenure Number	Expiry Date	Area Hc
Bronson 2	517754	Dec. 31, 2010	106.7**		Snippaker-1	705126	Feb. 1, 2011	444.2**
Bronson	517750	Dec. 31, 2015	409.1**		Gold Country	705127	Feb. 1, 2011	444.2**
Snip 1	523348	March 01, 2020	285.0**		Final Approach	705128	Feb. 1, 2011	444.1**
Katyadd	523932	Dec. 31, 2010	17.8**		Descent	705130	Feb. 1, 2011	301.9**
Cgadd	523933	Dec. 31, 2010	17.8**		Block	705133	Feb. 1, 2011	17.8**
Bronson Slope Fr.	552657	March 01, 2011	17.8**		Chopin I	222135	Oct. 19, 2011	500.0**
Snipped	598751	Feb. 05, 2011	160.1**		Chopin II	222136	Oct.19, 2011	300.0**
Ravel	221997	Oct. 19, 2013	500.0**		River	572338	Dec. 21, 2010	177.6**
Handel	221996	Oct. 19, 2013	500.0**					

Crown Grants	Lot Number	Taxes Due Date	Area Hc
Red Bluff	2857	July 2, 2010	20.85*
Homestake	2858	July 2, 2010	17.09*
Red Bird	2859	July 2, 2010	17.94*
Mermaid	2860	July 2, 2010	19.31*
El Oro	2862	July 2, 2010	20.87*
Golden Pheasant	2864	July 2, 2010	18.01*
Silver King	2863	July 2, 2010	18.95*
Brown Bear	2865	July 2, 2010	20.36*
Iskoot	2866	July 2, 2010	19.39*
Silver Dollar	2867	July 2, 2010	18.95*
Marguerite	2868	July 2, 2010	19.39*
Blue Grouse	2869	July 2, 2010	20.46*
Copper Queen	2870	July 2, 2010	20.34*

**From British Columbia Government Minerals Online Title Review & subject to confirmation by legal mineral title review

* Estimated area of surveyed crown grant

- An initial payment of $50,000 was made with a required further expenditure of $50,000 in geophysical work on the property by November 2010.
- Payment of a final $500,000 by November 17, 2011. The Company may at any time complete the purchase by making full and final payment of $575,000 cash or $500,000 cash plus 300,000 skyline shares, at the option of the vendor.
- Payment of either $75,000 or delivery of 300,000 Skyline shares to the vendor by November 17, 2010 with choice of cash payment or Skyline shares at the option of the vendor.

The most recent mineral tenures, acquired by Mineral Title Online staking, include 705126, 705127, 705128, 705130 and 705133.

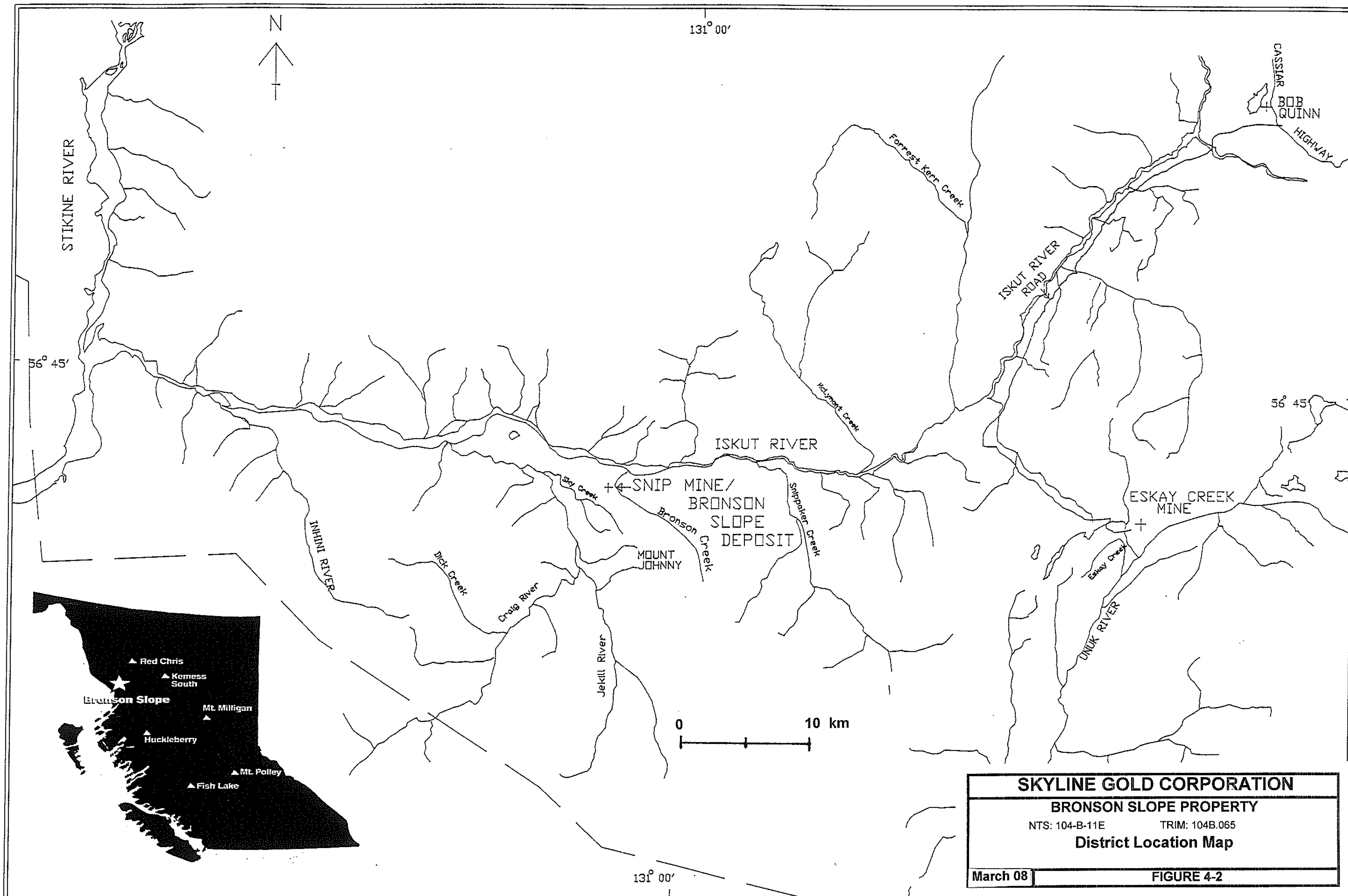
All proposed exploration work in the Province of British Columbia must receive prior approval by issuance of a work permit by the Ministry of Energy and Mines. Such approval is routinely given and will be obtained with no difficulty in the areas to be explored subject to normal reclamation and environmental guidelines. The Mines Permit MX-1-46, approval number 08-0101255-0822 was issued by the BC Department of Mines to complete mineral exploration in 2009. Under the terms of the agreement the Mines Permit, Skyline is responsible for all remediation and reclamation work resulting from exploration and drilling programs where trees were cut in order to construct drill pads. All proposed exploration work in the Province of British Columbia must receive prior approval by issuance of a work permit by the Ministry of Energy and Mines. Such approval is routinely given and will be obtained with no difficulty in the areas to be explored subject to normal reclamation and environmental guidelines. Cost of holding title to ground held by mineral cell claims for the first three years after registration is $4.00/hectare of exploration work plus a $0.40/hectare fee; in subsequent years the cost is $8.00 per hectare plus a fee. Crown granted mineral claims are assessed for taxes on May 1 of every year with notices sent to registered owners in May and taxes due July 2 in the given year.

4.2 Environmental Issues

The authors are not aware of any environmental issues or liabilities that affect the property and has been informed by Skyline that they are not aware of any environmental problems. At the present time, the infrastructure development at the Bronson Slope property is limited to that adjacent, but not on the Property, airstrip and buildings at the Bronson airstrip, the Johnny Mountain airstrip and a network of tote roads. There are several wooden drilling platforms on the side of Bronson Creek Valley some of which may be used as helicopter landing pads. Previous camps were located off of the Property.

There are rusty coloured seeps in the Bronson Creek valley, which are no doubt emanating from iron sulphide mineralization in the Bronson Slope deposit and these seeps are natural in origin.

140°0'0"W
120°0'0"W
140°0'0"W
N
E
S
W
Bronson Slope Property
Stewart
Terrace
Smithers
Prince George
Williams Lake
50°0'0"N
Revelstoke
Merritt
Courtenay
Vancouver
Penticton
Nelson
Abbotsford
Victoria
50°0'0"N
180°0'0"
160°0'0"W
60°0'0"W
20°0'0"W
Inuvik
Whitehorse
Yellowknife
Iqaluit
Bronson Slope Property
50°0'0"N
Edmonton
Vancouver
Calgary
Regina
Saskatoon
Winnipeg
Sudbury
Ottawa
Québec
Halifax
Toronto
100°0'0"W
80°0'0"W
SKYLINE GOLD CORPORATION
Property Location in British Columbia
Title:
BRONSON SLOPE PROPERTY
Scale: As Shown
Design:
Figure: 4-1
Date: Mar, 2008
Drawing: TERRACAD LTD.
Rev: 1.0



SKYLINE GOLD CORPORATION

BRONSON SLOPE PROPERTY

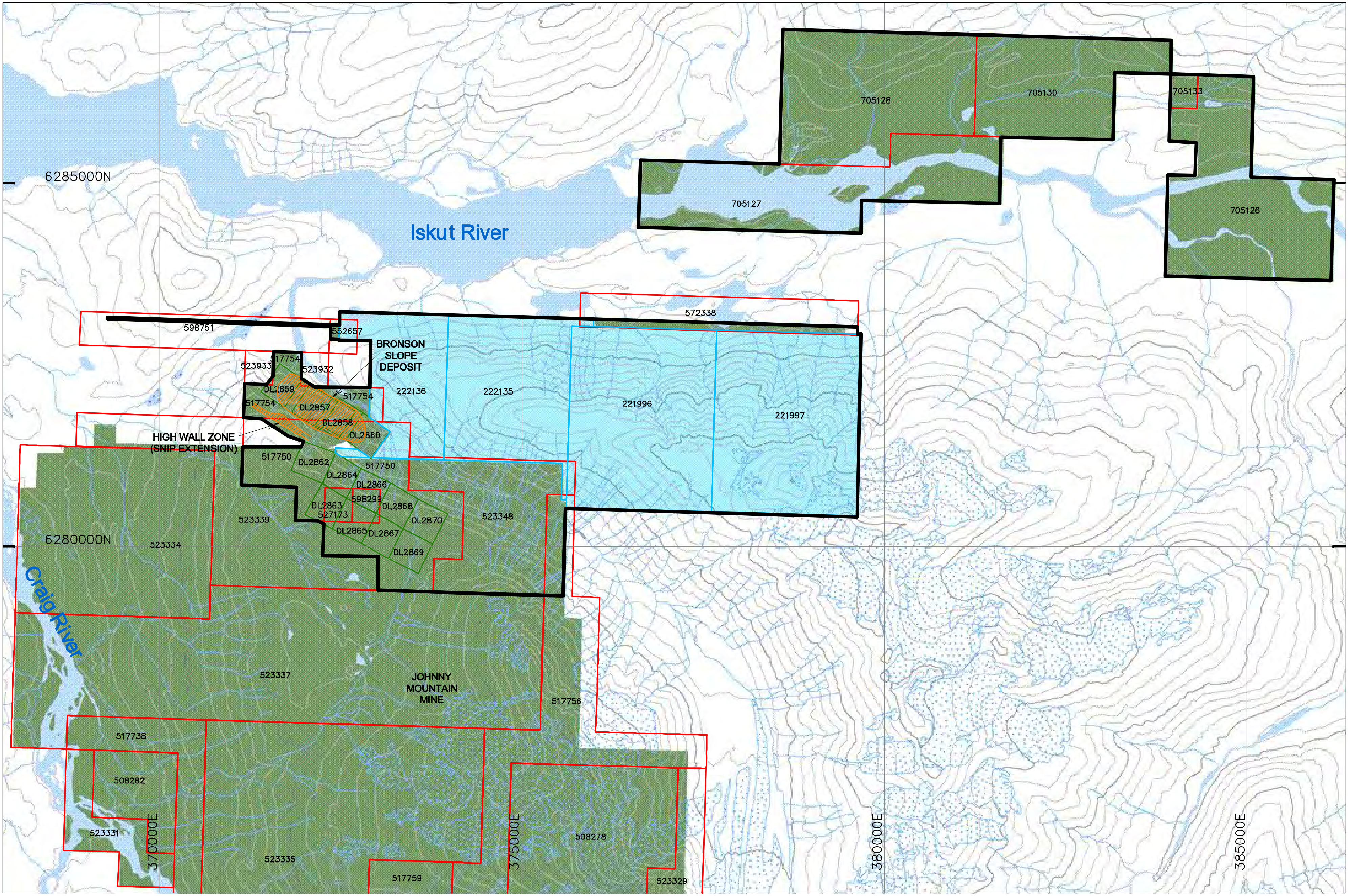
NTS: 104-B-11E TRIM: 104B.065

District Location Map

March 08 | FIGURE 4-2

pitlnee.pf

SURPAC SOFTWARE INTERNATIONAL, AUSTRALIA



Legend

- Skyline Gold Crown Grant Boundary
- Skyline Gold Claim Boundary
- November 2009 Claims Acquisition
- Skyline Gold: 100%

N

BRONSON SLOPE PROPERTY

PROPERTY BOUNDARY SHOWN IS SUBJECT TO DETAILED MINERAL TITLES REVIEW

0 500 1000 1500 2000m

SKYLINE GOLD CORP.

BRONSON SLOPE PROPERTY AND OTHER SKYLINE MINERAL TENURE

MINERAL TENURE

FEB 10	AB	FIG. 4-3

5.0 Accessibility, Infrastructure, Power, Climate, Physiography, Flora & Fauna

Item 5.5 is taken from the Preliminary Economic Assessment (PEA) report of Lawrence and Seen (2009). Here, an in depth discussion is also given for consideration of future mine production for topics including water use, tailings storage, mine waste disposal, process plant site and mining personnel. The reader is referred to the PEA for detailed mining considerations for accessibility, infrastructure, and local resources.

5.1 Access & Infrastructure

The property consists of 12 Mineral Tenures and 6 Crown Granted Mineral Claims in the Liard Mining Division of British Columbia. The property lies within the metallogenetically important Stewart-Iskut River area, northwestern British Columbia. It lies on NTS map sheet 104B 11/E (also 104B065) at 56° 40’ North Latitude and 131° 05’ West Longitude and 70 km west of Bob Quinn airstrip on the Stewart-Cassiar Highway.

The Bronson Slope property is 110 km northwest of Stewart, B.C and 70 km west of Bob Quinn airstrip on the Stewart - Cassiar Highway. The existing 40 km of road access to site is comprised first of a Forest Service Road leading from Bob Quinn Lake to the former producing Eskay Creek gold-silver mine turnoff and is under Road Use Permit to Barrick Gold. This 35 km segment is followed by a segment of approximately 5 km. long operated under a License of Occupation by AltaGas for its Forrest Kerr hydroelectric project. A mutual road sharing agreement will be required between SGC and Alta gas to maintain the road. The proposed access road location along the south side of the Iskut River, as outlined in **Item 5.2**, will be about 30 km in length. The road is a single lane “forest industry style” gravel road. Note **Figure 4-2**.

The property lies south of Bronson Creek and southeast of the Bronson airstrip and the former producing Snip gold mine on the south bank of the Iskut River. To the south the property covers glaciers and mountainous terrain including Johnny Mountain. The north property boundary lies 500 m immediately south of the closed Snip Mine just south of the Iskut River.

Two airstrips suitable for Hercules aircraft or equivalent service the Property. One occurs at 100m elevation at Bronson Airstrip, which is the old campsite of the closed Snip Gold Mine just north of the property. In October 2008 Skyline Gold announced receipt of the assignment by Barrick Gold of the Bronson Airstrip License of occupation (Skyline Gold Press Release October 16, 2008). The License is for 39 hectares of land covering an area of 1780 m by 220 m which is capable of serving C-130 Hercules cargo aircraft. The airstrip license is BC License No. 635844 and expires on October 1, 2018.

The second airstrip occurs in the alpine at 1100m elevation at the closed Johnny Mountain Gold Mine in the centre of the adjoining Iskut property. In recent years helicopters working for the mineral exploration industry out of Bob Quinn airstrip have been available for work in the area.

Access to the Property can be made from Smithers, B.C., Terrace, B.C., or Wrangell, Alaska to the airstrips mentioned above at the mine sites. Alternatively vehicles can be driven to Bob Quinn to co-ordinate access by helicopter when they are available. A 10 km road connects the two airstrips through the centre of the Iskut property thereby providing vehicle access to the south part of Bronson Slope. Old drill roads lead north and northwest from the Johnny Mountain airstrip and could be rehabilitated if warranted. The 10 km road referred to requires yearly maintenance. A dozer equipped tractor crawler, owned by Skyline, is available at Bronson Airstrip for this purpose.

A seasonal camp, catering to the mining industry, is operated at the Bronson Slope airstrip beside the Iskut River. The exploration field season is from late May through to early October.

5.2 Proposed Mine Access Road From Forest Kerr to Bronson Slope Property

Skyline Gold submitted a Special Use Permit ("SUP") application for an access road to the B.C, ministry of Forest and Range on May 12, 2008 (Skyline Gold Press Release May 6, 2008). The SUP access road will require construction of a 28 km road extension from AltaGas's Forest Kerr access road which itself extends from the Eskay Creek Mine's access road.

The following is a summary based on the reports prepared by Forsite (2006 and 2008). This proposal is for a permanent mine access road for the Bronson Slope Property if the project was to go into construction and operation. The proposed permanent road access to the project can be divided into two main sections. The first section is the relatively flat road on old lava beds. The second section starts at the end of the lava flats east of Bug Lake and continues to the Bronson Creek crossing and the airstrip.

The first section consists of approximately 24 km of road and four proposed bridge crossings. It starts at the west end of the existing built Forest Kerr power project access road and continues west to the end of the lava flats below the Bug Lake area.

The second section of proposed road starts at the end of the lava flats east of Bug Lake and continues to the Bronson Creek crossing and the airstrip. It is characterized by steeper side slopes and rock that will require drilling and blasting. It includes bridge crossings over Bronson Creek and tributaries of the Bug, Middle, and Triangle Lakes.

Bronson Creek is consistently wide and would require structures over 90m for a crossing. The chosen location is at the top of the alluvial fan at the Iskut River. A budgetary quote of $7.6 million including costs for supervision, survey, mechanical repair, fuel, travel, camp, office, safety and project support. The expected time to complete the construction of the road excluding the bridges is 6 months.

5.3 Power

It is assumed that power will be supplied from a proposed Northern Transmission Line (NTL) main grid line located at Bob Quinn Lake (approximately 60km from site). An opportunity exists for a direct connection to the BC Hydro grid near the proposed Forrest Kerr hydro power station, which is much closer to site (approximately 25km from site). Other alternative electricity generation and supply options are also being evaluated including self-generation of power using hydro assets for which Skyline Gold have submitted hydro generation license applications and for which Skyline Gold has received Notice of Sufficiency of Application from the BC government. For the purpose of this report it is assumed power will be supplied using a 138kV transmission line, which will run partially within the Access Road right of way. Up to 20MW of power will be provided from the Forest Kerr run-of-river hydroelectric power station, located 25km west of the Bronson Slope property.

Initially the BC Government had plans to extend the Northwest Transmission Line (NTL) from Terrace to Bob Quinn. This was going to be completed in two stages This was going to be completed in two stages with the first completed in 2009 providing 138kV and the second stage completed in 2011 increasing the line voltage to 287kV. However a delay has been announced by the EMPR due to the Galore Creek Project ceasing construction. In November 2008 the BC government announced that the environmental process was being restarted and that the Canadian federal government announced $130 million of funding support for the NTL. In December 2009 the federal government announced that it was delegating the NTL environmental assessment review to the Province of British Columbia. Skyline Gold is currently investigating alternative sources of power supply. The options include obtaining power from Alaska where there is adequate capacity and relatively low infrastructure requirements or local generation of electricity from coal, coal gas or hydro.

In addition to these options Skyline Gold has announced completion of the first stage of three water license applications on 7 water catchments (Skyline Gold Press Releases of April 12 and August 1, 2008). Skyline announced on August 12, 2008 that it had received “Notice of Sufficiency of Application” from the BC Government for all 7 of its proposed hydro licenses and that it was “first in line” as applicant for 6 of the 7 licenses. Preliminary indications are that hydro electricity, if augmented by water storage on Snippaker and Bronson Creek, will supply 25 MW or power required by the Bronson Slope Project.

5.4 Physiography

The Property is located on the south side of Bronson Creek Valley. The terrain is rugged with the range in elevation between the valley of Bronson Creek (about 120 metres) and the plateau of Johnny Flats above Bronson Creek is about 1000 metres. Below tree line, topography is moderate to steep. In the district area glaciers are common and extend to low elevations (400 to 800 metres) in the valleys.

Major valleys are densely vegetated with thick grass, brush and smaller trees. Peaks are barren and alpine in nature. Much of the area consists of sparse outcrops.

5.5 Climate

Climate in the area is typical for this portion of British Columbia – cool summers and cold winters. Although Pacific weather disturbances greatly influence the weather patterns at the site, temperatures are generally cooler than those of the northern coastal climate. The nearest weather monitoring station was located at Bronson Creek and was in operation until 1999. Data recorded from 1994 to 1998 (Lawrence and Seen 2009) shows the annual precipitation ranged between 2100 and 1300 mm. Approximately 30% of all precipitation fell as snow. Precipitation levels were highest in September and October and lowest in May through August.

TABLE 5-1

CLIMATIC DATA

Year	Total Precipitation (mm)	Total Snow (mm equiv.)	Mean T (C)	Extreme Min T (C)	Extreme Max T (C)
1998	1300.5	212.7	4.7	-26	31
1997	1572.7	298.8	5.2	-32	28
1996	1378.1	446.6	3.2	-33	29
1995	1286.9	401.8	4.9	-31	29
1994	2110.5	799.8	4.5	-23	30

Mean daily temperatures were highest in July and August reaching approximately 16 ^{o}C, and lowest in January falling to 15 ^{o}C. The highest temperature recorded on site over the 5-year period was -31 ^{o}C and the lowest temperature recorded was 32 ^{o}C. A summary of the climate data recorded at the Bronson creek location is included below in **Table 5-1**.

5.6 Flora and Fauna

The area is generally thickly vegetated with a forest of mountain hemlock and Sitka spruce. Steeper slopes and gullies are commonly covered with thickets of slide alder and devils club, which make traversing extremely difficult. On the Johnny Mountain plateau (Woznow and Yeager, 1999) within the Alpine Tundra Zone there is variety that is attributable to microenvironments primarily based on moisture conditions. The dominant species are Alaskan Moss Heather and Cream Mountain Heather, which comprise approximately 85% of the vegetative cover in the vicinity of Johnny Mountain.

Wildlife in the area is limited in its number of resident species due to the relatively exposed conditions that prevail on the Johnny Mountain plateau. Hoary marmots were the most prevalent species observed in the baseline studies. Marten, weasel, pack rat, deer mouse and northern red-backed voles are other species observed or expected to be present at the Johnny Mountain site prior to operations. Pre-existing hoary marmot colonies remained intact during operations despite extremely close proximity to heavy vehicular traffic. Marten presently inhabit the unused buildings, no doubt enjoying an abundant harvest of small rodents.

Large mammals comprising mountain goat, wolf, grizzly bear and black bear have all been observed directly or indirectly. These are all considered transient, however, as no sign of residency was observed.

Mountain goats have been observed on the side slopes of Johnny Mountain. Geologists on traverse on the flanks of Johnny Mountain have, on rare occasions, sighted individual or small groups of mountain goats. These goats were thought to be transient members of a known group normally resident on Snippaker Ridge, located on the northeast side of the Bronson Creek valley, or possibly members of groups normally resident in the mountain ranges further to the south of Johnny Mountain.

Grizzly bears and black bears were observed annually at the adjacent Johnny Mountain mine site during past mining operations but due to daily incineration of garbage and a ban on the casual discharge of firearms, there were no adverse effects on bears or humans. A small number (approximately ten) of black and grizzly bear encounters with exploration workers on remote parts of Skyline’s surrounding exploration property during the period 1987 to 1990 resulted in the bears being warned off by loud noise making devices or capsicum sprays.

Local bird species observed pre-development include white-tailed ptarmigan, ruffed grouse, raven, sparrow and golden eagle. These species remained resident at the site during operations and remain so at present. Raven and sea gull populations increased markedly during operations but quickly returned to normal levels when operations ceased. It is stated that approximately 55 species of songbirds possibly frequent the Johnny Mountain mine site

6.0 History

6.1 Summary

Skyline personnel have worked on the Property since 1988 and it was during a 1992 review of all exploration and drilling data by Burgoyne (1992) that the alteration and then defined mineralization indicated the potential for a large low-grade porphyry copper-gold deposit. In 1993 Skyline performed Induced Polarization and Chargeability surveys as noted by Burgoyne (1993a) and a limited drilling program of 872 metres over 7 drill holes on two separate cross-sections of the deposit. This program was successful and is recognized in partially defining the Bronson Slope porphyry copper- gold deposit. A total of 19,320 metres of drilling over 92 diamond drill core holes were drilled in 1965, 1984, 1988, 1993 through 1997, and 2006 and 2007. This drilling has defined the current resource that is detailed in **Item 17**. Also during the period of 1995 to 1997, extensive pre-feasibility engineering and scoping studies were completed. In 2008 a Preliminary Economic Study was completed that is detailed in **Item 18**.

6.2 Chronology

The major exploration activities on the Bronson Slope Property occurred between 1993 and 1997; however, exploration started much earlier and a summary review of each of these years' activities is given below. References include Yeager (1994), Yeager (1998b), and Yeager (2003).

1907-1920 - The earliest recorded work on the deposit was by the Iskut Mining Company who completed, between 1907 and 1920, surface and minor underground exploration of a number of base and precious metal prospects on the southwest slope of Bronson Creek valley. In the period 1911 to 1920 the Iskut Mining Company reported drifting, trenching and stripping a number of gold bearing veins on the Red Bluff and Iskut claims.

1962-1965 -The next phase of work for which accurate records were available was done during the period 1962 to 1965 (Parsons, 1965) during which time Cominco Ltd. had an option to develop the ground. Both regional and property scale surface mapping and prospecting were performed. This culminated, in 1965, with a packsack drill program comprising seven holes for a total of 337 metres of drilling. This program discovered several areas of promising copper and molybdenum mineralization, however the relatively low copper grade and gold prices prevailing at the time prohibited realization of the potential of the deposit.

1987-1988 - During the construction, in 1987, of the Johnny Mountain mine facilities by Skyline several contour lines were soil sampled in the vicinity of the Red Bluff (on the Red Bluff crown granted claim which is in part underlain by intrusive quartz porphyry) as a preliminary step to performing a comprehensive exploration program to rediscover the object of the early 1900's prospecting and claim staking activity. The soil samples contained, among other metals, extremely high gold values. In 1988, following initial grid soil sampling and prospecting, a total of 1938 metres of diamond drilling was performed in five areas of the Bronson Slope, defined by anomalous gold concentrations in rock and soil samples and by base metal sulphide mineralization. The object of the drilling was to locate high-grade concentrations of precious metals similar to the nearby Stonehouse (Johnny Mountain gold deposit) and Twin Zone deposits (Snip gold mine) and therefore it was directed at mineralized cross structures. Again, promising low-grade concentrations of gold, copper and molybdenum were found but the values encountered were insufficiently high to interest the company in continuing the program.

1990-1991 – Skyline completed exploration programs on behalf of Placer Dome Inc. in 1990 and 1991 that had an option on a block of the Skyline ground including where the current Bronson Slope deposit is located. This work consisted of 1:2500 scale geological mapping, prospecting, trenching, extensive geochemical soil sampling for precious and base metals. Geochemical and geological survey lines were oriented grid north (025° 12' azimuth) and were at about 100-metre spacing. This mapping work was instrumental in defining a geological favourable or "anomalous area" of alteration and anomalous soil geochemistry covering a southeast strike through the Bronson Slope Property parallel to the Bronson Creek Valley. The "anomalous area" is found over the complete strike length of the property, which is about 1800 metres. The Red Bluff potassium feldspar porphyry is defined by an intense gossan and cliff zone. This in turn is surrounded by an intense phyllitic zone comprising quartz, sericite, and pyrite. To the southeast along the south side of Bronson Creek Valley this alteration grades into a propylitic zone of quartz, biotite, pyrite and chlorite contained within sandstone/siltstone/wacke sedimentary and dacitic volcanic units. The "anomalous area" is for the most part underlain by a strong, well defined, and continuous in-situ gold anomaly. The anomaly threshold is considered to be 91 parts per billion gold, however, a majority of the anomaly is characterized by + 250 ppb values. Coinciding copper and zinc in-situ soil anomalies occur intermittently. A strong 1.2 kilometre long copper soil anomaly is coincident to the gold anomaly at its western edge. Most of the copper values are in excess of 400 parts per million (ppm). Placer was exploring for gold-vein mineralization contained within a south easterly extension of the then producing Snip gold mine owned by Cominco Ltd.; consequently they did not recognize or consider the porphyry copper-gold potential. In excess of $ 1 million dollars was funded by Placer for this 1990 and 1991 exploration although part of it was spent on the adjoining Iskut Property owned by Skyline.

1992 – A complete review of the Bronson Slope data was made by Burgoyne (1992) and on the basis of this evaluation, the recognition of a potential large porphyry copper-gold deposit was recognized and appropriate exploration recommendations, including diamond drilling, were made; these were subsequently followed out in 1993 through 1997.

1993-1997 - A complete review of the Bronson Slope data was made by Burgoyne (1992) and on the basis of this evaluation, the recognition of a potential large porphyry copper-gold deposit was recognized and appropriate exploration recommendations, including diamond drilling were made; these recommendations were subsequently followed out in 1993 through 1997. Skyline performed a limited program of Induced Polarization surveys on the Bronson Slope copper-gold porphyry system in 1993. These surveys were done by Scott Geophysics and covered most of the trend of the now Bronson Slope deposit and included 12 cross lines that varied from 330 to 700 metres in length. Most of the exploration work completed after the geophysical survey of 1993 was directed to core drilling in 1993, 1994, 1995, 1996, and 1997. This core drilling included nine separate drilling programs by Skyline (1994 and 1996 were subject to two separate programs each). All exploration and drilling ended on the deposit in 1997. **Note Table 11-1** and **Item 11.0.** Upon acquisition of the High Wall area (of the Bronson Slope deposit) from Prime Resources Group, Skyline also obtained access to previously drilled core completed in this area. Skyline's 1997 program included the surveying of 7 historic Cominco/Prime core holes from 1986 and 1994 totalling 2332 metres, re-logging of the drill holes, core splitting, and geochemical analyses of un-sampled porphyry mineralization. Also during the 1993-1997 periods, but mostly in 1997, extensive pre-feasibility, engineering, and scoping studies were completed; some of this work was done in 1998 and is detailed in **Item 18.0.** In 1999 Skyline completed an underground drifting program of 200.4 metres and 19 drill holes over 1494.5 metres on exploring for extensions to the Snip Gold Mine shear veins. Royal Gold Inc funded this program.

All drilling and exploration on the deposit ended in 1997.

Also during 1996 and 1997 Skyline completed a substantial amount of engineering scoping, environmental, cash flow, metallurgical, capital and operating costs, geotechnical, infrastructure and access, and other pre-feasibility studies on the Bronson Slope deposit. **Note Item 18 and Table 18-1.**

In late July 1997 the Company was able to announce the acquisition of two key mineral titles from Prime Resources Group Inc., which helped to enhance the Bronson Slope project. Two properties. The Kathleen fraction, and High Wall both of which are adjacent to Skyline's Bronson Slope. The Kathleen fraction allowed Skyline to consolidate its four principal Bronson Slope claims into one continuous block as indicated in **Figure 4-3**.

Upon acquisition of the High Wall area (of the Bronson Slope deposit) from Prime Resources Group, Skyline also obtained access to previously drilled core completed in this area. Skyline's 1997 program included the surveying of 7 historic core holes, re-logging of the drill holes, core splitting, and geochemical analyses of un-sampled porphyry mineralization. A six hole drill program conducted on the High Wall zone in 1997 defined a zone of gold mineralization with a strike length of 800 metres parallel to both the Bronson Slope porphyry deposit and to the Snip shear zone vein deposit. The High Wall gold zone is discussed further in **Item 11.0** and **Item 6.3.2.** The zone contains disseminated gold mineralization grading in the 0.5 g/t to 0.6 g/t range over a true thickness of 60 -70 metres; this has substantial exploration tonnage potential.

1999

In 1999 Skyline completed an underground drifting program of 200.4 metres and 19 drill holes over 1494.5 metres on exploring extensions to the Snip Gold Mine shear veins; this program was funded by Royal Gold Inc. These drill holes are not included in the Bronson Slope database.

It is estimated that in the order of $3.5 million 2006 dollars was spent in the period of 1988 through 1997 on drilling, geology, and other exploration surveys. It is estimated that an equivalent amount was also spent on development and engineering studies from 1996 and 1997 (Yeager 2006).

2006

An NI 43-101 compliant Technical Report was completed in June of 2006 defining the Historical Resource at Bronson Slope (Burgoyne 2006).

During 2006 an office recompilation of drilling data was done followed in September and October by a four hole 561.6 metre HQ diameter core drilling program. The total 2006 exploration expenditures were $1.45 million. In May of 2007 a NI 43-101 compliant Technical Report defining the current mineral resource at Bronson Slope was completed (Burgoyne and Giroux 2007).

2007

During 2007 a drilling program was carried out between July and October totalling 11 NQ thin wall holes over 3936 meters. The total 2007 exploration expenditures were $3.7 million. In April of 2008 a NI 43-101 compliant Technical Report defining the current mineral resource at Bronson Slope was completed (Burgoyne and Giroux 2008). Note **Item 17**.

6.3 Historical Mineral Resource Estimates

6.3.1 Base Case Historical Resource Estimate

The base case historical mineral resource estimate for the Bronson Slope deposit is that completed by Giroux (1996b) and is detailed in Skyline's 43-101 Technical Report dated June 2006. The Burgoyne (2006) reports detail the rationale and reasons for the definition of this historical resource estimate. Here Giroux used a block model and ordinary kriging to determine the resource. The base case estimate, at US $1.00 equivalent to C$1.33, a US $6 NSR (Net Smelter Return) cut off, after using US $ 385 / ounce for gold, US $5.25 / ounce for silver, and US $1.10 / pound for copper and metal recoveries, smelter payments, refining charges, treatment charges and transportation is given below in **Table 6-1**:

TABLE 6-1
BRONSON SLOPE HISTORICAL RESOURCE - BASE CASE (Giroux, 1996b)
Cut Off US $ 6 NSR

Category	Tonnes	**Au g/t**	**Ag g/t**	**Cu %**
Measured	2,280,000	0.574	2.59	0.210
Indicated	65,000,000	0.527	2.46	0.195
Total Measured + Indicated	**67,280,000**	**0.528**	**2.46**	**0.196**
Inferred	24,300,000	0.454	2.23	0.199

The Giroux (1996b) historical resource base case, detailed in Burgoyne (2006), is the second of four historical estimates done by Giroux.

6.3.2 Background

Several resource estimates were undertaken by Skyline in the period of 1994 through 1997. Some of the initial estimates were done mainly to identify zones of mineralization for future drilling and define tonnage ranges for future engineering studies. C.M. Turek undertook the in-house Skyline resource estimates, at this time, using the PC-EXPLORE software of Gemcom Services in Vancouver. The second group of resource estimates were completed over a plus one-year period (April 1996 to July 1997) using outside consultants G.H. Giroux, P. Eng. and G.F. Raymond, P.Eng. At the time of the consultant's estimates and later, Skyline also engaged Mr. W. Martin, a Skyline employee, to undertake combined resource /mine plan estimates for modelling and economic analyses using SURPAC software and Whittle optimization pit plan.

Table 6-2, below**,** illustrates the historical *base case estimate* plus several other historical estimates that were completed. These historical estimates are discussed in detail by Burgoyne (2006). The other historical estimate that is relevant and valid is that of Raymond (1997) where he uses essentially the same block modelling criteria and parameters and metal prices as that done by Giroux, to estimate 63.4 million tonnes grading 0.55 g/t gold, 2.59 g/t silver and 0.197 % copper in the measured and indicated category. No inferred resource was estimated although Raymond states there is an un-estimated inferred resource component. The measured and indicated resource and metal grades are quite similar to that of the base case Giroux study.

In addition to the above resource, Skyline, in late 1997, completed preliminary estimations as to the size and grade of the High Wall Gold Zone, which is located on the south side of the deposit, within the High Wall area of a potential open pit. There was no formal independent historical resource report and the resource estimations done by Skyline were not 43-101 or CIMM compliant and are not relevant on this zone. However, drilling indicated an exploration potential in the range of 12 to 15 million tonnes grading 0.5 to 0.6 g/t gold. The High Wall Zone has been incorporated into the current resource estimated for Bronson Slope given in **Item 17.0**.

The independent resource estimates given in **Table 6-2** are all based on a specific gravity of 2.65. The resource portion of the High Wall (HW) is not taken into account in the Giroux (1996b) and Raymond (1997) studies.

TABLE 6-2
BRONSON SLOPE HISTORICAL RESOURCE ESTIMATES

Study*	Date US $ 6 NSR Cut Off	Method**	Category***	Tonnes (Millions)	Au g/t	Ag g/t	Cu %	Mo ppm	NSR
Giroux	April 30 96	Kriging 100m**	Ind	54.7	0.557	2.38	0.186		8.89
40 ddh			Inf	20.7	0.473	1.84	0.169		7.69
		Kriging 250 m**	Ind	53.0	0.557	2.37	0.186		
			Inf	84.5	0.455	1.80	0.166		
Giroux	**Oct 8 96**	**Kriging+ 100 m**	**Meas + Ind**	**67.3**	**0.528**	**2.37**	**0.196**		**8.72**
47 ddh	**Base Case**	**	**Inf**	**24.3**	**0.454**	**2.23**	**0.199**		**7.95**
		Kriging 250 m**	Meas + Ind	67.3	0.529	2.37	0.196		8.72
			Inf	103.0	0.459	2.34	0.182		7.77
Giroux	Dec 16 96	Kriging100 m**	Meas + Ind	74.5	0.559	2.65	0.198		9.10
56 ddh			Inf						
		Kriging250 m**	Meas + Ind	78.4	0.638	2.74	0.194		9.87
			Inf	103.6	0.718	2.87	0.175		10.45
Giroux	May 1 97	Kriging100m**	Meas + Ind	85.9	0.590	3.05	0.163		8.91
63 ddh			Inf	41.1	0.629	3.62	0.116		8.66
		Kriging 250 m**	Meas + Ind	90.6	0.646	3.07	0.159		9.47
			Inf	179.7	0.670	3.35	0.123		9.20
Raymond	**July 15 97**	**Kriging**	**Meas + Ind**	**63.4**	**0.55**	**2.59**	**0.197**	**65**	**8.97**
62 ddh		Polygon	Meas + Ind	55.4	0.652	3.27	0.225	75	10.53

* ddh = diamond drill hole ** Search Ellipsoid Distance in metres * * *Meas = Measured, Ind = Indicated

6.3.3 Raymond 1997 Study

Raymond objectives (Raymond 1997) were to review deposit modelling on previously completed resource estimates; to review the problem with repeatability of higher-grade gold assays; and to recommend a drill spacing for feasibility mineral reserve estimates. The database consisted of 4284 samples with assays (typically 3 m samples) from 12,549 m of drilling in 62 drill holes. In assessing potential gold assay problems he used the strong correlation between gold and copper. Raymond's concern, at the time, was to define mineral resources of the measured and indicated categories that were drilled close enough for that required for production mine design and scheduling and consequently on completion of a pre-feasibility (or feasibility) study converted to a mineral reserve. Consequently the approach was one of constraint with respect to the geologic model, the assays and resource estimation. The resource part of the study was concerned with the measured and indicated categories; the inferred resource component was not estimated.

Raymond made a series of recommendations to firm up the Bronson Slope database and for future drilling. All of these recommendations, where applicable, were completed by Skyline in 1997 and in 2006 (Burgoyne 2006) and/or have been carried out in this report.

7.0 Geological Setting

7.1 Regional Geology

The Iskut River region is within the Intermontane Belt on the western margin of the Stikine Terrane. Three distinct stratigraphic elements are recognised in the western portion of the area (Anderson, 1989): (i) Upper Palaeozoic schists, argillites, coralline limestone and volcanic rocks of the Stikine Assemblage, (ii) Triassic Stuhini Group volcanic and sedimentary arc related strata, and (iii) Lower to Middle Jurassic Hazelton Group volcanic and sedimentary arc related strata.

Intrusive rocks in the Iskut River region comprise five plutonic suites. The Stikine plutonic suite comprises Late Triassic calc-alkaline intrusions, which are coeval with Stuhini Group strata. The Copper Mountain, Texas Creek and Three Sisters plutonic suites are variable in composition but are roughly coeval and co-spatial with Hazelton Group volcanic strata. Tertiary elements of the Coast Plutonic Complex are represented by predominantly granodiorite to monzonite Eocene intrusions of the Hyder plutonic suite, exposed 12 kilometres south of the Bronson Slope deposit (Alldrick et al., 1990).

The age, mineralogy and texture of the Red Bluff porphyry stock (associated with the Bronson Slope deposit), suggest that it belongs to the metallogenetically important Early Jurassic Texas Creek plutonic suite (Alldrick et al, 1990). Plutons of this suite are widespread in the Stewart, Iskut River region and range in age from 196 to 185 million years (Anderson, 1993; MacDonald et al., 1992). **Figure 7-1** illustrates Regional Geology taken from Rhys (1995b)

7.2 Property Geology

The description on property geology is taken largely from Rhys (1995a), Rhys (1995 b), Yeager (1998b) and Yeager (2003) and the surface geology, illustrated in **Figure 7-2,** is taken from Piteau Associates (1997). Geological sections from 25000E through 25700E are illustrated at the end of **Item 11.**

A folded sequence of turbiditic feldspathic greywackes with subordinate inter-bedded siltstones, mudstones, volcanic conglomerate and rare, carbonate lenses is intruded by the Red Bluff porphyry. The greywackes are massive to crudely bedded. Individual graded beds may have sharp, scoured basal contacts and may contain siltstone or mudstone rip up clasts. The sequence is weakly to moderately metamorphosed (lower greenschist facies). Alteration ranges from weak to strong in the vicinity of mineral prospects. Pebble to cobble sized clasts of fine-grained and porphyritic mafic to felsic volcanic rocks are present in coarser beds, and coupled with the common presence of angular to sub rounded plagioclase grains in greywacke units, imply a proximal volcanic source. These rocks are probably lateral equivalents of Stuhini Group strata exposed on Snippaker Ridge 4 km southeast of Bronson Slope, which contain Upper Triassic fossils.

Early Jurassic felsic to intermediate volcanoclastic, pyroclastic and flow rocks that probably belong to the Lower Hazelton Group are exposed on Johnny Mountain. They are flat-lying to moderately tilted and unconformably overlie the greywacke sequence noted above. The sequences are separated by a flat lying to gently dipping regional unconformity exposed approximately one kilometer to the northeast of the Johnny Mountain Gold mine.

The Bronson stock is a heterogeneous, medium-grained equigrangular plagioclase + clinopyroxene +/- amphibole phyric diorite. The stock lies north of the former producing Snip gold mine. A poorly constrained Late Triassic U-Pb zircon age date of between 197Ma and 225 Ma was obtained from a K feldspar + plagioclase phyric monzodiorite phase of this unit (Macdonald et al, 1992). Several small stocks, sills and dikes of unknown age and intermediate to mafic composition intrude the Bronson stock. Lamprophyre dykes of probable Jurassic age have been mapped at numerous locations on the property and in addition lower Jurassic feldspar porphyry dykes and Tertiary intrusive stocks have been noted. Basalt dykes, possibly correlative with Recent volcanism, have also been observed

The lower sequence is intruded by the Red Bluff porphyry stock (Bronson Slope deposit), a hydrothermally altered, potassium feldspar megacrystic, plagioclase porphyritic intrusion of probable granodioritic composition. The stock is approximately 2.0 kilometres long, up to 0.3 kilometres wide and trends southeast along the southwest side of the Bronson Creek valley. Contacts of the stock with country rocks are not well defined, but where observed in drill core or underground workings are either faulted or intrusive. The southwest and northeast contacts appear to be southwesterly dipping. Screens of altered greywacke up to 40 m wide are common throughout the intrusion. The age of the Red Bluff intrusive is Lower Jurassic.

The Red Bluff porphyry is a hydrothermally altered K-feldspar megacrystic, plagioclase porphyritic intrusion of probable quartz diorite to quartz monzonite composition. Subhedral tabular pink K-feldspar phenocrysts generally range in length from 2 mm to 20 mm. They usually comprise from less than 1% to 5% of the modal mineralogy. The matrix to the K-feldspar megacrysts consists of medium-grained porphyry containing phenocrysts of albitic plagioclase, altered amphibole and quartz. The plagioclase is usually completely altered to aggregates of sericite+/- quartz +/- K-feldspar. Mafic phenocrysts, probably original hornblende from grain shapes, are commonly altered to magnetite, hematite, pyrite, biotite, and chlorite. Equant, clear to smoky sub rounded quartz phenocrysts, 0.2 mm to 1.5 mm in diameter, comprise less that 1% to 4%. In areas of moderate to intense alteration original quartz is difficult to identify. Accessory minerals include apatite, zircon and titanite. The fine-grained matrix to the phenocrysts forms between 35% and 70% of the rock volume.

Mineralization and alteration in and adjacent to the Red Bluff porphyry system are detailed in **Item 9.0** and summarized below:

- Quartz-magnetite-hematite veins are the earliest phase of veining in the Red Bluff porphyry system. They form an intense stock work that is spatially related to the Red bluff porphyry.
- The quartz-Fe-oxide stock work and altered sediments on its southwest margin are overprinted by quartz-pyrite+/-chalcopyrite veins/alterations and pyrite + chalcopyrite veinlets that are associated with the highest gold and copper grades. Where quartz-pyrite assemblages overprint and sulphidize the quart-Fe-oxide stock work there is a net loss of iron from the system. Veins are discrete, with sharp boundaries outside the stock work in greywacke, but have indistinct alteration boundaries with quartz-Fe-oxide veins within the stock work.
- The overall sequence from intense early Fe-oxide veining to less intense Quartz-pyrite-chalcopyrite veins and finally to pyrite and carbonate stringers corresponds with a progressive decrease in the total amount and intensity of veining though time.
- A 25 to 50 metre wide zone known as the transition zone of K-feldspar + Fe oxide alteration in greywacke occurs along the western upper periphery of the quartz-magnetite-hematite stock work and separates stock work from biotitic greywacke to the west. Calcite veinlets, common in the biotitic greywacke, become predominantly quartz veinlets in the transition zone.

Biotite lamprophyre dikes, un-deformed and unaltered, intrude northeast-trending faults in the Red Bluff cliff area. They are confined immediately adjacent or within fault zones.

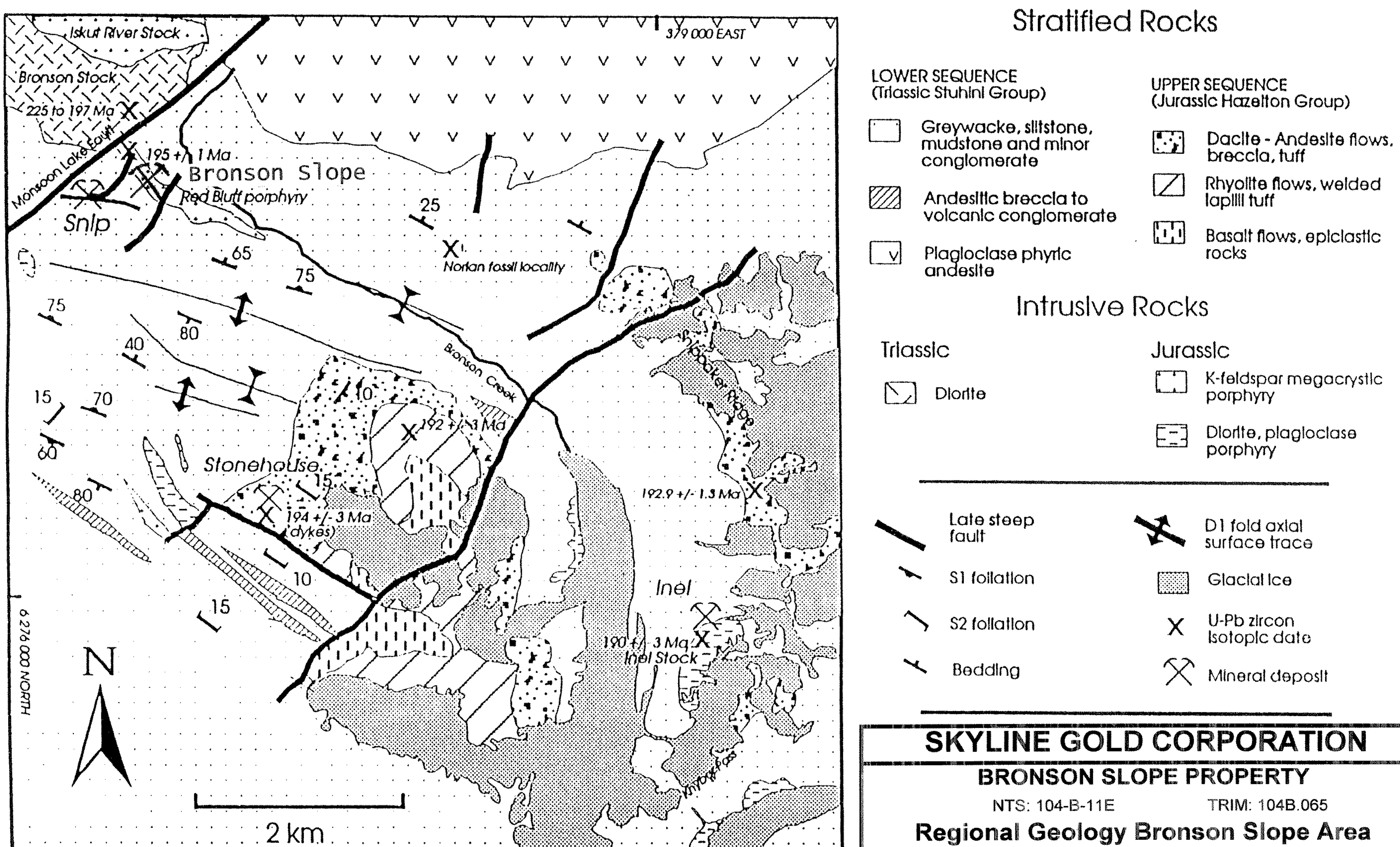
7.3 Structure

The Triassic strata on Johnny Mountain are folded into an anticlinal structure defined by tight, locally overturned, northwest-trending regional and parasitic folds. An adjacent syncline follows the Bronson Creek valley along strike from the Red Bluff porphyry. The folds are associated with a moderate to northeast-dipping axial planar phyllitic flattening fabric (S1). All of the structures, and the entire Triassic-Jurassic sequence were subject to a later deformation resulting in shallowly dipping to sub-horizontal foliation (S2). Abundant shallow-dipping extension veins cut the fabrics on Johnny Mountain. Moderate to steep northwest-dipping and southwest-dipping fault sets cut all other lithologies and structures in the area.

To date, with the exception of the Red Bluff porphyry system, other mineral prospects on the property appear to be in veins or silicified shear zones. Most of the mineralized prospects conform to the following three shear directions:

- Northwest dipping shears ($060^{O}/70^{O}$ NW) – e.g., Stonehouse Gold Deposit, Johnny Mountain
- Southwest dipping shears ($120^{O}/45^{O}$ SW) - e.g., former mined Snip Gold Deposit, and,
- Northeast dipping shears ($130^{O}/45^{O}$ NE).

In the case of the Snip shear direction, which trends onto Bronson Slope, the shearing may be related to regional folds that vary in intensity from small open fold belts to anticline-syncline pairs that can result locally in overturned bedding. The axial plane cleavage developed in these folds has created weakness in the rock and these zones of weakness have created conditions favorable for shearing in a northwest-southeast direction. The adjacent Snip veins appear to be emplaced in a shear zone that has developed in the axial plane cleavage of an anticline inferred from Skyline mapping of the sedimentary rocks further south along the Bronson Creek valley. The Red Bluff porphyry may be emplaced parallel to the axial plane cleavage of the corresponding syncline lying just to the northeast of the Snip anticline.



(from Rhys, D.A., 1995b)

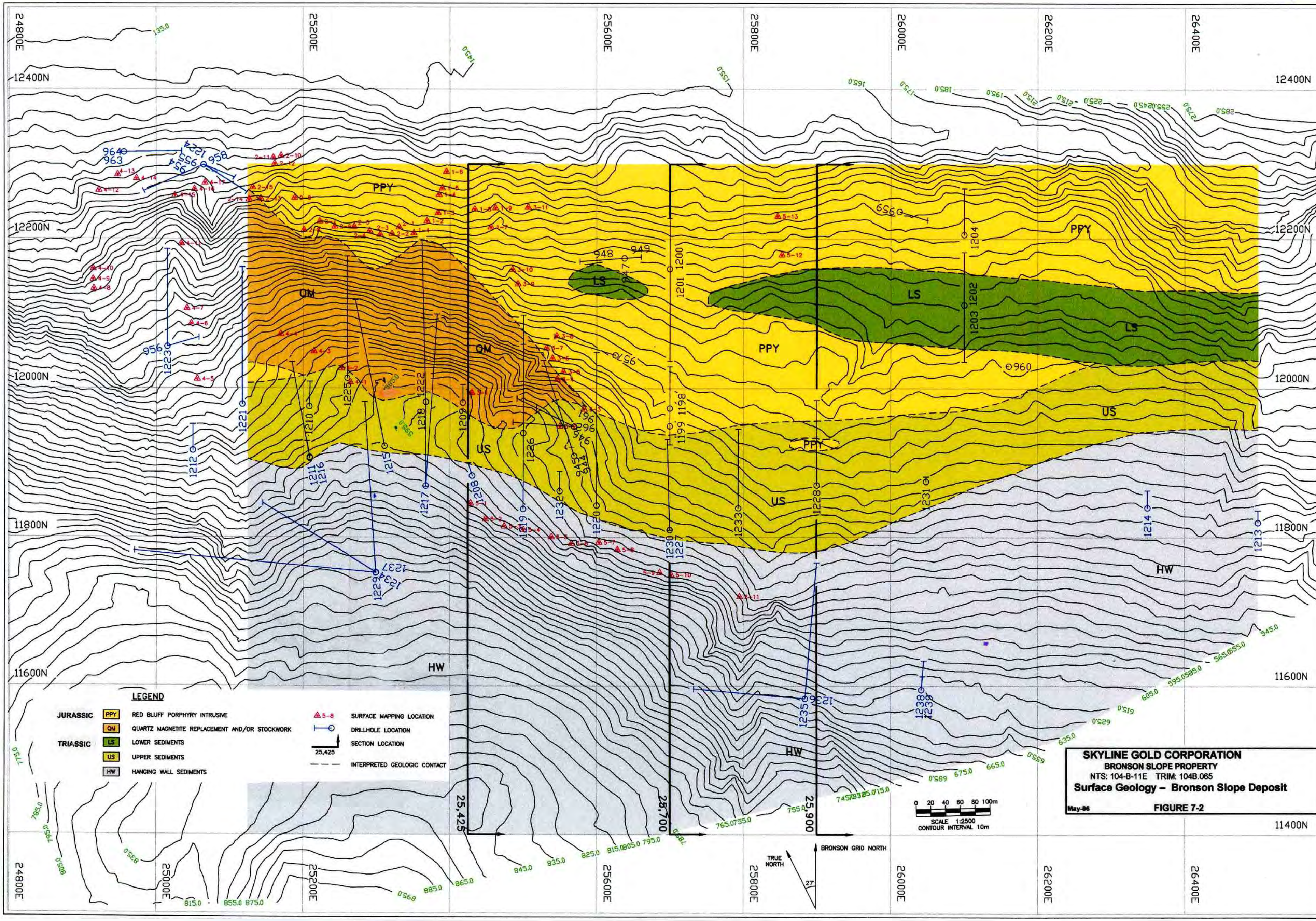
SKYLINE GOLD CORPORATION

BRONSON SLOPE PROPERTY

NTS: 104-B-11E TRIM: 104B.065

Regional Geology Bronson Slope Area

May 07	**FIGURE 7-1**


LEGEND
JURASSIC
PPY RED BLUFF PORPHYRY INTRUSIVE
QM QUARTZ MAGNETITE REPLACEMENT AND/OR STOCKWORK
TRIASSIC
LS LOWER SEDIMENTS
US UPPER SEDIMENTS
HW HANGING WALL SEDIMENTS
SURFACE MAPPING LOCATION
DRILLHOLE LOCATION
SECTION LOCATION
INTERPRETED GEOLOGIC CONTACT
SKYLINE GOLD CORPORATION
BRONSON SLOPE PROPERTY
NTS: 104-B-11E TRIM: 104B.065
Surface Geology – Bronson Slope Deposit
May-06
FIGURE 7-2
SCALE 1:2500
CONTOUR INTERVAL 10m
TRUE NORTH
BRONSON GRID NORTH
24800E
25200E
25600E
25800E
26000E
26200E
26400E
12400N
12200N
12000N
11800N
11600N
11400N
PPY
QM
LS
US
HW
25,425
25,700
25,900

8.0 Deposit Type

The Bronson Slope copper-gold-silver-molybdenum mineralization is considered to be a porphyry copper-gold deposit type that contains, dependent on rock type and alteration, abundant magnetite. Magnetite mineralization is spatially associated with the Quartz magnetite Breccia and the Red Bluff Porphyry Intrusive units.

Porphyry deposits (Kirkham, R.V. and Sinclair, W.D., 1996) are large, low to medium-grade deposits in which hypogene ore minerals are primarily structurally controlled and which are spatially and genetically related to epizonal and mezonal, felsic to intermediate porphyritic intrusions. The large size and structural control (e.g., veins, vein stock works, fractures, crackled zones, and breccia pipes) are of fundamental importance and serve to separate porphyry deposits from genetically-related (e.g., some skarns, high-temperature mantos, breccias pipes, etc.) and unrelated deposit types. Orientations of mineralized structures appear to be related to local stress environments around the top of the pluton or can reflect regional stress conditions.

Supergene minerals may be developed in enriched zones in porphyry deposits by weathering of primary sulphides.

The Bronson Slope deposit is considered to be a porphyry copper-gold subtype. This style of mineralization, many of which, but not all, are commonly associated with alkaline intrusive rocks. Bronson Slope is an exception in that it is associated with a plagioclase-clinopyroxene diorite or granodiorite intrusion. This subtype is defined if the gold content is greater than 0.4 g/t gold. If the content exceeds 0.8 g/t gold, the subtype can be identified as a porphyry gold deposit.

In British Columbia porphyry copper-gold deposits are commonly associated with Triassic and Lower Jurassic silica saturated intrusions, formed in an island-arc setting, but possibly during periods of extension.

9.0 Mineralization

This discussion of mineralization is taken in part from Rhys (1995a).

On the southwest side of the Red Bluff porphyry foliated sedimentary greywacke rocks contain calcite+/-quartz +/-pyrite +/- chlorite veinlets and stringers are either parallel to foliation or folded by the foliation. Sericitic shear zones are developed locally and are parallel to the surrounding pervasive foliation. On the southwest side of the Red bluff porphyry within 25 to 50 metres of the quartz magnetite-hematite stock work that defines the core of the system, foliation in the sediments generally disappears, magnetite appears as disseminations in veinlets and in quartz veins. Here veins become quartz-dominant with sparse calcite and intense K-feldspar alteration is widespread. The rock is commonly pale to dark green, mottled with disseminated blebs of magnetite + hematite. Quartz-magnetite-hematite veins, generally 0.3 to 2 cm wide, increase in density and thickness gradually down hole as the quartz-Fe-oxide stock work is approached. This area of distinctive alteration is termed the transition zone.

The Red Bluff porphyry hydrothermal system is dominated by an intense quartz-magnetite-hematite stock work that trends northwest along the northern slope of Johnny Mountain and the south side of Bronson Creek valley. The stock work overprints and is intimately associated with the Red Bluff porphyry intrusion. Margins of the stock work are usually discrete. Over intervals of a few metres vein abundance increases from 10-25% of the total rock outside the stock work to greater than 60% within it. The veins form an intense stock work that usually contains less than 20% interstitial rock. Drill intersections of 20 to +100 metres long are composed entirely of intersecting to sheeted sets of quartz-magnetite-hematite veins. Individual veins range from 0.5 to 10 cm in thickness. Vein to core axis angles are highly variable.

The quantity and tenure of magnetite mineralization defined by the 2009 core-sampling program in certain drill holes of the Bronson Slope deposit is discussed in **Item 11**. Magnetite mineralization is spatially associated with the Quartz Magnetite Breccia and the Red Bluff Porphyry Intrusive units. Magnetite mineralization also occurs adjacent to the Quartz magnetite unit within the Lower Sediments unit.

The quartz-magnetite-hematite stock work is overprinted by quartz + pyrite + chalcopyrite +/- carbonate veins and by carbonate and pyrite veins. The textures suggest that much of the quartz-pyrite may be an in situ alteration of the quartz-Fe-oxide assemblage. The total sulphide content in the quartz-pyrite assemblage is around 5%. The quartz-pyrite assemblage comprises less than 10% of the older quartz-magnetite-hematite veins.

Pyrite + chalcopyrite +/- carbonate veinlets and veins frequently cut, but are intimately associated with the quartz-pyrite veins and alteration. They commonly have consistent core to axis angles suggesting they are sheeted.

The quartz-pyrite veins/alteration are locally brecciated. Breccias have variable contacts with the surrounding quartz veins that vary from gradational to sharp. A late set of quartz veins, possibly Tertiary in age, cuts all of the rock types and veins. These veins are flat to shallow southeast dipping, lenticular in shape and commonly occur in en echelon arrays. In drill core they are difficult to distinguish from veins in the Red Bluff porphyry system.

Gold and copper grades reflect the distribution of the different veins and alteration types. Areas of quartz-magnetite-hematite veining with sparse or no pyrite-chalcopyrite or quartz-pyrite overprinting typically grade less than 600 ppm copper, and less than 0.2g/t gold (Rhys 1995a). Higher copper and gold grades occur in quartz-pyrite-chalcopyrite veins and alteration and in areas of abundant pyrite-chalcopyrite veining both inside the quartz-Fe-oxide stock work and in adjacent greywacke; here grades can vary from greater than 600 ppm to 5000 ppm copper and greater than 0.2g/t gold to 10 g/tonne gold (Rhys 1995a).

The Red Bluff potassium feldspar porphyry is defined by an intense gossan and cliff zone. This in turn is surrounded by an intense phyllitic zone comprising quartz, sericite, and pyrite. To the southeast along the south side of Bronson Creek Valley this alteration grades into a propylitic zone of quartz, biotite, pyrite and chlorite contained within sandstone/siltstone/wacke sedimentary and dacitic volcanic units.

10.0 Exploration

Pre 1987 exploration conducted prior to Skyline is detailed in **Item 6** and in Burgoyne and Giroux (2007**)**. The earliest recorded work on the deposit was by the Iskut Mining Company who completed, between 1907 and 1920, surface and minor underground exploration of a number of base and precious metal prospects on the southwest slope of Bronson Creek valley. In the period 1911 to 1920 the Iskut Mining Company reported drifting, trenching and stripping a number of gold bearing veins on the Red Bluff and Iskut claims of the Property.

The next phase of work for which accurate records are available was done during the period 1962 to 1965 during which time Cominco Ltd. had an option to develop the ground. Both regional and property scale surface mapping and prospecting were performed. This culminated, in 1965, with a packsack drill program comprising seven holes for a total of 337 metres of drilling. This program discovered several areas of promising copper and molybdenum mineralization, however the low copper grades and low gold prices prevailing at the time prohibited realization of the potential of the Property.

Exploration expenditures carried out by Skyline on the Bronson Slope Property have been extensive but have not been quantified, as much of these expenditures have been included with those on the adjoining Iskut Property including the Johnny Mountain gold mine. Although no quantitative numbers are available, considering the amount of drilling and other ground surveys, it is estimated that the equivalent of $3.5 million of 2006 dollars has been spent (Yeager, 2006). Prior to 2006, the exploration programs by Skyline occurred over an 11-year period from 1987 through 1997 with most of the exploration consisting of diamond core drilling from 1993 through 1997. In 2006 (November 1, 2005 through October 31, 2006) an HQ diameter drilling program and other studies cost $ 1.4 million. In 2007 (November 1, 2006 to October 31, 2007) an NQ diameter drilling program and mine development studies cost $ 3.7 million. The drilling is detailed in **Item 11.0** and the mine development studies are detailed in **Items 16** and **18.**

During September and October 2006 Skyline completed 561.6 meters over 4 HQ diameter holes within the Red Bluff Zone, a higher grader part of the Bronson Slope deposit. This drilling was done, in part, to compare the HQ core diameter results to those of previous NQ diameter holes in this particular area.

During July through October 2007 Skyline completed 3936 meters over 11 NQ diameter holes within the Bronson Slope deposit. This drilling was done, in part, to develop additional resource and to increase mineral resource confidence by up grading inferred and indicated categories in certain parts of the deposit to measured and indicated, respectively.

During October 2009 Skyline, using a 7 person sampling team, sampled 5923 meters of historical and 2006/2007 drill core for parts of the Bronson Slope deposit and sent the respective samples to Met-Solve Laboratories in Burnaby, BC for magnetite analyses. On the basis of these analyses a magnetite resource has been determined for the Bronson Slope deposit. Approximately $255,000 was spent on this program.

Also, separate from the sampling program, Skyline during October 2009 completed a two hole, 729-meter drilling program on the Snip 1 some 900 meters east of the Bronson Slope deposit costing approximately $250,000. **Note Item 11**, Drilling.

In summary the placement of grids, surveying, collection of the soil samples, the extensive geological mapping, the location of the drill holes, the drill hole orientations, the analyses, and the collection and analyses of core samples appears to be to good industry standards.

11.0 Drilling

11.1 Background & Summary

This drilling has defined the Bronson Slope porphyry gold-copper-silver-molybdenum system in the order of 1.5 km long and 0.4 to 0.6 km wide and an additional gold-pyrite zone known as the High Wall or Snip Extension located on the south side of the deposit. The plan of drill hole locations is illustrated on **Figure 11-1** and the distribution of the Bronson Slope porphyry style gold-copper-silver-molybdenum deposit and the High Wall Gold Zone are illustrated on **Figure 4-3**. Geological cross-sections for the 2009 magnetite sampling program and results are illustrated for Sections 25000 to 26700E at the end of **Item** 11. The High Wall Gold Zone is about 800 metres in length, 60-70 metres wide, and is located on the south side of the Bronson slope deposit.

All drilling to date has been by wire line diamond core drilling. Drilling on the Bronson Slope Deposit in 1965, 1986,1988 and 1993 through 1997, and 2006 and 2007 involved a total of 19,320 metres over 92 core drill holes. Drilling by Skyline in 1988 and 1993 through 1997 involved a total of 12,153 metres over 63 core drill holes. Drilling done in 1986 and 1994 by Cominco and Prime Resources, with respect to exploration on the adjacent Snip mine, was acquired by Skyline in 1997 – this drilling, in the High Wall of the Bronson Slope deposit, was evaluated in 1997 and included the surveying of 7 historic core holes, re-logging of the drill holes, core splitting, and geochemical analyses of un-sampled porphyry mineralization. Drilling in 2006 involved a total of 562 metres over 4 holes. Drilling in 2007 involved a total of 3936 metres over 11 holes.

The summary of diamond core drilling is given in **TABLE 11-1.**

TABLE 11-1
SUMMARY OF DIAMOND DRILLING
BRONSON SLOPE DEPOSIT

Period	Company	Drilling Contractor	Core Size*	Hole Numbers	Holes	Meters
1965	Cominco	Cominco	Packsack	1073 to 1080	7	337
1986	Cominco		BQ	S 6	1	108
1994	Prime Resources	Olympic Drilling	BQ	S101, S125-127, S129, S130	6	2224
1988	Skyline	Falcon Drilling	BQ tw	944 to 949, 954 to 964	17	1,938
1993	Skyline	Boisvenu Drilling	BQ tw	1198 to 1204	7	872
1994	Skyline	Olympic Drilling	BQ tw	1208 to 1216	9	1,550
1995	Skyline	Olympic Drilling	BQ tw	1217 to 1223	7	2,429
1996	Skyline	Britton Brothers	BQ tw	1224 to 1239	16	3,529
1997	Skyline	Britton Brothers	NQ**	1240 to 1246	7	1,835
2006	Skyline	Phil's Drilling & Boart Longyear	HQ	#BS0601 to BS0604	4	562
2007	Skyline	Blackhawk Drilling	NQ	BS 0701 to BS 0706, BS 0708 to BS 0712	11	3936
	* tw = thin wall	** One HQ hole		**Totals**	**92**	**19,320**

11.2 Bronson Slope Deposit Historical And 2006/2007 Drilling

Diamond drill hole data including hole number, depth, northing, easting, elevation, azimuth and dip are given in **Appendix A.** **Figure 11-1** should be referred to for exact drill hole location.

The surface drilling by Skyline consisted of drill holes that were completed over the Bronson Slope deposit. Drill holes varied from 28 m to 452.9 m and were BQ size diameter for the 1993 through 1996 campaigns and NQ size in the 1997 drilling campaign. The 2006 drilling program consisted of HQ diameter size. The Cominco 1965 drilling was by packsack and therefore less than 1.3 cm diameter. The Skyline drills were transported to the drill site location by helicopter. The drilling contractors are given in **Table 11-1**. All drill hole collars were transit surveyed – down the hole acid etch dip deviation surveys were completed on most core holes (from 50 to 125 metre intervals) generally on holes greater than 100 metres. No down hole surveys were done on the 1965 Cominco holes

The drilling was completed over approximately 1400 metres of strike length and 600 to 700 metres across trend on drill lines perpendicular to the assumed strike of the deposit. The stratigraphic trend is 115 degrees and many of the drill lines were perpendicular at 025 degrees azimuth. The mineralization is in the form of stock works that dip in the order of 45 to 60 degrees to the south. Many of the earlier 1988 drill holes were drilled oblique to the trend. These drill hole sections were nominally at 100 m spacing over defined mineralization although this varied in parts of the grid and was lesser and greater in certain parts of the deposit. Much of the drilling, as indicated above, was positioned to intersect the mineralization perpendicular to the trend and to its probable dip. Weighted drill core recovery for drill holes in the Bronson Slope deposit is in the order of 95% to 99% (Yeager, 2006).

It is significant that the Bronson Slope deposit is open to the east and at depth.

The analytical results and significant drill intercepts for all drilling programs have been reported in detail and summary form in Burgoyne and Giroux (2008) and the reader is referred to www.sedar.com of September 16, 2008 for skyline Gold. This aforesaid reference also gives the most current resource estimate for the Bronson Slope deposit.

Drill core from the Skyline 1994 through 1997, 2006, 2007 programs, and the Cominco/Prime 1984, 1986 and 1994 programs are contained in core racks at the Bronson Airstrip. Holes 1227, 1228, 1230, 1233 and 1234 from 1996 are missing**. Also,** drill core from the 1988 and 1993 campaigns is no longer available having been lost on collapse of drill core sheds due to snow load in the winter of 2000-2001. Also, remaining drill core sample rejects and drill sample pulps were disposed of by Skyline subsequent to 2000.

Details for the Cominco (1965) and Skyline (1988, 1993 through 1997, 1999, 2006 and 2007) drilling programs are described in detail in Burgoyne and Giroux (2008).

11.3 2009 Sampling & Magnetite Analyses Program - Results and Interpretation

The drill core intervals sampled and analysed for magnetite during 2009 are given in **Table 11-2**, while intercepts containing potentially economic concentrations (exceeding 2% magnetite over 9m) of magnetite are summarized in **Table 11-3**. All drill core sampled in 2009 was NQ (48 mm nominal) size and core was nominally sampled at 3 metre intervals from block to block in the hole as detailed in **Item 12**. Once at the core handling facility, core boxes were laid out on benches, and a Terraplus KT-10 magnetic susceptibility meter was used to take a magnetic susceptibility measurement every meter along the core length. Magnetic susceptibility measurements were recorded in SI units.

The Bronson Slope Diamond Drill Hole Data is reported in **Appendix A**. The analyses for magnetite by Met-Solve Laboratories of Burnaby, BC is given in **Appendix B** and magnetite assay – magnetic susceptibility plots are given in **Appendix C**.

A series of drill sections on 50m centres is presented at the end of **Item 11**. As shown on the sections, the zone containing potentially economic grades of magnetite appears to be approximately 300m wide and 400m deep at its northwestern end. Its dimensions apparently taper toward the southeast over a strike length of about 600m, with the copper and gold mineralization extending beyond.

TABLE 11-2
INTERVALS SAMPLED AND ANALYSED FOR MAGNETITE
2% Magnetite Cut-Off

Hole	Depth Sampled From (m)	Depth Sampled To (m)	Interval Length (m)	Sample Source*
1211	5.2	165.5	160.3	C
1212	13.1	135.3	122.2	C
1216	9.0	256.7	247.7	C
1217	60.0	423.4	363.4	C
1218	3.0	405.6	402.6	C
1219	20.2	444.2	424.0	C
1220	25.6	306.4	280.8	C
1221	9.1	312.1	303.0	C
1223	7.0	200.9	193.9	C
1225	3.7	218.6	214.9	C
1226	2.3	275.4	273.1	C
1229	209.0	450.2	241.2	C
1232	15.2	219.6	204.4	C
1245	334.5	493.0	158.5	C
1246	401.5	545.7	144.2	C
TOTAL CORE			3734.2	
0602	2.7	138.6	135.9	P
BS 07 01	216.4	466.3	249.9	P
BS 07 02	3.4	393.2	389.8	P
BS 07 03	18.3	295.7	277.4	P
BS 07 04	5.5	360.0	354.5	P
BS 07 05	3.5	429.8	426.3	P
BS 07 10	10.7	365.8	355.1	P
TOTAL PULPS			2188.9	
TOTAL METERAGE SAMPLED			5923.1	

*Sample Sources:
C=drill core split during 2009
P=pulps obtained from laboratory storage

Potentially economic magnetite grades occur in three rock units: Quartz Magnetite Breccia, Red Bluff Porphyry, and Upper Sediments. As some of the drill holes analysed for magnetite ended in magnetite mineralization, the base of the magnetite zone is not fully defined.

TABLE 11-3:
INTERCEPTS CONTAINING POTENTIALLY ECONOMIC MAGNETITE GRADES

Hole	From (m)	To (m)	Length (m)	Grade (%)
1211	90.8	165.5	74.7	7.8
1212	127.4	135.3	7.9	4.7
1216	97.2	256.7	159.5	8.8
1217	105.7	423.4	317.7	9.5
1218	3.0	405.6	402.6	7.3
1219	148.2	404.2	256.0	5.4
1220	146.6	277.6	131.1	3.6
1221	10.4	312.1	301.7	9.0
1223	35.4	200.9	165.5	6.7
1225	3.7	218.6	214.9	8.9
1226	7.9	275.4	267.5	7.2
1229	248.6	450.2	201.6	8.7
0602	2.7	138.6	120.4	6.2
0702	3.4	134.1	130.7	4.7
0702	146.5	180.0	33.5	3.0
0703	30.5	39.6	9.1	2.5
0705	6.1	30.5	24.4	2.3

The strongest magnetite mineralization is contained within a quartz-magnetite-hematite stock work, in which magnetite occurs as fine to coarse-grained disseminations and occasional semi-massive blobs. Magnetite also occurs as disseminations in highly potassic altered intrusive and sedimentary country rock surrounding the stock work.

While the Bronson Slope copper and gold deposit is open to the east and at depth, the Quartz Magnetite Unit is open to the west and appears to terminate to the east although lower grade magnetite mineralization is found in the Red Bluff Porphyry Unit to the east. The magnetite mineralization is also open at depth.

The magnetite assay results have been collated and used to prepare the resource evaluation presented in **Item 17**.

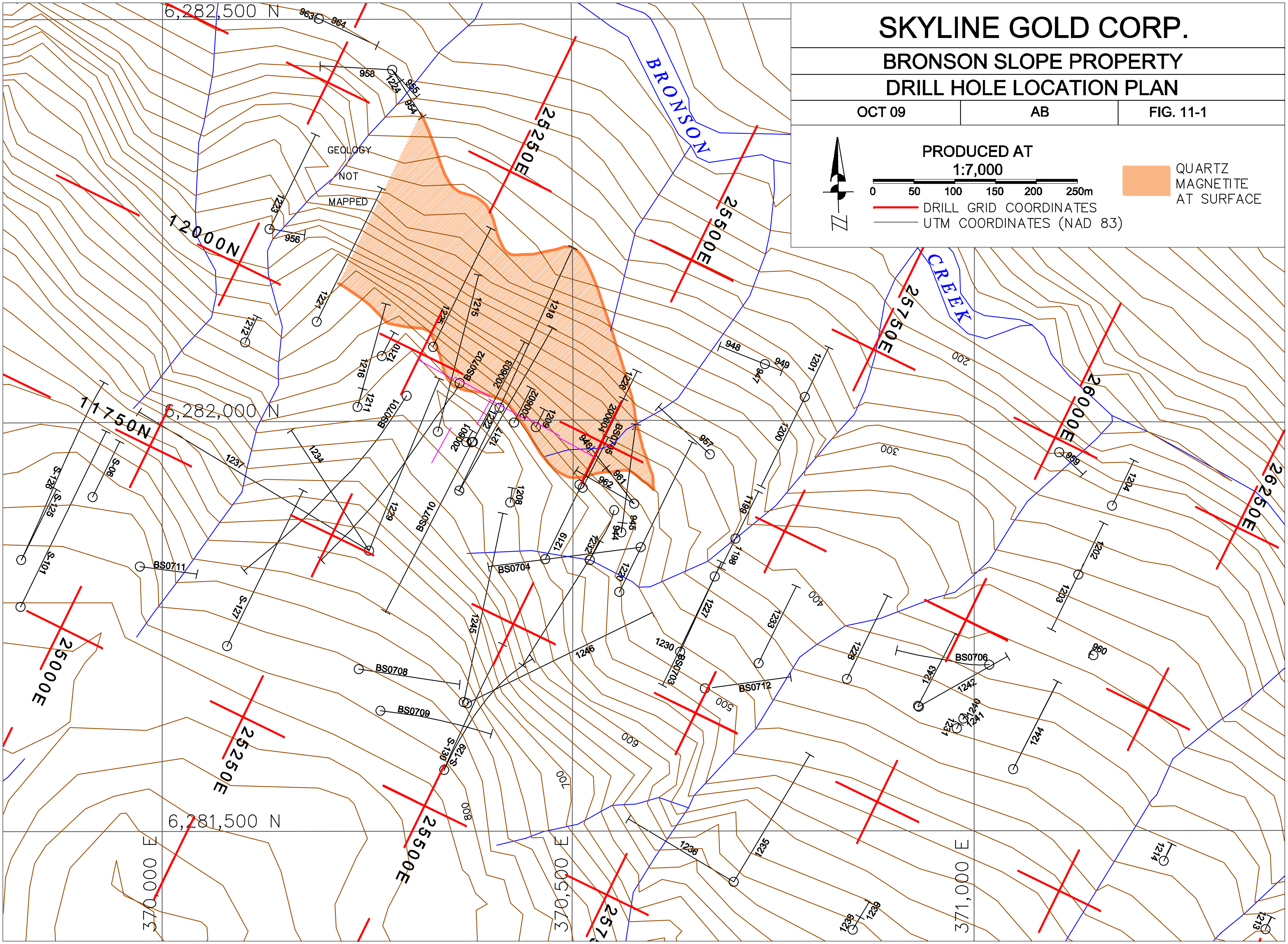
11.4 2009 Drilling on Snip 1 Claim

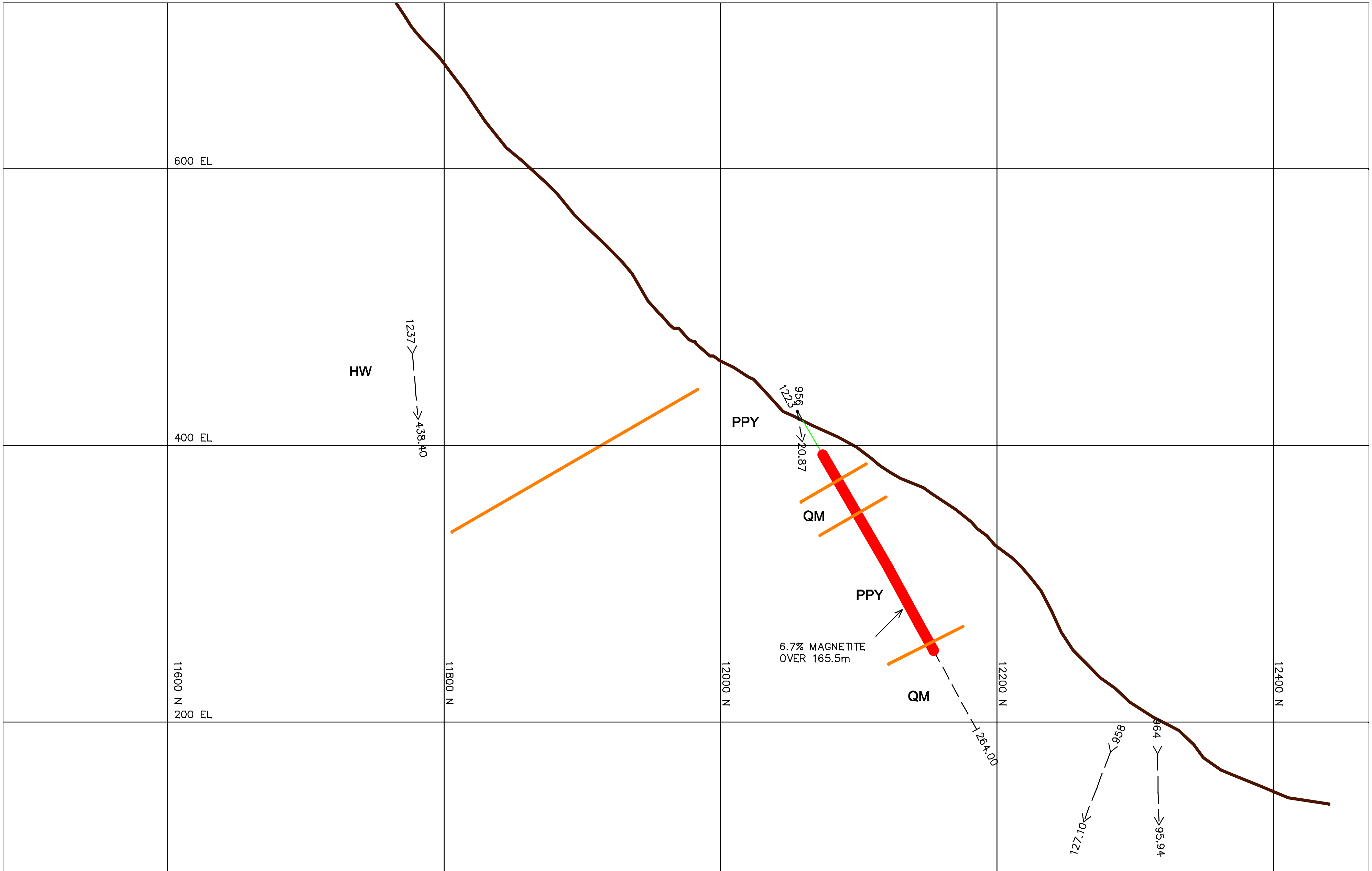
Skyline completed, in October 2010, 728.9 meters of drilling over two drill holes from a single drill pad on the Snip-1 mineral tenure. The writers have not reviewed the detailed technical information and results on this drilling program as the program was being undertaken by Equity Engineering of Vancouver, BC who are in the process of compiling and completing a report. The information given here was taken from Skyline Gold Press Releases as noted below.

The drill holes are located approximately 900 meters south east of the nearest Bronson Slope deposit drill hole and are reported on trend to the Bronson Slope deposit (Skyline Gold Press Releases of November 18 and 29, 2009). Hole SK-09-01 was drilled to 438 m at an azimuth of 011 degrees and at a dip of –65 degrees. Hole SK-09-02 was drilled to 290.8 meters at an azimuth of 061 degrees and a dip of –55 degrees. Drill core was split at Bronson Airstrip and assayed for gold, silver, copper and zinc at ALS Chemex Laboratories in North Vancouver, BC. Equity Engineering of Vancouver, BC managed the work. The following significant assays are reported by Skyline and includes screening for metallic gold on twelve selected intervals:

TABLE 11-4
2009 DRILL HOLE RESULTS – SNIP 1 CLAIM

DRILL HOLE	**FROM**	**TO**	**INTERCEPT**	**Au g/t**	**Ag g/t**	**Cu %**	**Zn %**
SK-09-01	metres	metres	metres				
	3.7	438.0	435.3	0.47	6.6	0.03	0.34
includes	5.5	32.0	26.5	1.56	17.2	0.07	0.29
includes	166.0	188.4	22.4	1.72	14.5	0.05	1.27
includes	234.1	248.0	14.0	2.07	23.2	0.12	2.11
SK-09-02							
	6.1	290.8	284.7	0.96	12	0.04	0.36
includes	39.0	120.0	81.0	2.07	30.4	0.08	0.70
includes	48.0	75.0	27.0	4.70	75.9	0.13	1.15
includes	202.7	221.4	18.7	1.94	11.5	0.04	0.43


SKYLINE GOLD CORP.
BRONSON SLOPE PROPERTY
DRILL HOLE LOCATION PLAN
OCT 09
AB
FIG. 11-1
PRODUCED AT
1:7,000
0 50 100 150 200 250m
DRILL GRID COORDINATES
UTM COORDINATES (NAD 83)
QUARTZ MAGNETITE AT SURFACE
N
BRONSON CREEK
GEOLOGY NOT MAPPED
6,282,500 N
6,282,000 N
6,281,500 N
370,000 E
370,500 E
371,000 E
12000N
11750N
25000E
25250E
25500E
25750E
26000E
26250E



GEOLOGY LEGEND

HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

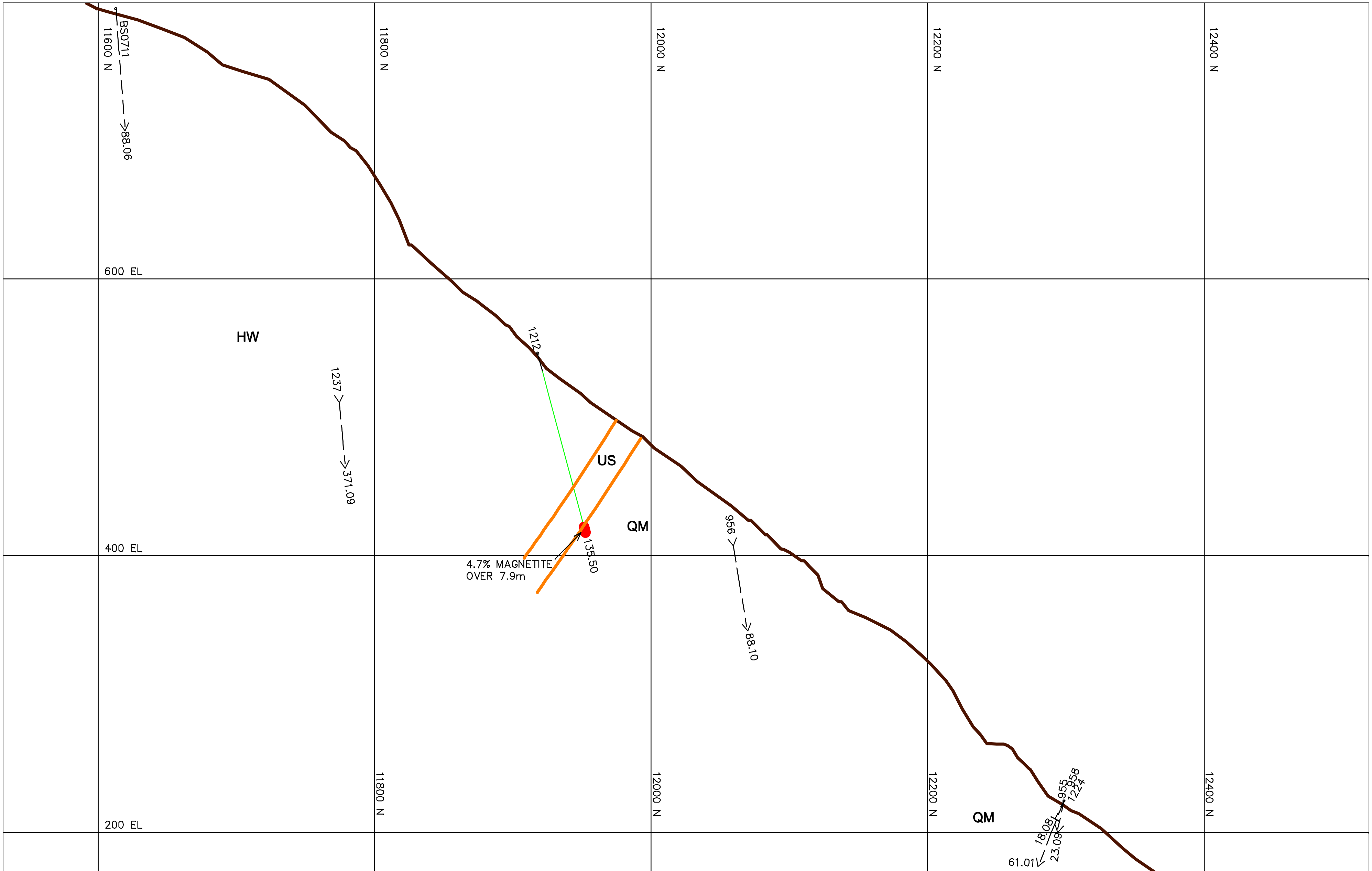
ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25000 E

DRAWN BY	DATE	PRODUCED AT
AB	JAN 10	1:4,000



GEOLOGY LEGEND

HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

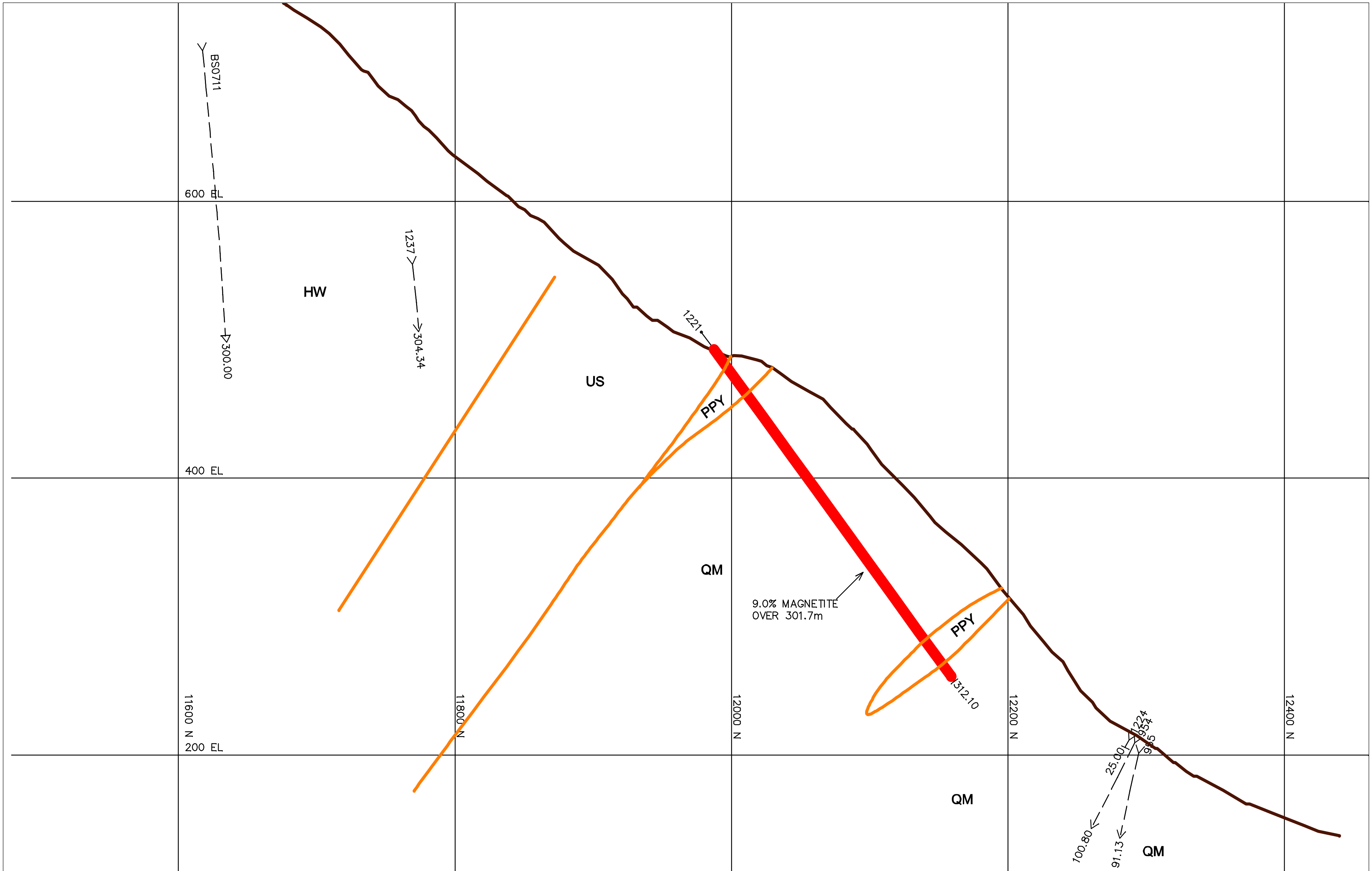
ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >7.9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25050 E

DRAWN BY	DATE	PRODUCED AT
AB	JAN 10	1:4,000



GEOLOGY LEGEND

HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

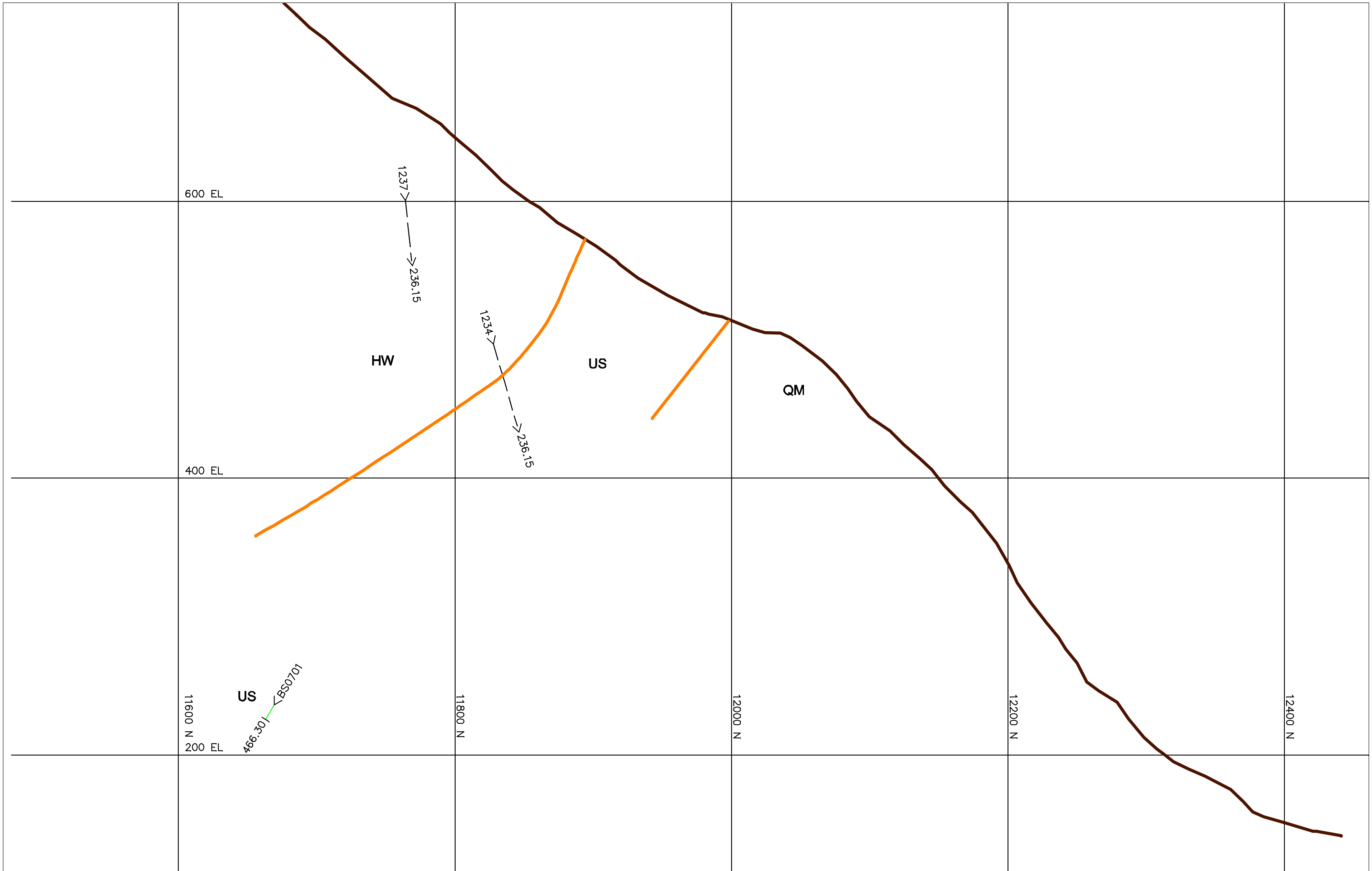
ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25100 E

DRAWN BY	DATE	PRODUCED AT
AB	JAN 10	1:4,000



GEOLOGY LEGEND

- **HW** HANGINGWALL SEDIMENTARY ROCKS
- **US** UPPER SEDIMENTARY ROCKS
- **QM** QUARTZ MAGNETITE BRECCIA
- **PPY** RED BLUFF PORPHYRY
- **LS** LOWER SEDIMENTARY ROCKS
- CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

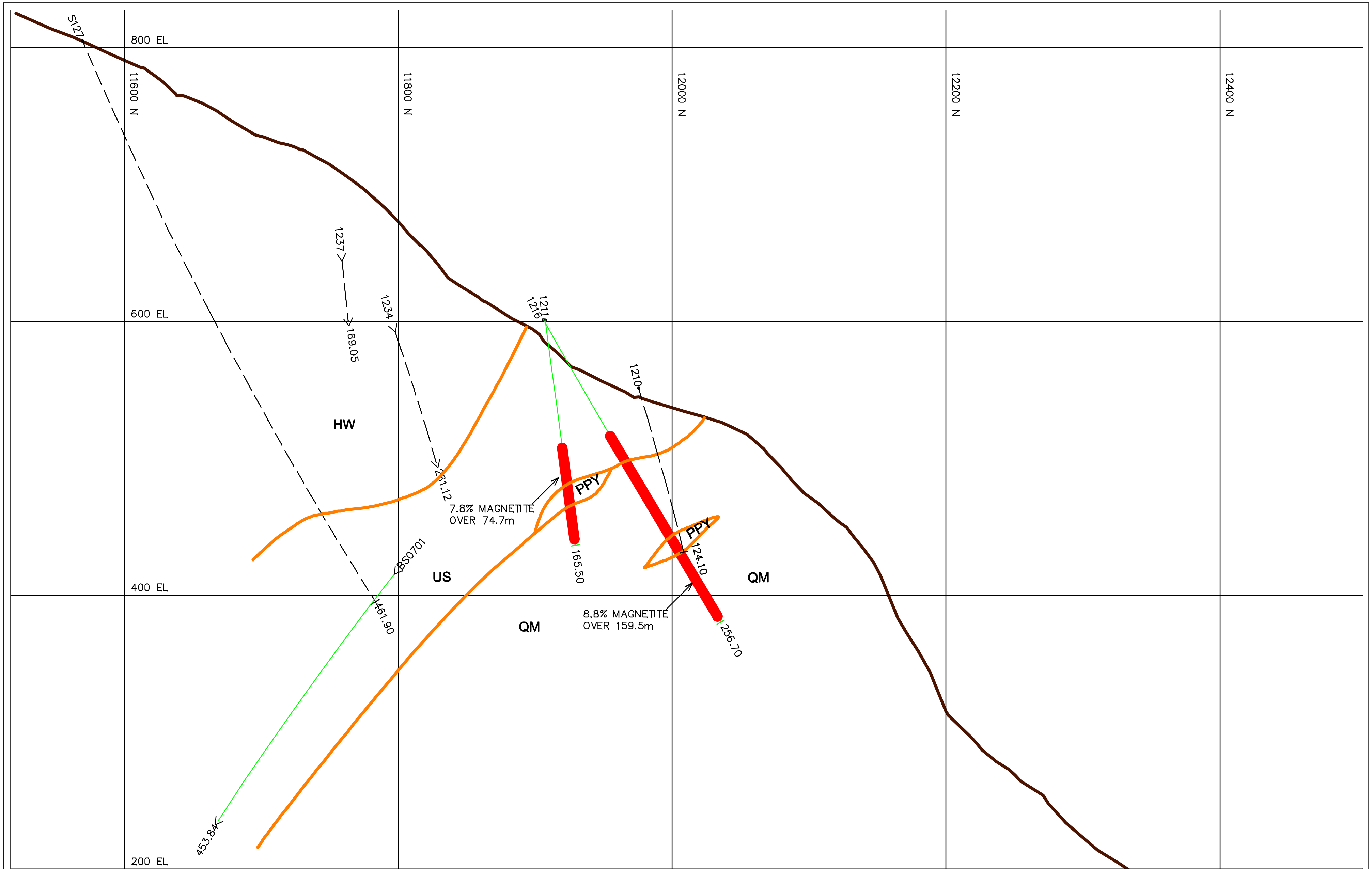
0 50 100 150 200m

SYMBOL KEY

ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.		
DRILL SECTION 25150 E		
DRAWN BY AB	DATE JAN 10	PRODUCED AT 1:4,000



GEOLOGY LEGEND

HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25200 E

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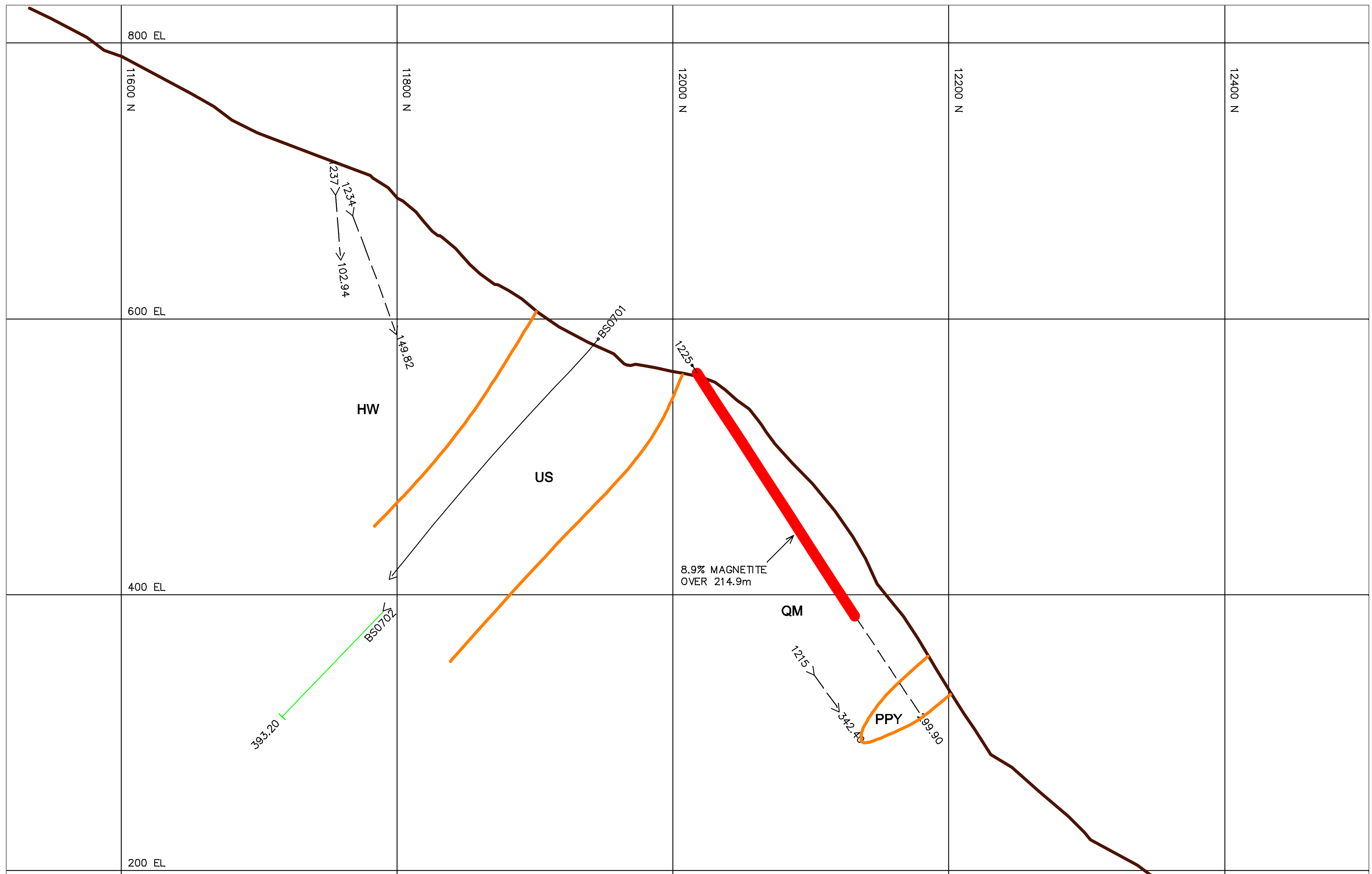

GEOLOGY LEGEND

HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25250 E

DRAWN BY	DATE	PRODUCED AT
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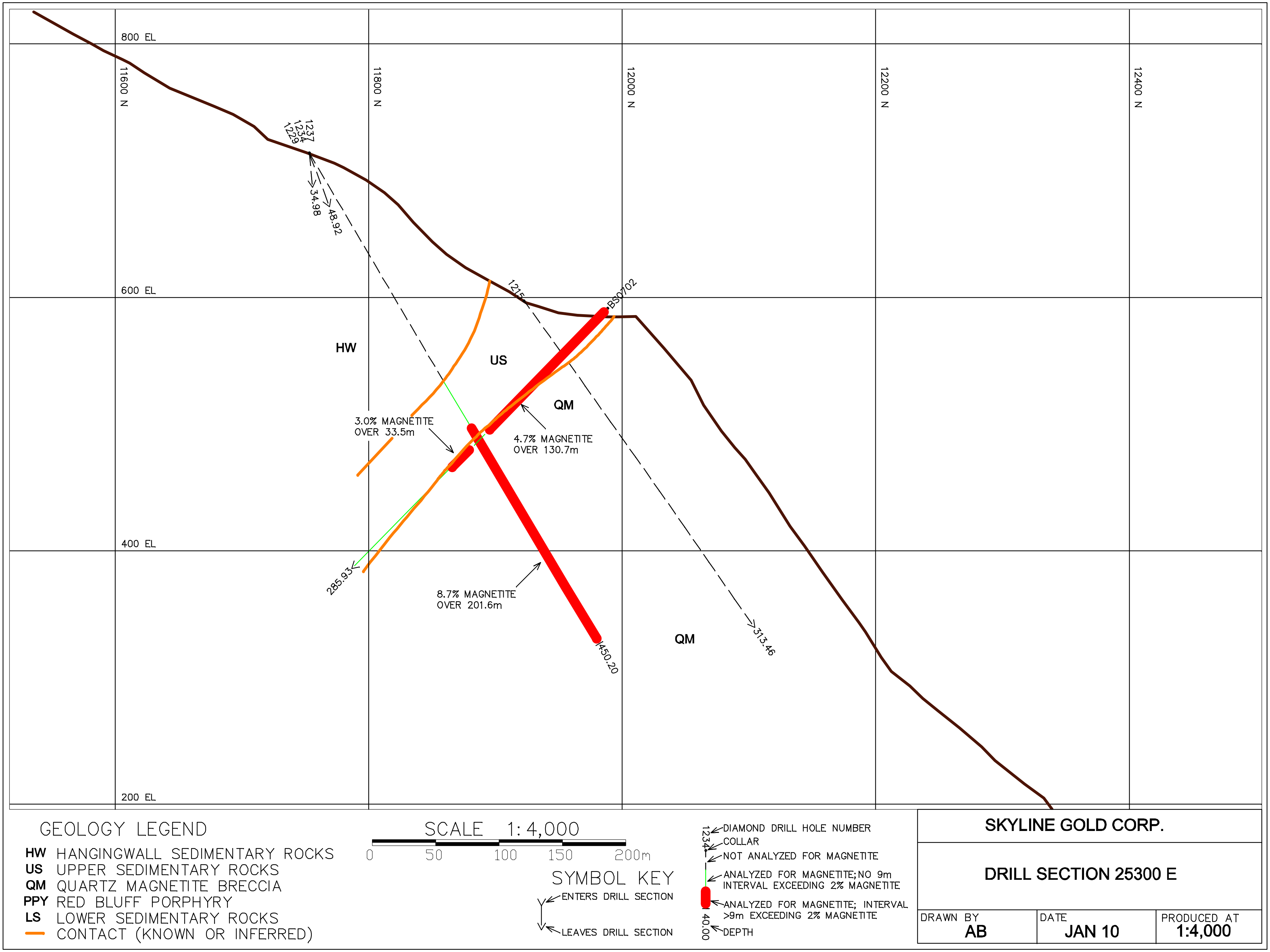
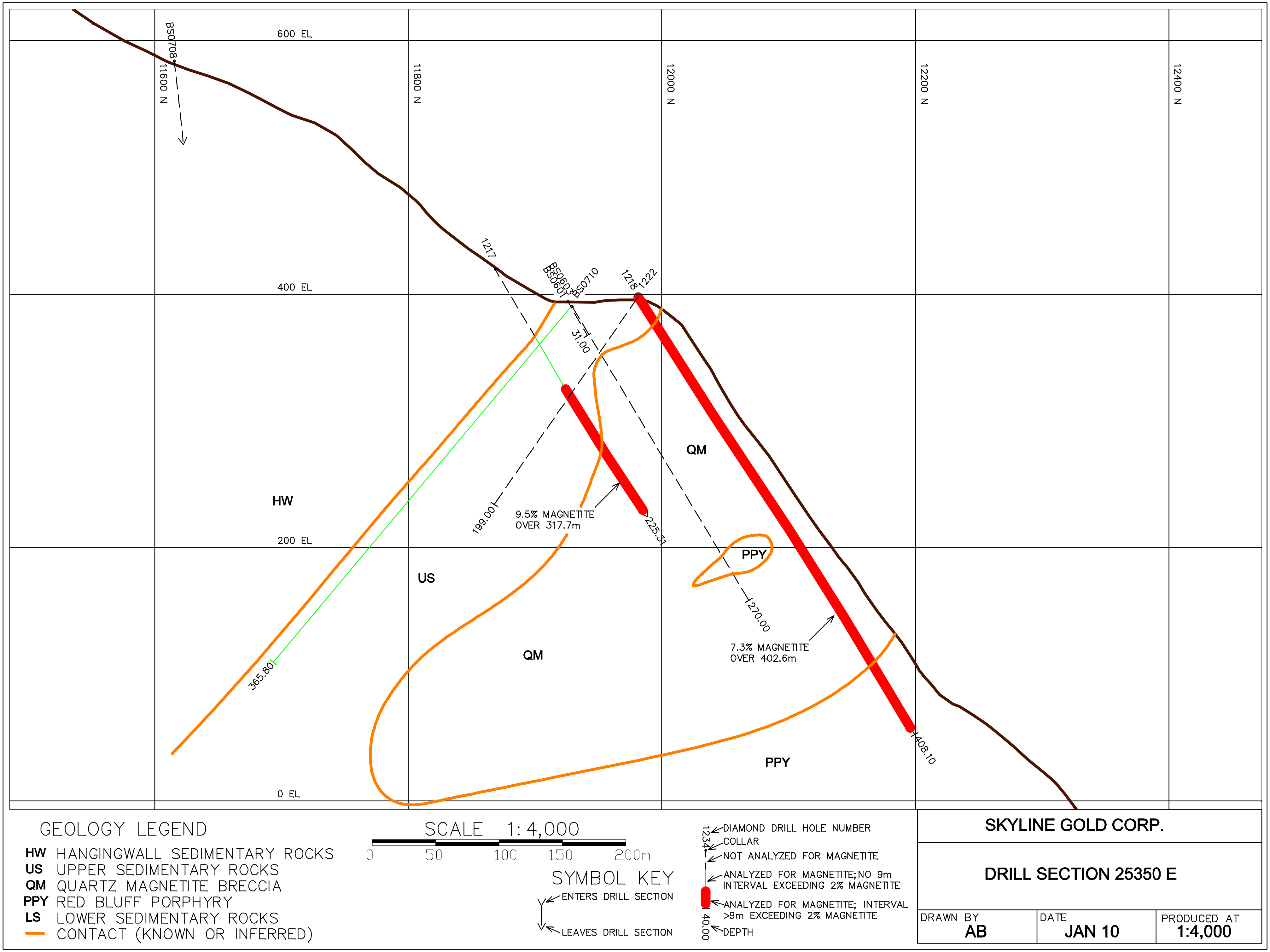
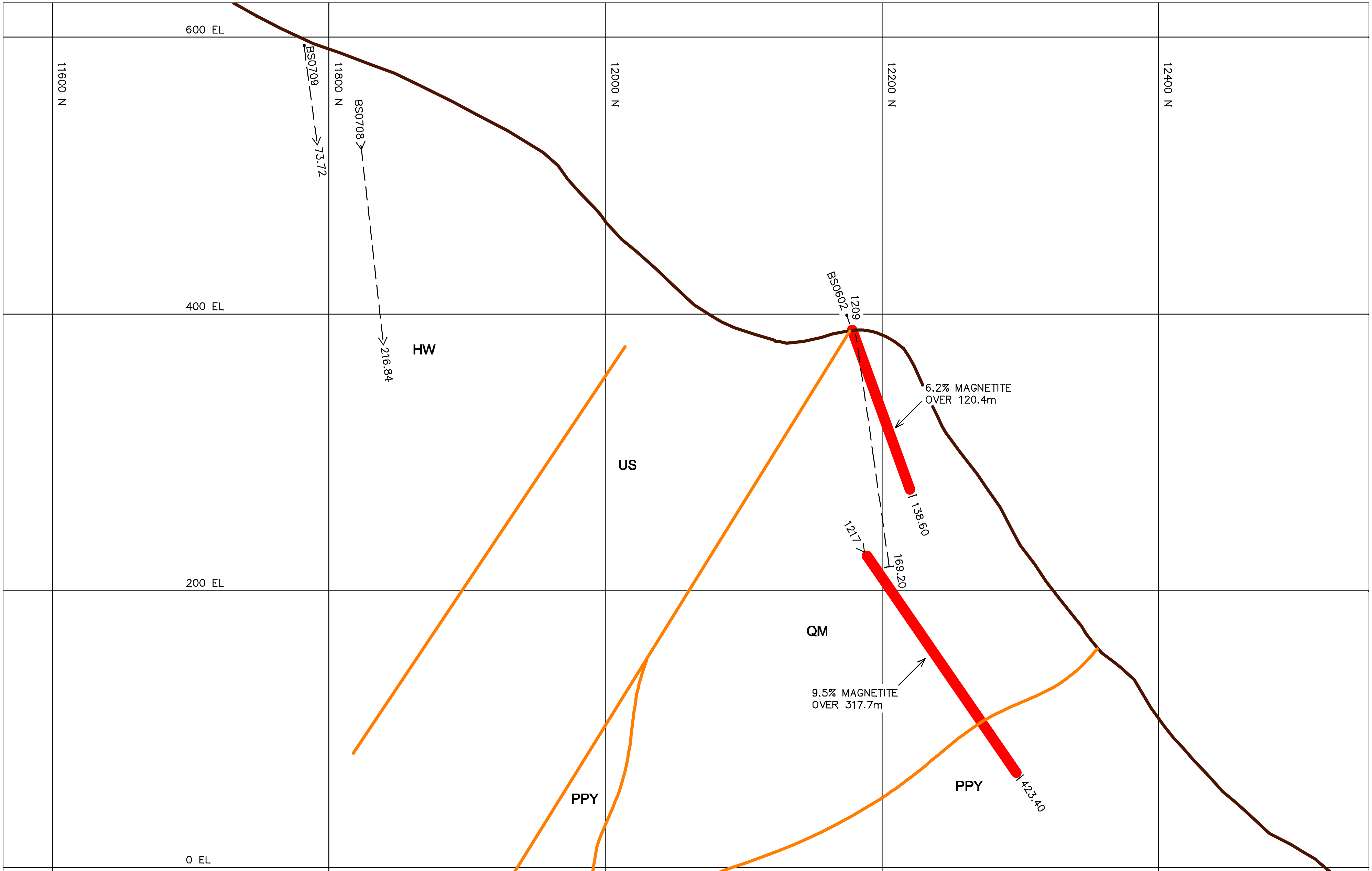

800 EL
600 EL
400 EL
200 EL
11600 N
11800 N
12000 N
12200 N
12400 N
1237
1234
1229
34.98
48.92
1215
BS0702
HW
US
QM
3.0% MAGNETITE
OVER 33.5m
4.7% MAGNETITE
OVER 130.7m
285.93
8.7% MAGNETITE
OVER 201.6m
450.20
QM
313.46
GEOLOGY LEGEND
HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)
SCALE 1: 4,000
0 50 100 150 200m
SYMBOL KEY
ENTERS DRILL SECTION
LEAVES DRILL SECTION
1234
DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00
DEPTH
SKYLINE GOLD CORP.
DRILL SECTION 25300 E
DRAWN BY AB
DATE JAN 10
PRODUCED AT 1:4,000



600 EL
400 EL
200 EL
0 EL
11600 N
11800 N
12000 N
12200 N
12400 N
BS0708
1217
BS0603
BS0601
BS0710
1218
1222
31.00
199.00
225.31
270.00
365.80
408.10
9.5% MAGNETITE OVER 317.7m
7.3% MAGNETITE OVER 402.6m
HW
US
QM
QM
PPY
PPY
GEOLOGY LEGEND
HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)
SCALE 1: 4,000
0 50 100 150 200m
SYMBOL KEY
ENTERS DRILL SECTION
LEAVES DRILL SECTION
1234
DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00
DEPTH
SKYLINE GOLD CORP.
DRILL SECTION 25350 E
DRAWN BY AB
DATE JAN 10
PRODUCED AT 1:4,000



GEOLOGY LEGEND

- **HW** HANGINGWALL SEDIMENTARY ROCKS
- **US** UPPER SEDIMENTARY ROCKS
- **QM** QUARTZ MAGNETITE BRECCIA
- **PPY** RED BLUFF PORPHYRY
- **LS** LOWER SEDIMENTARY ROCKS
- CONTACT (KNOWN OR INFERRED)

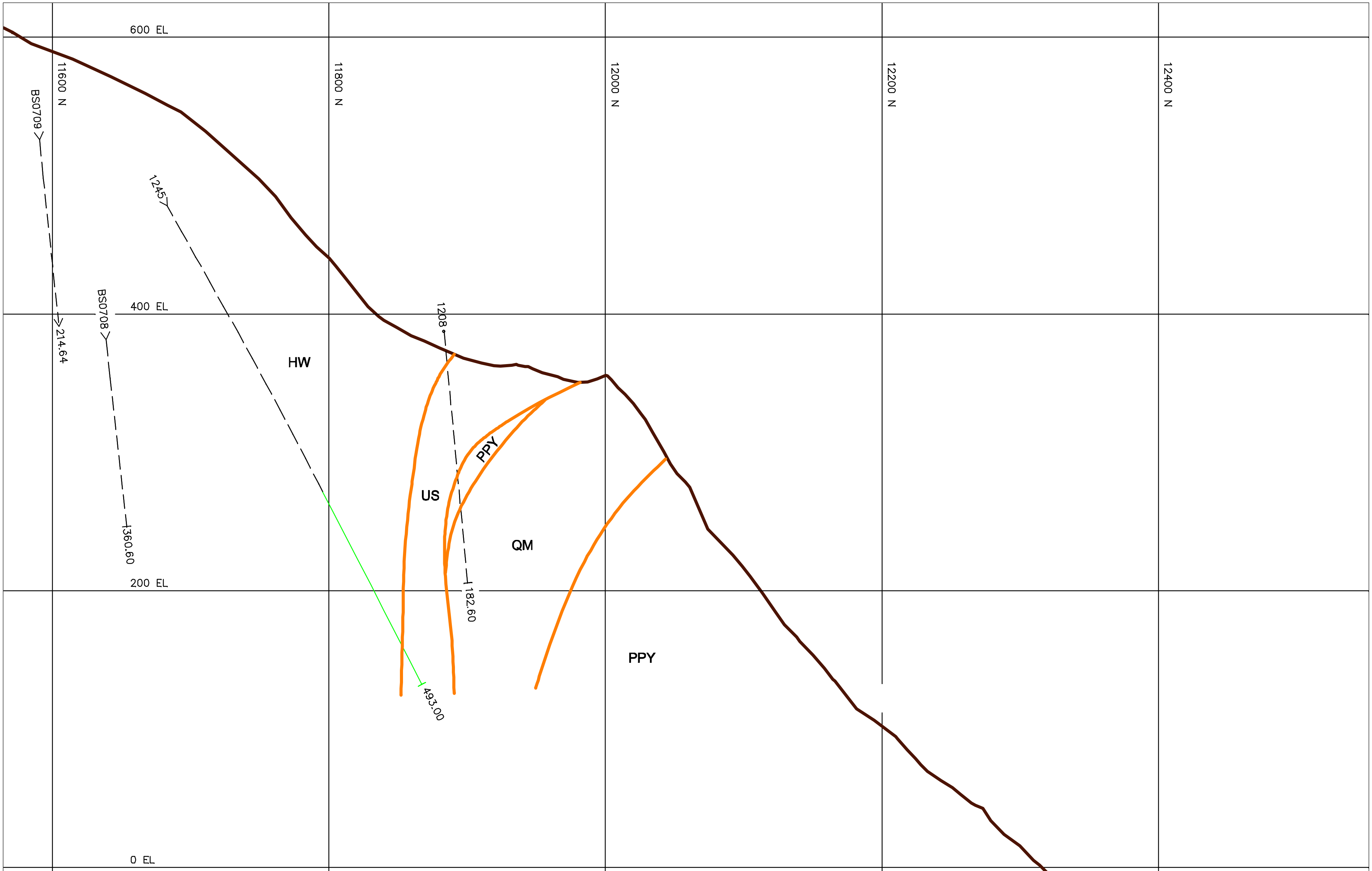
SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

- ENTERS DRILL SECTION
- LEAVES DRILL SECTION
- 1234 DIAMOND DRILL HOLE NUMBER
- COLLAR
- NOT ANALYZED FOR MAGNETITE
- ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
- ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
- 40.00 DEPTH

SKYLINE GOLD CORP.		
DRILL SECTION 25400 E		
DRAWN BY AB	DATE JAN 10	PRODUCED AT 1:4,000



GEOLOGY LEGEND

HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

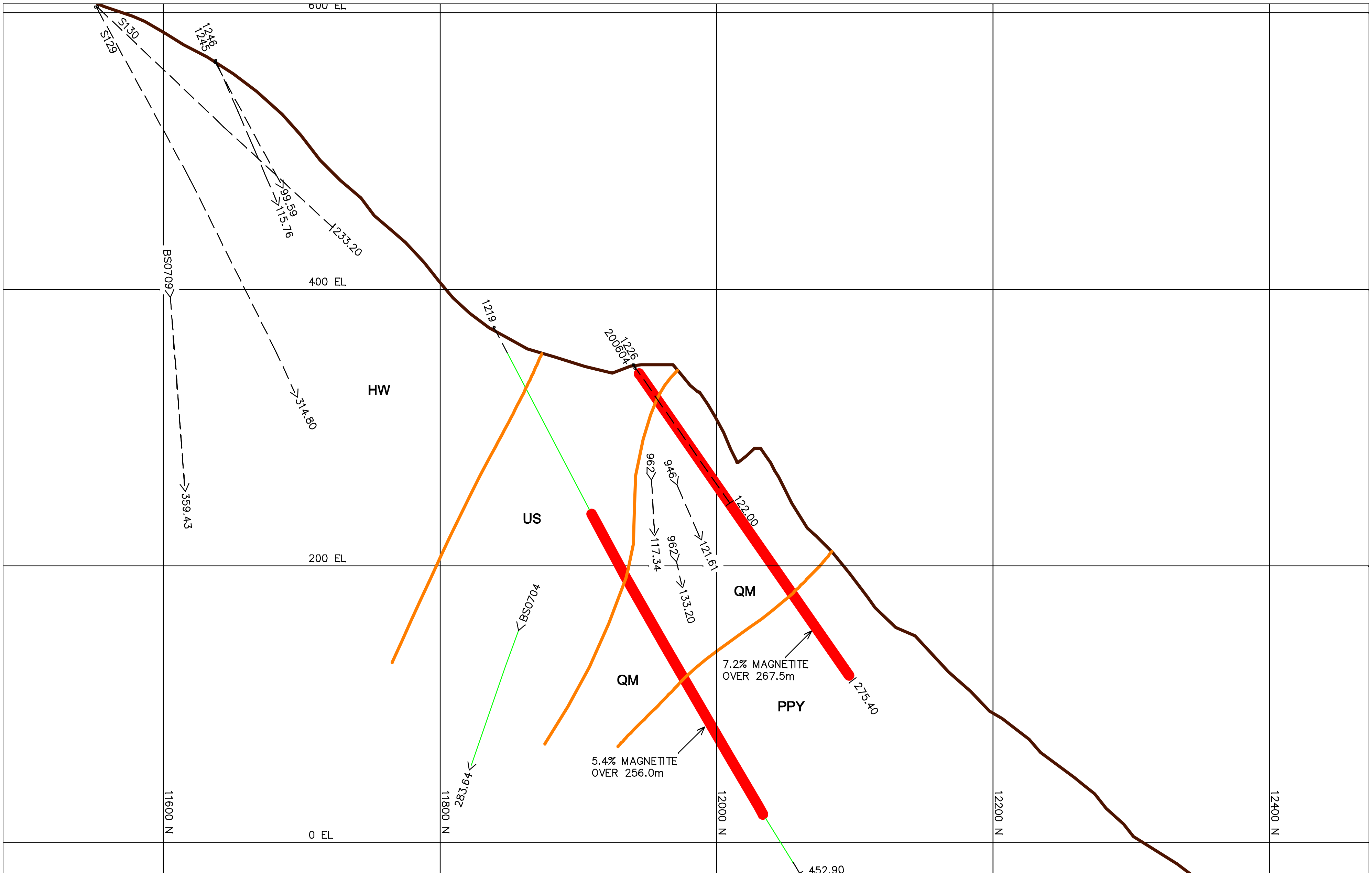
ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25450 E

DRAWN BY	DATE	PRODUCED AT
AB	JAN 10	1:4,000



GEOLOGY LEGEND

HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25500 E

DRAWN BY	DATE	PRODUCED AT
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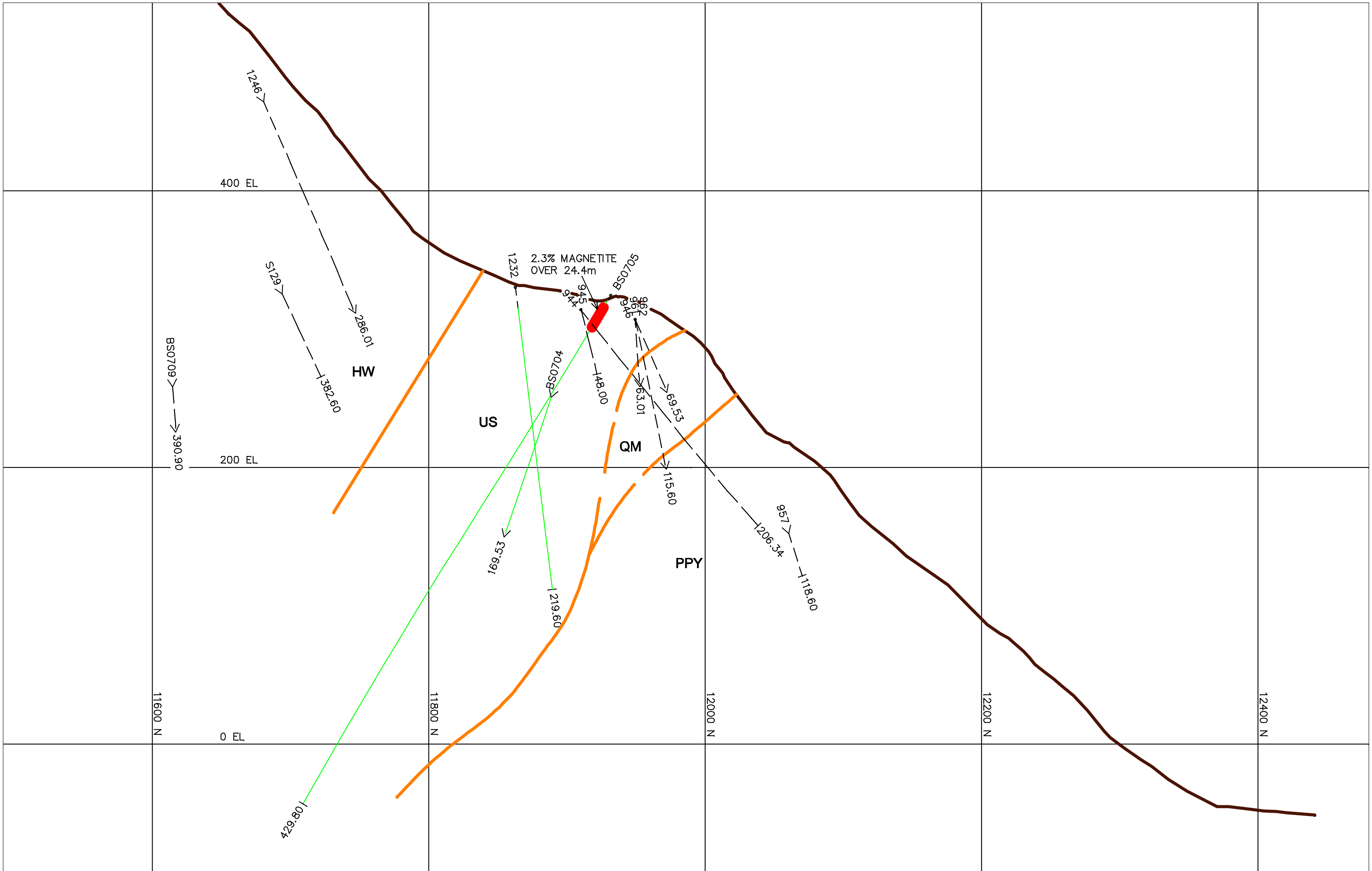

GEOLOGY LEGEND

HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25550 E

DRAWN BY	DATE	PRODUCED AT
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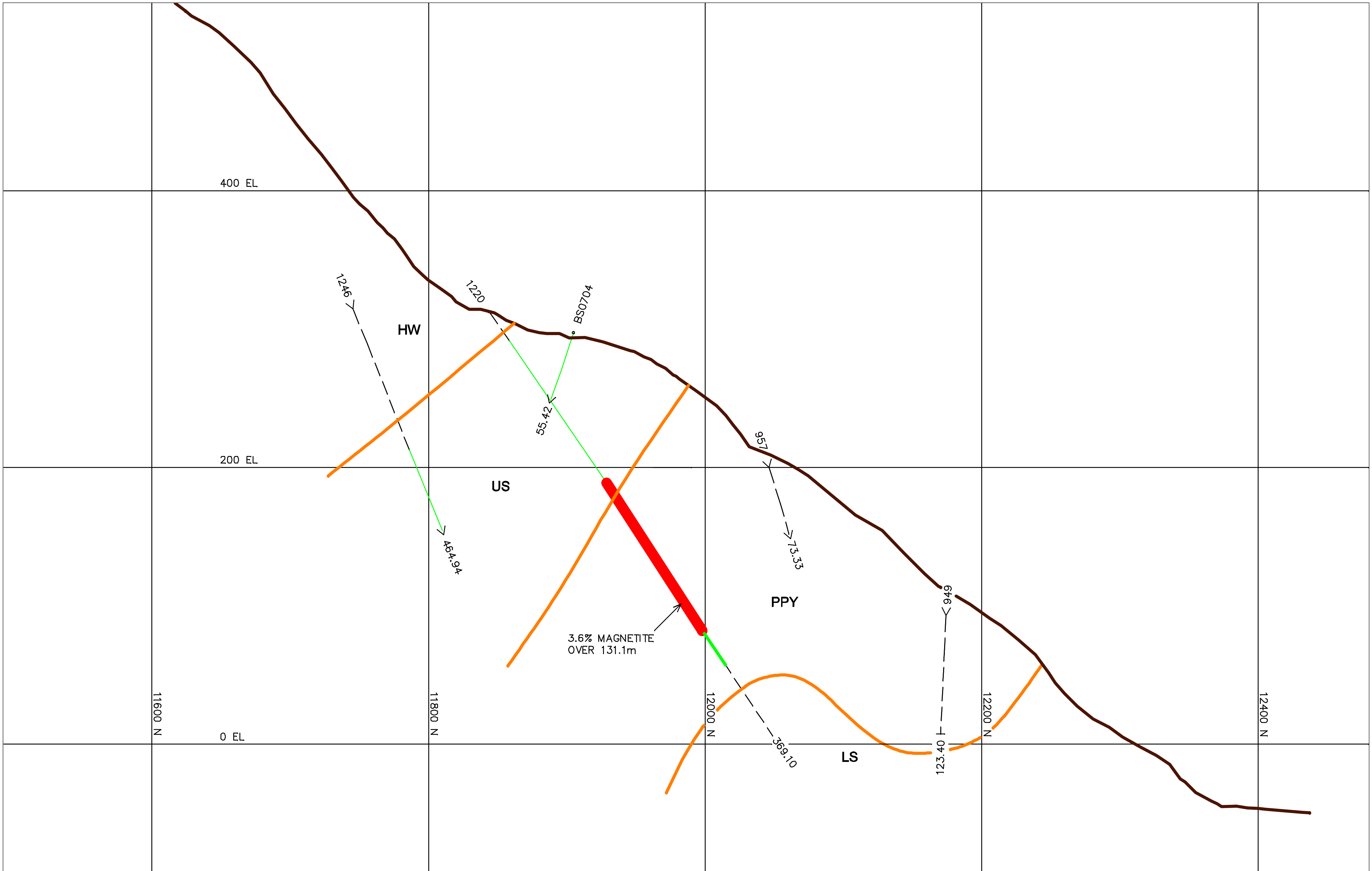


GEOLOGY LEGEND

HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

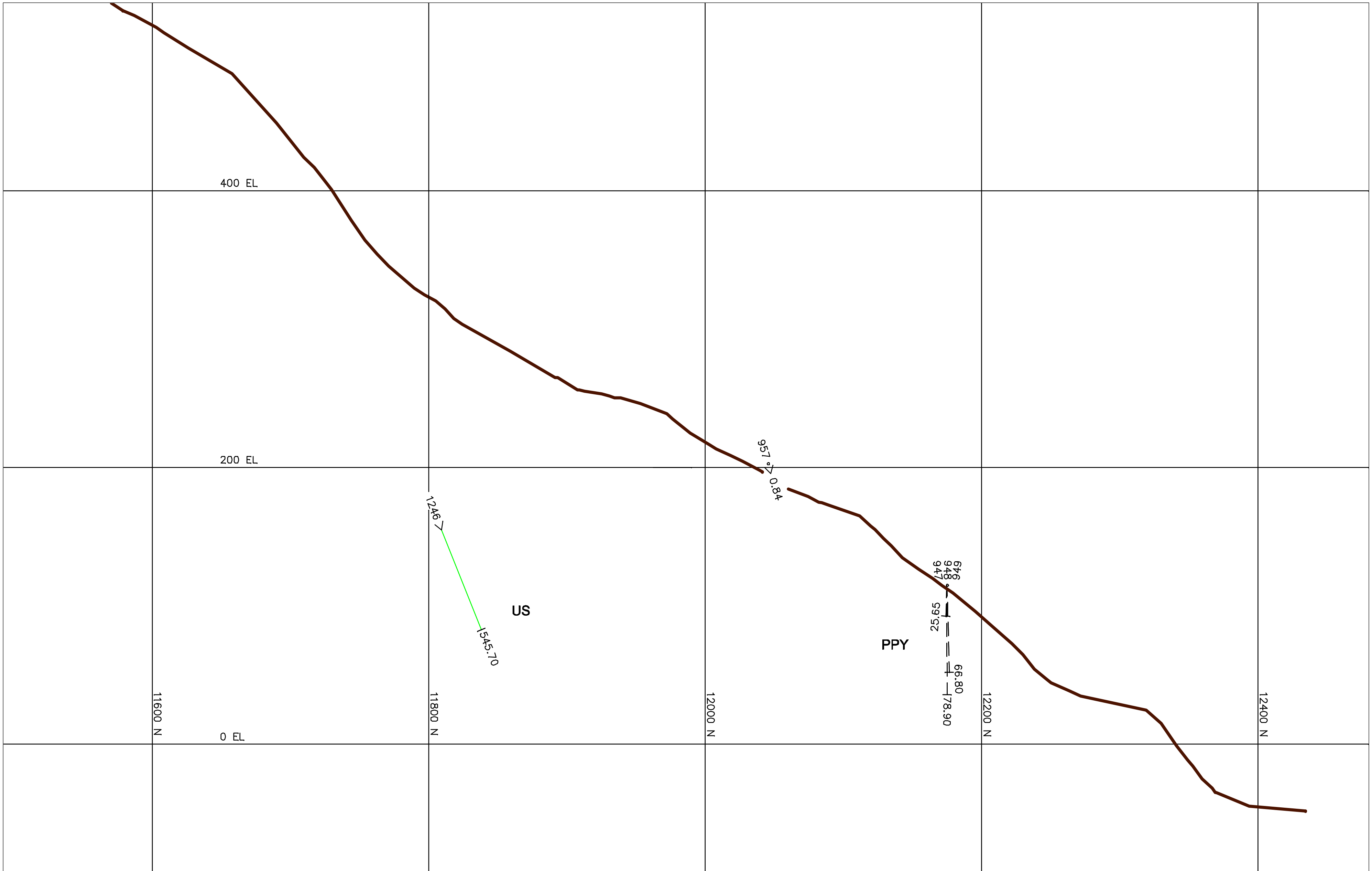
ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25600 E

DRAWN BY	DATE	PRODUCED AT
AB	JAN 10	1:4,000



GEOLOGY LEGEND

HW HANGINGWALL SEDIMENTARY ROCKS
US UPPER SEDIMENTARY ROCKS
QM QUARTZ MAGNETITE BRECCIA
PPY RED BLUFF PORPHYRY
LS LOWER SEDIMENTARY ROCKS
CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

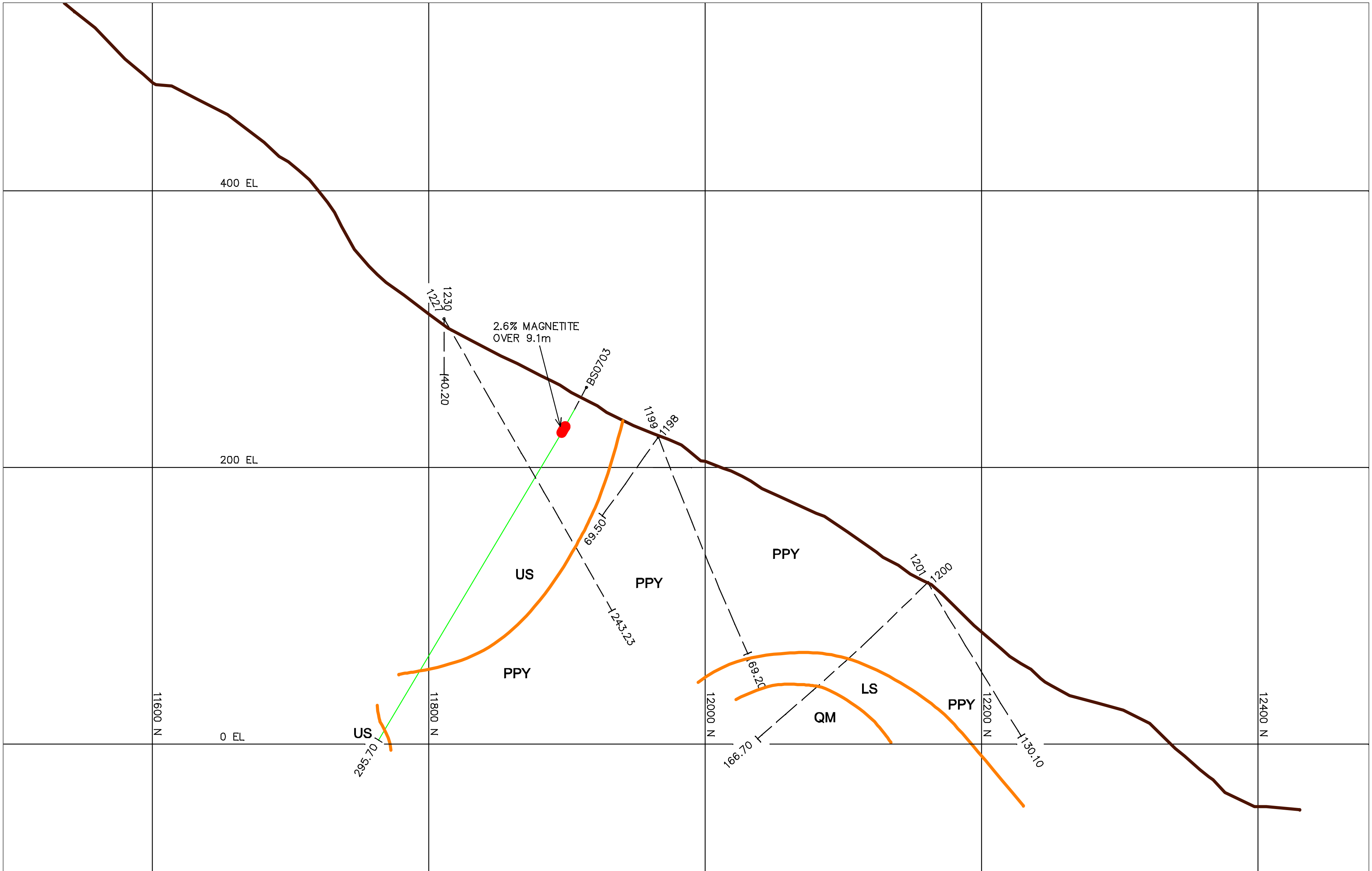
ENTERS DRILL SECTION
LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER
COLLAR
NOT ANALYZED FOR MAGNETITE
ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE
ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE
40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25650 E

DRAWN BY	DATE	PRODUCED AT
AB	JAN 10	1:4,000



GEOLOGY LEGEND

- **HW** HANGINGWALL SEDIMENTARY ROCKS
- **US** UPPER SEDIMENTARY ROCKS
- **QM** QUARTZ MAGNETITE BRECCIA
- **PPY** RED BLUFF PORPHYRY
- **LS** LOWER SEDIMENTARY ROCKS
- CONTACT (KNOWN OR INFERRED)

SCALE 1: 4,000

0 50 100 150 200m

SYMBOL KEY

ENTERS DRILL SECTION

LEAVES DRILL SECTION

1234 DIAMOND DRILL HOLE NUMBER

COLLAR

NOT ANALYZED FOR MAGNETITE

ANALYZED FOR MAGNETITE; NO 9m INTERVAL EXCEEDING 2% MAGNETITE

ANALYZED FOR MAGNETITE; INTERVAL >9m EXCEEDING 2% MAGNETITE

40.00 DEPTH

SKYLINE GOLD CORP.

DRILL SECTION 25700 E

DRAWN BY	DATE	PRODUCED AT
AB	JAN 10	1:4,000

12.0 Sampling Method and Approach

The drill core sampled for the 2009-magnetite resource evaluation, summarized in **Table 11-1**, was obtained by diamond drilling during previous years. Core handling protocols applied during the previous years' drill campaigns, described by Burgoyne and Giroux (2008), followed industry practices typical of those years during which the drilling took place. Samples for 2009 magnetite analyses were derived from two sources: drill core stored at Bronson Airstrip, and drill core pulps stored at the assay laboratory.

12.1 Drill Core

Diamond drill core was found in good condition at core storage racks located 70m northwest of the Bronson Airstrip, 550m from the airstrip's southwestern end. The core is stored in standard core boxes 1.5m (5') in length.

Core boxes were sequentially removed from the core storage racks and transported by flatbed truck to Skyline's core handling facility located about 100m northwest of the Bronson Airstrip, approximately midway along the strip. Once at the core handling facility, core boxes were laid out on benches, and a Terraplus KT-10 magnetic susceptibility meter was used to take a magnetic susceptibility measurement every meter along the core length. Magnetic susceptibility measurements were recorded in SI units.

Next, technicians identified the depth intervals to be sampled, referring to a sample log that had been prepared for each hole. Intervals were marked by stapling a two-part assay tag onto the core box at the start of each interval. Most samples consist of 3m of core length. For each hole, the place for insertion of standards, blanks, and field duplicates into the sample stream was predetermined on the sample log, and assay tags for these were inserted into the core boxes accordingly. For standard, blank, and duplicate assay tags, the portion remaining in the core box was labelled as standard, blank, or duplicate, while the portion to be submitted to the laboratory was unmarked. Details on Skyline's QA/QC protocols are reported in **Item 14.0**. Core boxes with attached assay tags were then stacked aside until a core sampler was available to sample the core. Accuracy of the KT-9 magnetic susceptibility instrument was checked by using a Scintrex DM5 instrument to take duplicate measurements along a 51 were made by metre section of drill core from Hole 1221. The correlation between the two meters, shown on the plot included at the end of Appendix C, is good. The KT-9 instrument readings are comparable to the DM5."

Most of the core had been split in half and sampled for the gold-silver-copper-molybdenum resource evaluation during previous years, so during the 2009 program the remaining half was quartered. Exceptions are holes 1211, 1216, and 1232. These three holes had already been quartered for metallurgical testing, and as a result could not be meaningfully split again. During 2009, samples from holes 1211, 1216, and 1232 were made, by consuming the entire remaining core.

For all holes except 1211, 1216, and 1232, each core sample was made by using one of four core splitters to break the existing core half into two quarters. One quarter was placed back into the core box as reference, and the other quarter was placed into a polyethylene sample bag. When an entire sample interval had been split and one quarter placed into the sample bag, one portion of the two-part assay tag marking the sample interval was added into the sample bag to identify the sample, while the other half of the sample tag remained stapled in the core box. The bag was closed using a plastic ladder-lock cable tie.

Sampled core boxes were loaded back onto the flatbed truck and returned to the core racks. Completed and sealed samples were packed, in sequential order, into woven polyethylene textile sacks (rice sacks) for shipment to the laboratory. A freight scale was used to standardize sack weights, simplifying later aircraft payload allowance calculation. Sacks were double sealed with a ladder lock cable tie and a numbered locking security (NLS) tie. Each sack's NLS serial number was recorded along with the sample sequence enclosed in each sack.

Samples were stored in a locked sample storage shed behind the core shack until a cargo flight was available. All core sample sacks, except one load, were flown by fixed wing aircraft from the Bronson Airstrip directly to Smithers Airport. The planes were met by personnel from either Skyline's expediter, Blue Bear Exploration Ltd., or from the laboratory, Assayers Canada. Blue Bear or Assayers Canada personnel then took possession of the samples at the airport and delivered them to the Assayers Canada sample preparation laboratory located at 1387 Birch Street in Telkwa, B.C. One load of sample sacks was flown from Bronson Camp by helicopter to a secure storage facility at Quantum Helicopter's base located at km 2 of the Eskay Road, near Bob Quinn Lake. This load was then picked up by personnel from Black Hawk Drilling Ltd. for transport by truck to Smithers. At Smithers, the sample sacks were passed to Blue Bear exploration that in turn passed them to Assayers Canada personnel for delivery to the laboratory.

12.2 Pulps

Crushed and pulverized core pulps from a series of 2006/ 2007 drill holes (see **Table 11-1**) were available from storage at Acme Analytical Laboratories (Canada) Ltd. in Vancouver (Acme), where the previous suite of analyses had been performed. Accordingly, drill core from this series of drill holes was not quartered in the field. The pulps were forwarded by Acme to the analytical laboratory for magnetite analysis.

12.3 Historical and 2007 & 2006 Diamond Drilling for Copper, Gold, Silver & Molybdenum

Bronson Slope sampling data includes surface core drilling results for copper, gold, silver and molybdenum and used in resources estimates are detailed in Burgoyne and Giroux (2008), Burgoyne and Giroux (2007) and Burgoyne (2006). This drill core was completed by Skyline in the periods of 1988 and 1993 through 1997, 2006 and 2007, and historic drilling by Cominco and Prime Resources in 1965, 1986 and 1994. All drill data, excluding the Cominco 1965 drilling, was used to define the current resource estimate completed and reported in early 2008 (Burgoyne and Giroux 2008).

Diamond Drilling 2007 and 2006

Skyline core diamond drilling in 2007, all of NQ core size, was completed by Blackhawk Drilling of Smithers, BC. The 2006 drilling, Phils Drilling and Boart Longyear completed all of HQ core size. The core, for both years, was moved by the drilling contractor via helicopter to the core logging facility at Bronson Creek airstrip where a team consisting of a Skyline geologist and technicians logged, including RQD data, and photographed the drill core in detail. It was subsequently marked, split, sampled, bagged, and packed. Technicians split the drill core with a Longyear diamond drill core splitter. The sampling interval averaged 3 metres continuous intersections, which were bagged, labeled and secured, placed in sacks, and then forwarded, in 2006, by aircraft to Acme Laboratories in Vancouver, BC. In 2007 the core was sent to Bob Quinn on the Cassiar Stewart Highway by aircraft and thence by truck (Bandstra Transportation) to the Acme laboratories preparation laboratory in Smithers, BC. The analyses and assays were gold, copper, silver and molybdenum. The Core Handling Procedure (Delong 2006a) was developed prior to the drilling and included a detailed protocol on laying out core, geotechnical logging, sample layout including standard and blank sample insertions, and core logging procedures on descriptive terminology for alteration and lithology, type of structures, mineralization, veins and styles/types, and storage of core. The core, at all time, was under direct supervision of Skyline personnel and kept in a secure and locked core logging building.

Diamond Drilling 1988 & 1993 - 1997

Skyline diamond drill core from surface, mostly of BQ core size, (1988, 1993 through 1996) and some NQ core size (1997) was completed by Falcon, Boisenvu, Olympic, and JT Thomas Drilling over this period of time. The drill core in 1988 was moved from the respective diamond drill setup by helicopter to the Red Bluff exploration camp where it was logged and split. In 1993 the drill core was taken from the drill sites to the main Johnny Mountain mine site. In the period of 1994 through 1997 the core was moved by the drilling contractor via helicopter to an exploration campsite on the north end of the Bronson Creek airstrip where a team of Skyline geologists logged, including RQD data, and photographed the drill core in detail. It was subsequently marked, split, sampled, bagged, and packed. Technicians split the drill core with a Longyear diamond drill core splitter. The sampling interval varied from 1.5 to 4-metre, and averaged 3 metre range, continuous intersections, which were bagged, labeled and secured, placed in sacks, and then forwarded by aircraft to the Rossbacher Laboratories in Burnaby, BC, and where applicable, to Chemex Labs in North Vancouver, BC. The analyses and assays were predominantly gold, copper, silver and molybdenum, and in certain cases, other metals were completed. The above information is given by Yeager (2006)

In 1997 the former Cominco and Prime Resources drill core, acquired by Skyline, was re-sampled (quartered where previously assayed) and un-assayed portions were split and assayed at Chemex Labs Ltd.

The surface drilling, logging, and sampling procedures were essentially constant over the continuous five-year drilling period.

13.0 Sample Preparation, Analyses & Security

13.1 Drill Core

All drill core samples were submitted to the Assayers Canada sample preparation lab in Telkwa, BC, where samples were logged according to the security protocol described in **Item 13.3.1**. Samples were then dried, weighed, crushed, and split using a riffle splitter. The coarse reject fraction was placed into secure storage at the Assayers Canada Telkwa facility, while the split fraction was forwarded to the Assayers Canada facility in Vancouver for pulverization.

Once crushed splits were received at Assayers Canada's Vancouver facility, the routine procedure involved pulverizing for 90 seconds and sieving through a 150-mesh size screen. A riffle splitter was then used to obtain a representative 200g split. The split pulp samples were forwarded to Met-Solve Metallurgical Laboratories in Burnaby, BC (Met-Solve) for analysis.

An orientation program was performed by Assayers Canada and Met-Solve to determine the pulverization time for optimal magnetite liberation and the sub sample size for optimal magnetite recovery. The orientation study is described in **Item 13.1.1**.

The magnetic separator used for the magnetite analyses is a Davis Tube apparatus. The analytical procedure involves first weighing out a 20-gram dry pulp sample into a beaker and adding enough water to wet and cover the dry pulp sample. The discharge end of the Davis Tube is clamped off, and the Davis Tube filled with enough water to cover the magnet poles. The magnet is turned on and the slurry sample washed into the Davis Tube. The discharge hose clamp is unclamped to regulate a steady flow of water through the Davis Tube, and the tube is then agitated for two minutes, allowing the slimes or cloudiness to be washed out of the tube. Magnetic material is attracted and held fast in the magnetic zone between the two magnet poles. After two minutes the agitator is stopped, the magnet turned off, and the magnetic fraction flushed to the bottom of the tube. The magnetic material is then collected through the discharge tube, dried, and weighed to determine the percentage of magnetic material.

13.1.1 Magnetite Analyses Orientation Study

Met-Solve prepared laboratory standard material from a sample of Bronson Slope drill core that had been collected for a metallurgical study in 2008. The material was used to prepare fifty-six standard samples to determine the pulverization time for optimal magnetite liberation and the sub sample size for optimal magnetite recovery. Of the fifty-six standard samples, half were pulverized for each of 90 seconds and 120 seconds. Each of these two subsets was then split into three additional subsets for analysis of 10g, 15g, and 20g samples.

The shorter (90 second) pulverization time consistently gave very slightly higher assay values. The standard deviation among assay values of 10g sub samples was higher than the standard deviation of the 15g sub sample set. The standard deviation among the 20g set was similar to that among the 15g set.

Based on these data, the 90-second pulverization and 15g sub sample were selected as the routine parameters. However, review of the initial batch of 56 core pulp samples revealed lower than expected repeatability among laboratory duplicates and laboratory repeats, so further analyses used 20g sub samples. Repeatability improved markedly using 20g sub samples, and the larger sub sample size was adopted for all remaining analyses.

The series of ten standard samples from the orientation study subjected to 90-second pulverization of 20g samples is included in the data set used for statistical analysis of laboratory standards, described in **Item 14.3.6**.

13.2 Pulps

The pulps obtained from Acme had been prepared from drill core in 2006 and 2007 according to the following methodology. The diamond drill core and the respective standards and duplicates were delivered to Acme in Vancouver, BC where laboratory staff assumed the chain of custody of the samples. Acme is an ISO 9001:2000 accredited company using accepted and good quality analytical technology and protocol with respect to current industry standards. The samples were recorded, dried, crushed, and split. The split portion was then ground or pulverized. Standard sample procedure during this process involved pulverization of split core so that 1 kg is crushed to 70% passing a No. 10 mesh size sieve screen with a 250 gram split pulverized to 95% passing a No. 150 mesh.

During the 2006 and 2007 programs, Skyline had used a blank standard for gold and five separate standards for gold, copper, molybdenum, and silver that were inserted as rock pulps into the sample chain in the field. Before submitting the series of 2007 pulps for magnetite analyses, Skyline supplied Met-Solve with a series of standard QA/QC pulps for magnetite, including a supply of magnetite blank and two magnetite standards. Assayers Canada then removed all 2007 gold, copper, and molybdenum standards from the sample stream, replacing each with one of the new magnetite standards.

The new series of pulps was then submitted for magnetite analysis following the procedure described in **Item 13.1**.

13.3 Sample Security

13.3.1 Core Sample Security

For all core samples processed during 2009, Skyline implemented a chain of custody procedure to ensure sample security. Drill core was handled at Skyline's core facility at Bronson Camp where doors were locked when unattended. Once packed in rice sacks, completed samples were stored in a locked sample storage shed behind the core shack. Following sample transport by air, samples were either taken into possession by trusted personnel or held in secure storage until delivered to Assayers Canada where laboratory staff assumed custody.

Assayers Canada is an ISO 9001:2008 certified laboratory. Samples were submitted to Assayers Canada in rice sacks sealed with numbered locking security (NLS) ties. As laboratory personnel unpacked each rice sack, the NLS serial number was recorded along with the sample sequence therein contained. This information was sent by Email to the Project Geologist for verification against the data in the sample log.

13.3.2 Pulp Security

Core and sample security, up to the point of the 2007 analyses, is described by Burgoyne and Giroux (2008) as noted in **Item 13.4**. After the 2007 analyses were performed, secure custody of the sample pulps was retained by Acme until they were shipped to Met-Solve in 2009, where Assayers Canada staff took custody of the pulps.

13.4 Sample Preparation & Analyses 2007, 2006, and Historical Drilling

This is detailed in Burgoyne and Giroux (2008) at www.sedar.com.

The authors are of the opinion that the techniques and analytical methods used by the Skyline external labs, at the time, were "state of the art" and were effective in determining accurately the amounts of gold, copper, silver, and molybdenum in the mineralized drill core.

13.5 Site Security and Chain of Custody for 2007, 2006, and Historical Drilling

During the 2007 and 2006 drilling programs the site security was documented and a protocol was developed as part of the Quality Assessment and Quality Control (QA/QC). A sampling/chain of custody was adhered to as outlined in Delong (2006b). This is detailed in Burgoyne and Giroux (2008).

The pre 2006 site security at the Johnny Mountain and Bronson airstrip exploration camps is not documented; it is assumed that they followed normal mining company security standard of the time, which was strict. Normally drill core and bagged core samples were kept in a secure room or place. The chain of custody for the samples would be from the exploration personnel at the camps to commercial transport personnel and finally to the laboratory personnel in the respective analytical laboratories as documented in Item 12.3.

14.0 Data Verification

Background

Quality Control and Quality Assurance Programs for the 2007 and 2007 drilling which were directed toward the definition of gold-silver-copper-molybdenum mineralization grade are detailed in Burgoyne and Giroux (2008) and given on www.sedar.com and are not repeated here. These programs included inserted standards, duplicate sample insertion, check analyses, and laboratory internal standards. Likewise the Quality Assurance Programs for pre 2006 (historical) drilling are detailed in Burgoyne and Giroux (2007) and given on www.sedar.com and are not repeated here.

14.1 Quality Control and Quality Assurance Program for 2009 Magnetite Sampling Program

During the course of Skyline Gold's Magnetite Sampling Program 2,255 samples were analyzed, including 1,232 diamond drill core samples, 745 pulp samples, and 278 samples comprising the Quality Control and Quality Assurance (QA/QC) Program. Protocols followed for the QA/QC program are described in **Item 14.2**, and results are presented in **Item 14.3**. The following six types of samples were prepared and analysed as QA/QC checks, by either Skyline field personnel or the assay lab:

- Field blanks;
- Field duplicates;
- Field standards;
- Laboratory duplicates;
- Laboratory repeats;
- Laboratory standards.

The QA/QC program indicates that no significant analytical problems were encountered, and no contamination of samples occurred. The assay values as reported are considered reliable.

14.2 QA/QC Protocols

14.2.1 Field Blank Protocol

Field blanks were inserted into the sample stream to test for contamination of samples at any stage of handling and analysis. Blank samples are meant to contain none of the commodity being analyzed, and the analysis values returned by the lab are expected to be below the detection limit. An assay value significantly higher than the detection limit would suggest an analytical blunder or sample contamination. Different blanks were used for pulp samples and core samples.

Blank samples inserted into the pulp sample stream were prepared by packaging 70g packs of blank rock pulp supplied by ALS Chemex Laboratory in North Vancouver, BC. These packs were inserted into the sample stream at an interval of approximately every 40th sample, for a total of eleven blank pulps. Since the blank rock pulp was intended for use as a blank for base and precious metals assays, it turned out to contain some magnetite. Accordingly, it did not return values below the detection limit, and the data are not useful as blanks. The data are treated as an additional field standard for the pulp sample set, and results are discussed as Standard 3 in **Item 14.3.3.**

Blanks inserted into the core sample stream were prepared by packaging 200g samples of coarse crushed, non-magnetic, white marble in standard rock sample bags. These packages were inserted into the sample stream at an interval of approximately every 40th sample, for a total of thirty-three blank rock samples. The samples were submitted blind to the lab, where they were prepared and analyzed the same as every other sample.

14.2.2 Field Duplicate Protocol

The purpose of field duplicate samples is to test for analytical precision and repeatability. The value of a duplicate sample analysis is expected to be close to the original analysis value. Due to natural variability of the magnetite concentration throughout the rock formation (and hence drill core), small disparities between initial and duplicate assay values are expected, and not indicative of an analytical problem. A large disparity between initial and duplicate analysis values would suggest an analytical problem.

No field duplicates were available for the pulp series. For the drill core series, field duplicate samples were prepared by sampling half of the available drill core as usual, but rather than replacing the remaining core portion in the core box as a reference, the remaining portion was bagged and prepared as an additional (duplicate) sample. The duplicate sample was submitted blind to the laboratory, where it was prepared and analyzed the same as every other sample. Duplicate samples were prepared approximately every 40th sample, for a total of thirty-five duplicate core samples.

14.2.3 Field Standard Protocol

Field standards were inserted into the sample streams for both pulps and drill core to test for analytical accuracy and repeatability of assays and systemic analytical deviations. Standards of three magnetite concentrations were used.

No prepared standard material for magnetite was commercially available. Material for standards was obtained from two sources. Standards 1 and 2 were prepared before the start of fieldwork by Skyline personnel from rock chips of a rock formation containing fine-grained magnetite. Two batches of magnetite-bearing rock chips were prepared, one of which was blended in a desired proportion with chips of a non-magnetic sandstone formation. The two rock chip batches were then submitted to Acme Analytical Laboratories (Canada) Ltd. in Vancouver, where the entire batches were crushed and pulverized to pass a No. 150 mesh size sieve screen. These were then homogenized by tumbling each batch in a rock sample bag. Standard 3 was in the form of rock pulp obtained from ALS Laboratory Group in North Vancouver, BC (ALS). The ALS standard was intended for use as blank pulp in the stream of pulp samples, but turned out to contain some magnetite, and has therefore been treated as an additional standard.

Standard samples were prepared by packaging 70g packs of the prepared standard material in small paper envelopes. These were then placed in standard rock sample bags and inserted into the sample sequence approximately every 30th sample, for a total of seventy-seven standard samples.

At the sample preparation laboratory (Assayers Canada in Telkwa, BC), the standard samples were crushed, sieved, and transferred into the laboratory's pulp envelopes the same as every other sample. They were submitted blind to the analytical lab.

14.2.4 Laboratory Duplicate Protocol

Laboratory duplicates were not available for the sequence of pulp samples. For the core sample sequence, laboratory duplicates were inserted into the sample stream by the sample preparation laboratory. The purpose of laboratory duplicates is to test for repeatability of assays. The value of a duplicate sample analyses is expected to be close to the original analysis value. Some variability is expected due to inherent in homogeneity in mineral distribution within the drill core (and hence within the coarse crushed core from which duplicate samples are prepared). A large disparity between initial and duplicate analysis would suggest an analytical problem.

At the crushing stage of sample preparation, a duplicate pulp sample was produced from approximately every 20th sample, for a total of eighty-five laboratory duplicate samples. The laboratory duplicate samples were identified by the original sample number plus the suffix “DP”.

14.2.5 Laboratory Repeat Protocol

The purpose of laboratory repeats is to test for repeatability of analyses without the influence of inhomogeneous mineral distribution in the rock formation (and hence drill core and crushed core). The value of a repeat sample assay is expected to be close to the original assay value. Small disparities between initial and repeat analysis values can be used to judge the precision of the analytical technique. A large disparity between initial and repeat analysis would suggest an analytical problem.

Laboratory repeat analyses were performed by analyzing a pulp sample as usual, and then performing a second analysis using a fresh sub sample of pulp from the same pulp sample. Laboratory repeat analyses were performed by the assay laboratory on approximately every 50^{th} sample, for a total of twenty-four repeat analyses.

14.2.6 Laboratory Standard Protocol

Laboratory standards were used to test for analytical accuracy and repeatability of analyses and systemic analytical deviations. Met-Solve prepared laboratory standard material from a sample of Bronson Slope drill core that was collected for a metallurgical study in 2007. The drill core was crushed, pulverized, and homogenized for use as a laboratory standard. An initial batch of samples from the standard material was analyzed as part of an orientation study described in **Item 13.1.1.** Laboratory standard samples were inserted into the core and pulp sample streams at an interval of approximately every 100th sample, for a total of fourteen laboratory standards.

14.3 QA/QC Results

14.3.1 Field Blank Results

Analyses results from the blank rock sample analyses are presented in **Table 14-1**. Of the thirty-three blank rock samples submitted, thirty-two returned values below the detection limit, while a single sample returned a value of the detection limit (0.1%). These results are consistent with what is expected for blank samples, and are not indicative of contamination at any stage of sampling, sample transport, sample preparation, or analyses.

TABLE 14-1
FIELD BLANK ANALYSES RESULTS

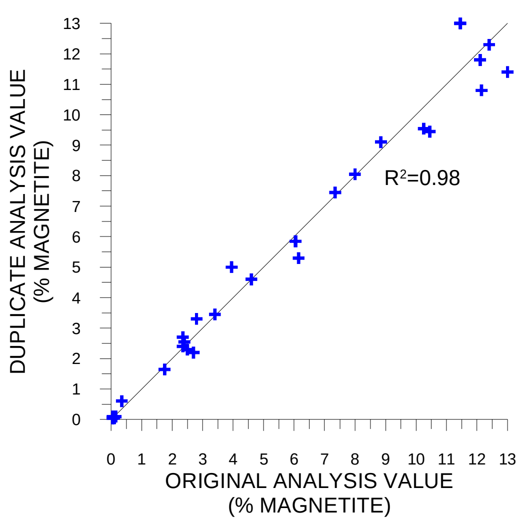
Sample No.	Magnetite Assay (%)	Sample No.	Magnetite Assay (%)	Sample No.	Magnetite Assay (%)
126547	BDL	127049	BDL	127571	BDL
126744	BDL	127089	BDL	127602	BDL
126791	BDL	127128	BDL	127634	BDL
126816	BDL	127250	BDL	127674	BDL
126866	BDL	127290	BDL	127714	BDL
126916	BDL	127330	BDL	127754	BDL
126578	BDL	127376	BDL	127814	BDL
126628	BDL	127416	BDL	127854	BDL
126678	BDL	127460	BDL	127894	BDL
126981	0.1	127502	BDL	127926	BDL
127019	BDL	127529	BDL	127966	BDL

Note: BDL means Below Detection Limit.

14.3.2 Field Duplicate Results

Analyses results from the thirty-five field duplicate samples are plotted on **Figure 14-1**. Perfect results in which assays of initial and duplicate samples returned identical values would plot on the diagonal line in the figure. The distribution of the value pairs (points) about the line can be described by the coefficient of determination (R^2), where 0.0 would describe a random scatter of points, and 1.0 would describe a perfect fit to the line. The R^2 for the field duplicate data set is 0.98. This degree of scatter is expected, and not indicative of any analytical problem.

FIGURE 14-1
FIELD DUPLICATE ANALYSES RESULTS



14.3.3 Field Standard Results

Statistics for the set of analysis results for standards 1 through 3 are summarized in **Table 14-2**, and the data are presented graphically in **Figures 14-2** through **14-4**, respectively. A sample falling outside the second deviation (SD) from the mean is generally considered a failed standard analysis.

TABLE 14-2
STATISTICAL SUMMARY OF FIELD STANDARD RESULTS

Standard 1		Standard 2		Standard 3	
n	33	n	32	n	11
Mean	1.84	Mean	0.62	Mean	1.24
Median	1.85	Median	0.70	Median	1.25
SD	0.20	SD	0.24	SD	0.10
2 SD	0.40	2 SD	0.48	2 SD	0.21

The mean value of the thirty-three Standard 1 assays is 1.84%. As shown on **Figure 14-2**, all Standard 1 analyses are within the 2 SD limit, except Sample 127829. The initial Sample No. 127829 assay, at 0.5% magnetite, lies well outside the expected range, and is considered a failed standard analysis. Met-Solve performed a re-analysis of the failed sample plus three other samples from the same sample sequence. The re-analysis of the failed standard returned 1.4% magnetite, while the re-analyses of the three remaining samples returned values similar to the respective initial values. A summary of the four re-analyses values is given in **Table 14-3**. Although the re-analysis value of 1.4% remains slightly below the 2 SD cut-off, it does appear to belong within the dataset, and does not appear to indicate a systematic analytical problem. Met-Solve could offer no explanation for the variable result. The failed standard assay (0.5%) has been omitted from statistical calculations, but the re-analysis value (1.4%) is included.

FIGURE 14-2
STANDARD 1 ANALYSES RESULTS

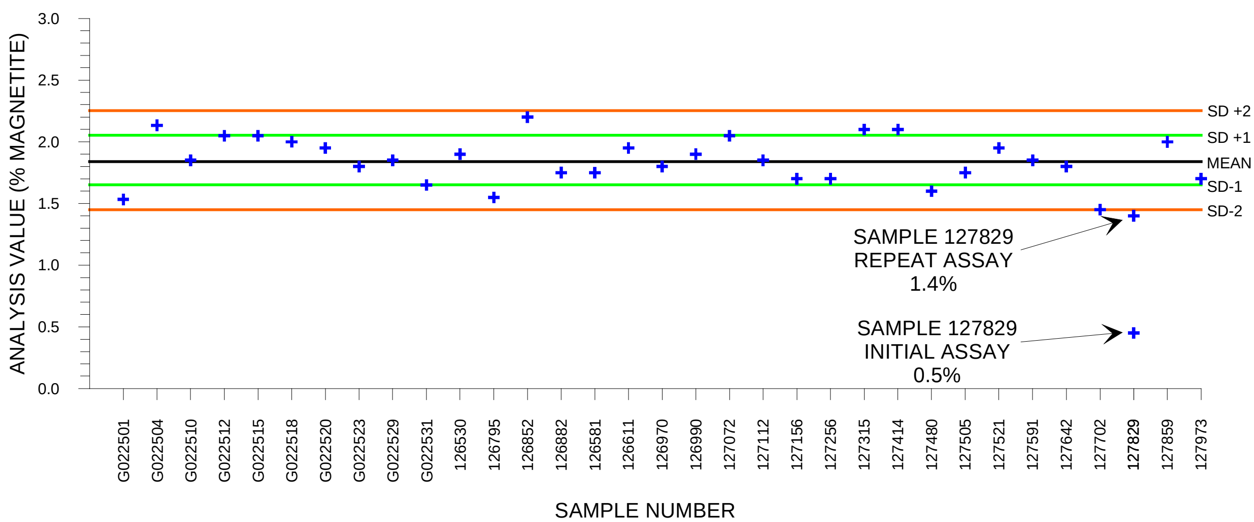
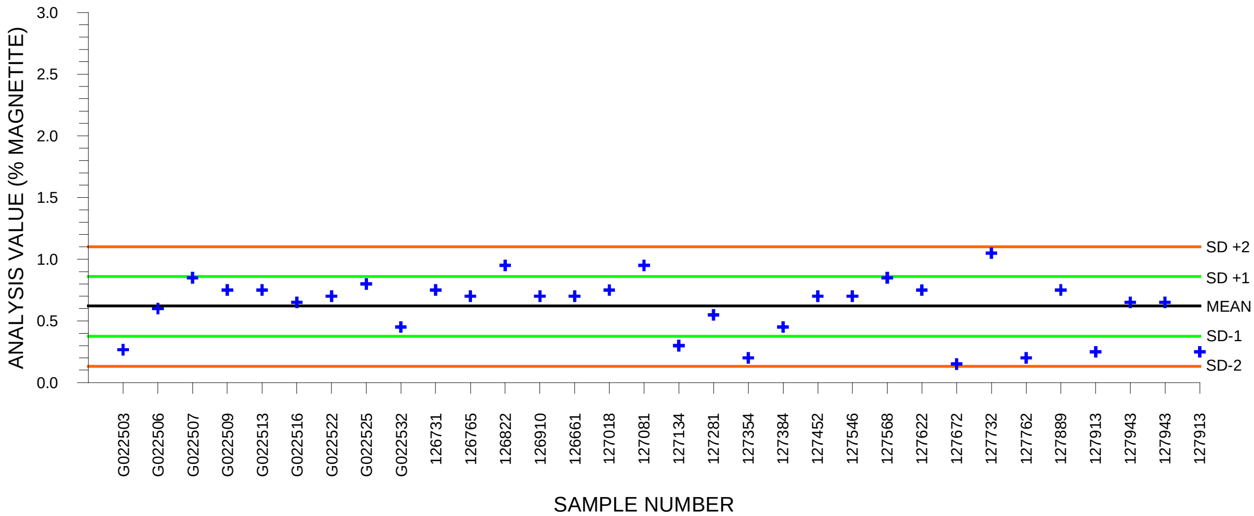


TABLE 14-3
SUMMARY OF FAILED STANDARD RE-ANALYSES

Sample No.	Magnetite (%)	
	Initial Analysis	Re-analysis
127829 (STA 1)	0.5	1.4
127828	BDL	BDL
127830	0.1	0.1
127839	0.7	0.8

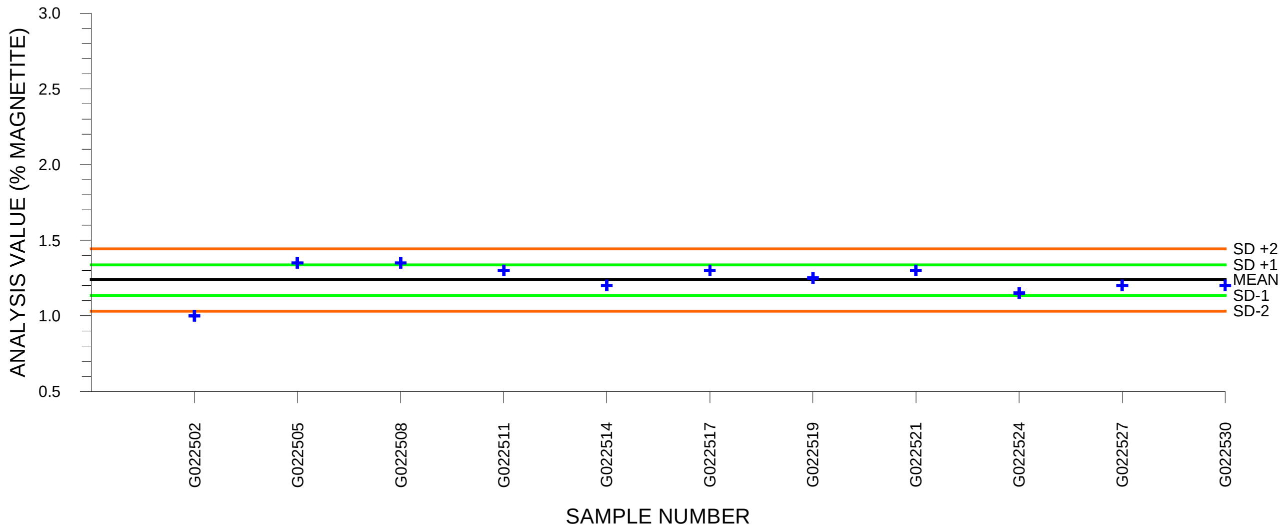
The mean value of the thirty-two Standard 2 analyses is 0.62%. As shown on **Figure 14-3**, all Standard 2 analyses are within the 2 SD limit.

FIGURE 14-3
STANDARD 2 ANALYSES RESULTS



The mean value of the eleven Standard 3 analyses is 1.24%. As shown on **Figure 14-4**, all Standard 2 assay values are within the 2 SD limit except one. Sample G022502 is slightly below the 2 SD limit. This sample was analysed with the initial batch of samples to be assayed at the lab. For the initial batch, sub samples of 15 g were analysed in the magnetic separator. An assessment of the duplicate and repeat analysis values for this sample batch determined that analytical precision and repeatability were relatively low, so for all subsequent analyses, 20g sub samples were analysed. The analysis value of Sample G022502 confirms the relatively low precision of this first sample batch, and the problem was corrected by using 20g sub samples for all subsequent analyses.

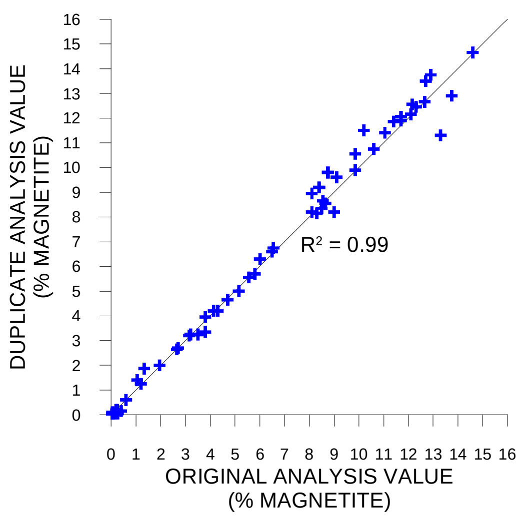
FIGURE 14-4
STANDARD 3 ANALYSES RESULTS



14.3.4 Laboratory Duplicate Results

Analysis results of the eighty-five laboratory duplicate samples are presented graphically in **Figure 14-5**. The correlation is very good, with an R^2 of 0.99. No analytical problem is indicated.

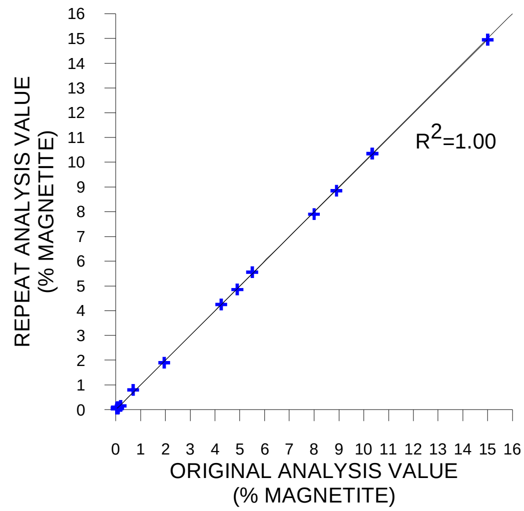
FIGURE 14-5
LABORATORY DUPLICATE ANALYSES RESULTS



14.3.5 Laboratory Repeat Results

Analysis results of the twenty-four laboratory repeat samples are presented graphically in **Figure 14-6**. The correlation is almost perfect, with an R^2 of 1.00. No analytical problem is indicated.

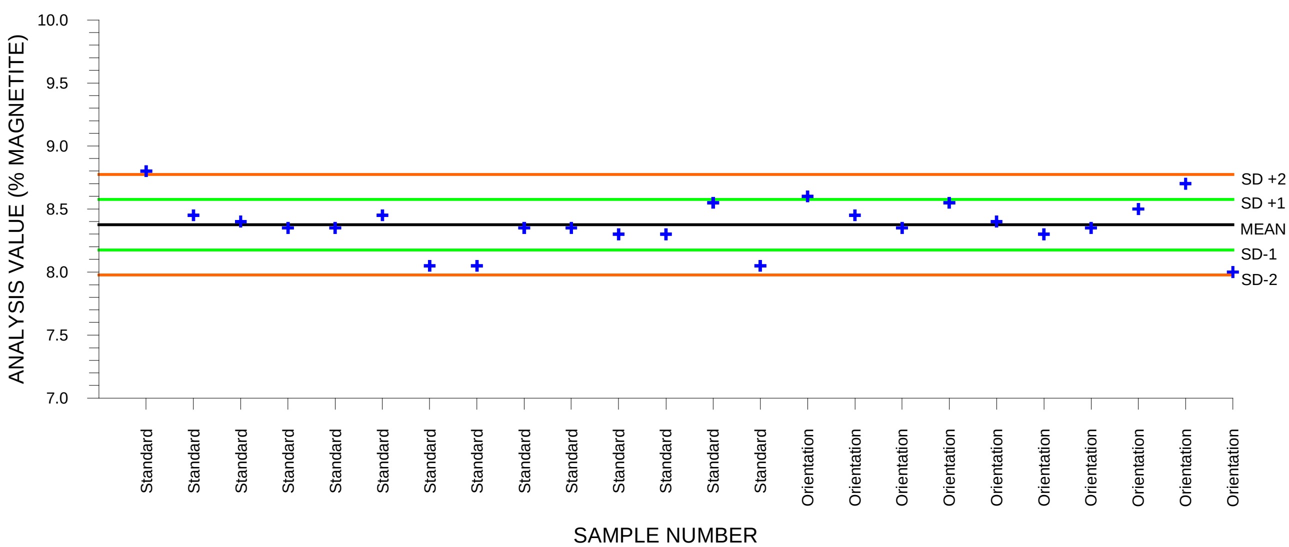
FIGURE 14-6
LABORATORY REPEAT ANALYSIS RESULTS



14.3.6 Laboratory Standard Results

The twenty-four laboratory standard samples comprising the statistical population include ten samples from the orientation study described in **Item 13.1.1.** These ten orientation samples are identified on **Figure 14-7** as "Orientation". The mean value of the twenty-four laboratory standard analyses is 8.38% magnetite. As shown on **Figure 14-7**, all Laboratory Standard analysis values are within the 2 SD limit except one. At 8.8%, the first sample at the left side of the plot is slightly above the 2 SD limit of 8.77. However, the data point does appear to belong with the data set, and is suggestive of variability in the analytical precision rather than any analytical problem.

FIGURE 14-7
LABORATORY STANDARD ANALYSIS RESULTS



14.4 Technical Review by Authors

The 2009 drill-sampling program contained a good QA/QC protocol that has established good repeatability and relatively low variance for the sample chains. This QA/QC program has demonstrated no laboratory contamination and good accuracy.

All of the exploration work conducted on the Bronson Slope property from 1988 through 2007 was performed by competent, professionally qualified persons.

Due diligence studies by the writers include those completed during the site visits and review of the data on this property during 2006, 2007, and 2009. During 2009, Mr. Burgoyne was at the property from October 1 through 3, 2009, and Mr. Burgert was on site through the complete sampling program from October 1 through 22, 2009. This evaluation work in 2009 and 2010 is summarized as:

- Property site visits including review of geology, mineralization and site setting.
- An examination of drill core at the Bronson Airstrip from the 1988 and 1994 through 1997, and 2006 and 2007 programs.
- A detailed review of a large database of technical reports and many maps and sections dealing with the property.
- A review of the geologic model with respect to controls on mineralization at the Bronson Slope deposit.
- Auditing and checking of calculations leading to Mineral Resource estimates, a review of the drill hole and analysis database and resource methodology parameters, and evaluation of mineralized cross-sections.
- Detailed review of the QA/QC procedures.
- A detailed review of all mine development studies undertaken in 2007 through 2009.

15.0 Adjacent Properties

There are nearly four hundred mineral occurrences in the Iskut River are of NTS 104B. Only those major deposits that are within several kilometers of Bronson Slope and/or where production is recorded are described here.

Iskut Deposit
Newcastle Minerals Ltd. owns the Snip North property, located 2.5 km northwest of Bronson Slope deposit. **.** The limited drilling and preliminary geological modeling to date has defined the Iskut gold-copper-molybdenum deposit. Based on eight 2007 and 2006 drill holes and four historical drill holes the following definition on the geometry and grade of the deposit was reported in the February 22, 2008 Newcastle Minerals Press Release and is detailed in Burgoyne (2008). Using dimensions of 500 and 600 meters in strike length, a width of 225 meters and a depth of 175 meters along with a specific gravity of 2.90 yields a potential quantity of 57.1 to 68.5 million tonnes. The grade varies from 0.3 to 0.6g/t gold, 0.09 to 0.17% copper and 0.003 to 0.023% molybdenum. ***This estimate of quantity and grade is conceptual in nature and there has been insufficient exploration and drilling to define a mineral resource and that it is uncertain if further exploration will result in the target being delineated as a mineral resource***

Snip Deposit
The adjacent Snip Mine (Minfile 104B 250), located within 500m of the north boundary of the Bronson Slope property was operated by Cominco Limited, and Prime Resources Group and Homestake Canada Inc. From 1991 to 1999, the Snip Mine produced 32,093 kilograms of gold, 12,183 kilograms of silver, and 249,000 kilograms of copper from about 1,267,642 million tonnes of ore. The Twin vein zone is a 0.5 to 15 meter wide sheared quartz-carbonate-sulphide vein that cuts through a massively bedded feldspathic greywacke-siltstone sequence. The mineralization occupies a 120° structure with dips varying from 30 to 90 degrees southwest. A post-mineralization dyke divides the vein into two parts for most of its length. The dip length of the deposit is about 500m and has been traced over a strike length of 1000m.

Johnny Mountain
The closed Johnny Mountain Gold Mine (Stonehouse gold deposit - Minfile 104B 107) of Skyline Gold, located 4.5 km south-southeast of Bronson Slope, is optioned out to Spirit Bear Minerals Ltd. Recorded production from 1987-1993 totals 2815.4 kilograms of gold from 227,247 tonnes. This is a structurally disrupted mesothermal gold-bearing quartz vein deposit. Mineralization includes pyrite, chalcopyrite with some sphalerite, galena and minor pyrrhotite within a number of sub parallel sulphide-K-feldspar-quartz veins and stock work systems occurring along a series of northeast-trending structures in close proximity to plagioclase porphyry dykes.

The writers are unable to verify the above information, except that on Iskut Deposit, and the information is not necessarily indicative of the mineralization on the Bronson Slope property.

16.0 Mineral Processing & Metallurgical Testing

Magnetite
Klein (2008) completed metallurgical and marketing studies with respect magnetite that could be recovered from the Bronson Slope deposit. The market study estimated the amount of magnetite used for BC and Alberta Coal industries for dense media separation and the metallurgical study assessed the properties of the Bronson Slope magnetite use in dense media. Dense media separation is a process in which finely ground magnetite is mixed with water to create a medium that has properties of a dense liquid. Specifically when coal and rock particles are added to the medium, the low-density coal particles will float while the high-density rock particles will sink thereby facilitating separation of coal from waste rock. The dense media is used in two types of separators referred to static separators, such as the dense media drum or dynamic separators such as the dense media cyclone. The specifications for magnetite used in dense media applications is as follows:

Particle size: 90% passing 325 mesh
Density: >4.7 g/cm3
Magnetics content: >93% magnetics

Based on the study by Klein (2008) the estimated usage of magnetite by BC and Alberta Coal Mines for 2007 was 52,743 tonnes.

Klein (2008) completed metallurgical testing from bulk samples obtained from drill core from the Quartz Magnetite Unit of the Bronson Slope deposit. The testing confirmed the metallurgical process, determined the grinding work index for regrinding and characterize the magnetite product with respect to the specifications. The testing involved grinding and flotation to recover copper sulphides. The flotation tailings were used and for magnetic separation testing.

The quartz magnetite sample used for the testing graded 8.94% Fe, 0.27% Cu, and 0.91 g/t Au. From flotation, the copper concentrate contained 79.1% of the copper and the combined flotation-gravity concentration gold recovery was 81.7%.

The flotation tailings were subjected to three stages of magnetic separation. The final product had a density of 4.97 g/cm3 and magnetic content of 99.9%. These specifications exceed those required for dense media confirming that a high-grade magnetite product can be produced that is suitable for dense media separation. The product accounted for 3.68% of the feed mass and contained 28% of the total iron. Based on rougher mass it is expected these values could be increased to close to 10% and 55%, respectively.

Klein (personal communications, 2010) estimates an approximate 95% recovery of the magnetite can be possible although this must be confirmed in further metallurgical studies.

This report by Klein (2008) gives details on Magnetite Usage, Metallurgical Balance Test Report, Metallurgical Balance Flow sheet, Flotation Test Report, Davis Test Tube Report, and Particle Size Analysis and is given as **Appendix D**.

Bronson Slope Cu-Au-Ag Porphyry Deposit – A Summary

The following discussion of copper, gold, silver, and molybdenum metallurgical studies and recoveries are detailed in Lawrence and Seen (2009) and Burgoyne and Giroux (2008). Detailed discussions are given for the 1994, 1995, 1996 and 1997 programs, which are

detailed in Burgoyne and Giroux (2008). These reports can be found on www.sedar.com. The following is a summary of this information.

Skyline Gold has performed a series of metallurgical studies on Bronson Slope drill core samples from 1994 to 1997 as part of engineering scoping and process flow sheet development studies.

- In 1994 Lakefield Research was commissioned by SGC to conduct a preliminary metallurgical testing of the Bronson Slope ore. The purpose of the test was to determine recoverability of copper gold minerals using a conventional flotation method.
- In January 1995 SGC commissioned Process Research Associates (PRA, Vancouver, BC) to conduct additional metallurgical test work to further define the expected metallurgical results.
- In 1996 further metallurgical testing was commissioned by PRA and Beattie Consulting Ltd. The program was designed to assess the preliminary ore characterisation, copper and molybdenum flotation and acid base accounting test work.
- In 1997 PRA was retained by SGC to undertake an expanded metallurgical test work program. The objective was to obtain design criteria as part of a feasibility study.

From then onwards no further metallurgical work has been carried out until recently in 2007 some testing has been conducted on some drill core samples of high wall material, which hasn't been tested before.

The report entitled "Metallurgical Study on the Bronson Slope Samples" by Process Research Associates (PRA), 1997 forms the basis for metallurgical comments within this report.

Some coarse gold effect was observed in the average composite sample since gold grade of this sample varied from 0.37g/t to 0.86g/t. Gravity recovered gold of 25.5% with a gold content of 23.8g/t gold was recovered using a gravity Knelson concentrator. Other composite samples were also tested. The gold recovery varies from 18.7% for the upper sediment to 38% for the quartz magnetite. The study showed that pre-concentration with a gravity separator should be included in the process to recover the coarse gold that will not be recovered by the flotation process.

The Bond millwork index of the composites ranged from11.5 kWh/t to 13.3 kWh/tonne. The specific gravity ranged from 2.72t/m^3 to 2.83t/m^3.

The projected copper and gold recoveries of the bulk copper flotation are as follows:

- Average composite – 84% Au, 87% Cu, 61% Ag, 46% Mo at 27% copper concentrate.
- Upper Sediment – 82% Au, 89% Cu, 68% Ag, 58% Mo at 24% copper concentrate.
- Upper Sediment Oxidised – 88% Au, 82% Cu, 50% Ag, 52% Mo at 22.8% copper concentrate.
- Porphyry – 83% Au, 83% Cu, 67% Ag, 53% Mo at 20% copper concentrate.
- Quartz Magnetite – 88% Au, 87% Cu, 66% Ag, 33% Mo at 19% copper concentrate.
- Starter Pit – 87% Au, 88% Cu, 66% Ag, 43% Mo at 24% copper concentrate.
- High Grade – 86% Au, 90% Cu, 68% Ag, 53% Mo at 22% copper concentrate.

The recovery of gold is a combined gravity and flotation recovery.

TABLE 16-1

HEAD ASSAY OF COMPOSITES

Composites		Average	US	USO	PPY	QM	SP	HG
		Average Blend	Upper Sediment	Upper Sediment Oxidized	Porphyry	Quartz Magnetite	Starter Pit	High Grade
Au	g/t	0.472	0.446	0.776	0.369	0.518	0.517	0.724
Ag	g/t	2.44	2.42	3.18	2.66	2.79	2.74	3.72
Cu	%	0.192	0.206	0.252	0.133	0.181	0.227	0.358
Mo	%	0.007	0.009	0.014	0.008	0.006	0.007	0.009
Fe	%	6.43	4.76	4.03	5.66	7.48	7.06	7.11

TABLE 16-2
COMPARISON OF ASSAY GRADES OF
COMPOSITED METALLURGICAL TEST SAMPLES (1996, 1997)

METALLURGICAL ASSAYING									
Comp. Sample Name		**BC**	**US**	**USO**	**PPY**	**QM**	**SP**	**HG**	Average of
No. Of Tests		28	3	2	2	4	2	2	All Comps
Average Metallurgical	Au g/t	0.472	0.446	0.776	0.369	0.518	0.517	0.724	0.546
Calculated Head Grades	Ag g/t	2.44	2.42	3.18	2.66	2.79	2.74	3.72	2.85
	Cu %	0.192	0.206	0.252	0.133	0.181	0.227	0.358	0.221
	Mo %	0.007	0.009	0.014	0.008	0.006	0.007	0.009	0.009

CORE SAMPLE ASSAYING									
Comp. Sample Name		**BC**	**US**	**USO**	**PPY**	**QM**	**SP**	**HG**	Average of
No. Of Core Samples		1488	462	195	199	817	115	145	All Comps
Unweighted Average	Au g/t	0.50	0.49	0.9	0.4	0.54	0.58	0.66	0.58
Assay Grades	Ag g/t	2.60	2.7	3.3	2.5	2.6	2.9	3.1	2.8
	Cu %	0.18	0.19	0.23	0.14	0.18	0.19	0.24	0.19
	Mo %	0.005	0.008	0.013	0.006	0.003	0.004	0.007	0.01
Comp. Sample Name		**BC**	**US**	**USO**	**PPY**	**QM**	**SP**	**HG**	Average of
No. Of Core Samples		1488	462	195	199	817	115	145	All Comps
Weighted Average	Au g/t	0.47	0.47	0.99	0.4	0.49	0.54	0.63	0.57
Assay Grades	Ag g/t	2.3	2.2	3.3	2.2	2.4	2.3	3.1	2.5
	Cu %	0.16	0.18	0.23	0.13	0.16	0.17	0.23	0.18
	Mo %	0.004	0.007	0.013	0.006	0.003	0.003	0.007	0.006

No. = Number	BC = Bulk Composite 350 m Pit (1996)	PPY Porphyry	(1997)
Comp. = Composite	US = Upper Sedimentary Rock (1997)	SP Starter Pit	(1997)
	USO = Oxidized Upper Sedimentary Rock (1997)	HG High Grade	Sample

17.0 Mineral Resource Estimation

MAGNETITE MINERAL RESOURCE

17.1 Data Analysis

A total of 22 diamond drill holes totalling 7,521 m were re-sampled for magnetite content. The drill holes used for this Magnetite Resource are listed in **Appendix A**. The drill holes were compared to the domain solids used to estimate the Cu-Au Resource in 2008. Individual magnetite measurements, as determined by the Davis Tube method and discussed in **Item 13** were tagged with a Domain Code. The statistics for each Domain are tabulated below.

TABLE 17-1
SAMPLE STATISTICS FOR MAGNETITE IN ANALYSES
(Weight Percent)

	US	QM	PPY	HW
Number	928	691	225	113
Mean	0.86	7.22	6.05	0.06
Standard Deviation	1.97	4.09	3.56	0.02
Minimum	0.05	0.05	0.05	0.05
Maximum	12.95	16.55	17.85	0.20
Coefficient of Variation	2.29	0.56	0.59	0.41

No capping was required in any of the lithologies.

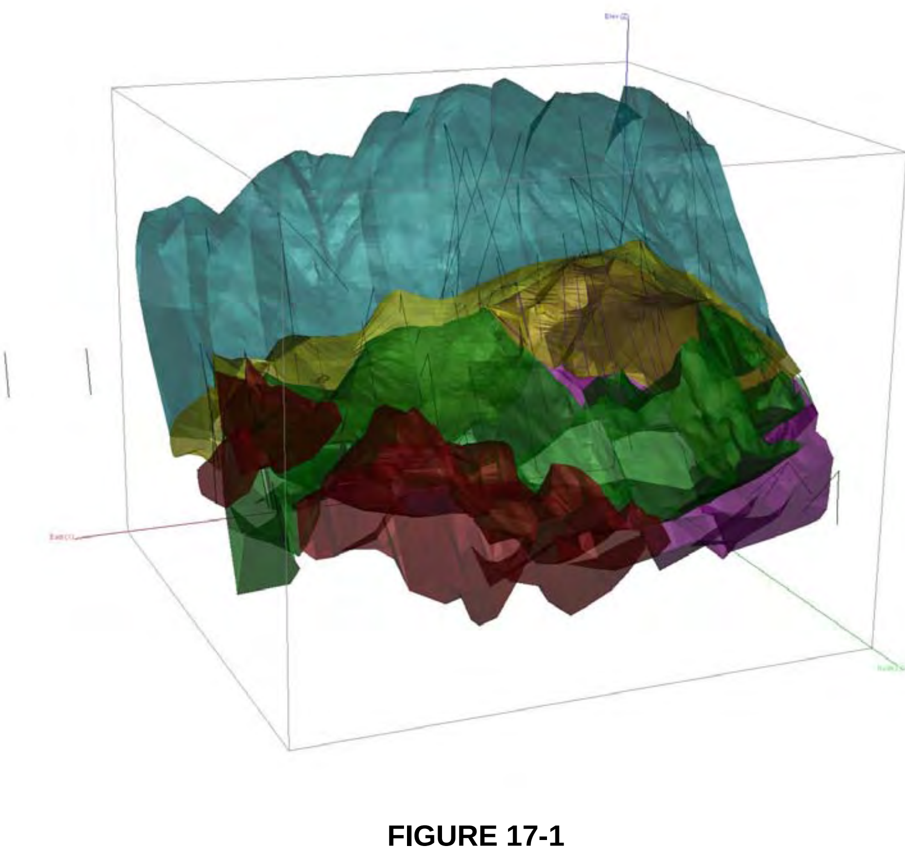


FIGURE 17-1
ISOMETRIC VIEW LOOKING SOUTH SHOWING DRILL HOLES AND THE VARIOUS DOMAINS,
HW IN BLUE, PPY IN MAGENTA, QM IN GREEN, US IN YELLOW-GREEN AND LS IN RED.

17.2 Composites

Uniform down hole composites were produced at 5 m intervals within each of the four domains. Intervals less than 2.5 m at the domain boundaries were combined with the adjoining assay to produce a uniform support of 5 ± 2.5 m.

TABLE 17-2
SAMPLE STATISTICS FOR MAGNETITE IN 5 M COMPOSITES
(Weight Percent)

	US	QM	PPY	HW
Number	551	417	141	74
Mean	0.84	7.26	5.98	0.06
Standard Deviation	1.85	3.77	3.38	0.04
Minimum	0.05	0.05	0.05	0.05
Maximum	12.44	14.94	14.06	0.33
Coefficient of Variation	2.20	0.52	0.56	0.58

Contact plots, showing the changes in average grade taken at different distances from a contact, between QM and PPY show similar grades on both sides indicating a soft boundary could be used. There are however roughly three times as many measurements in the Quartz Magnetite as in the Intrusive (PPY) and as a result a hard boundary was used to avoid smoothing higher QM grades into PPY blocks where there were gaps in the PPY coverage. The contact plot between QM and US shows that while the QM has significantly higher grades on average the contact area of up to 20 m on each side shows very similar grades in the 3 to 4 % range. Again, however, in areas where there are no US data to mitigate an estimate the higher grade QM could overestimate the US grades, so a hard boundary was placed between these two domains for interpolation. Note plots at end of **Item 17**.

17.3 Semivariograms

Due to the limited amount of composite data a single set of semivariograms was run using all composites containing Magnetite assays. Pair-wise relative semivariograms were run in the four principal horizontal directions; E-W, N-S, SW-NE and NW-SE. Geometric anisotropy was demonstrated with the longest continuity in the E-W direction. The second longest range was in the vertical direction. Nested spherical models were fit to all the semivariograms and the results are tabulated below with the models included as **Figures 17-2 to 17-4.**

TABLE 17-3
SUMMARY OF SEMIVARIOGRAM PARAMETERS

Variable	Az	Dip	C_o	C_1	C_2	Short Range (m)	Long Range (m)
Magnetite	90	0	0.05	0.30	0.50	20	200
	0	0	0.05	0.30	0.50	20	50
	0	-90	0.05	0.30	0.50	40	60

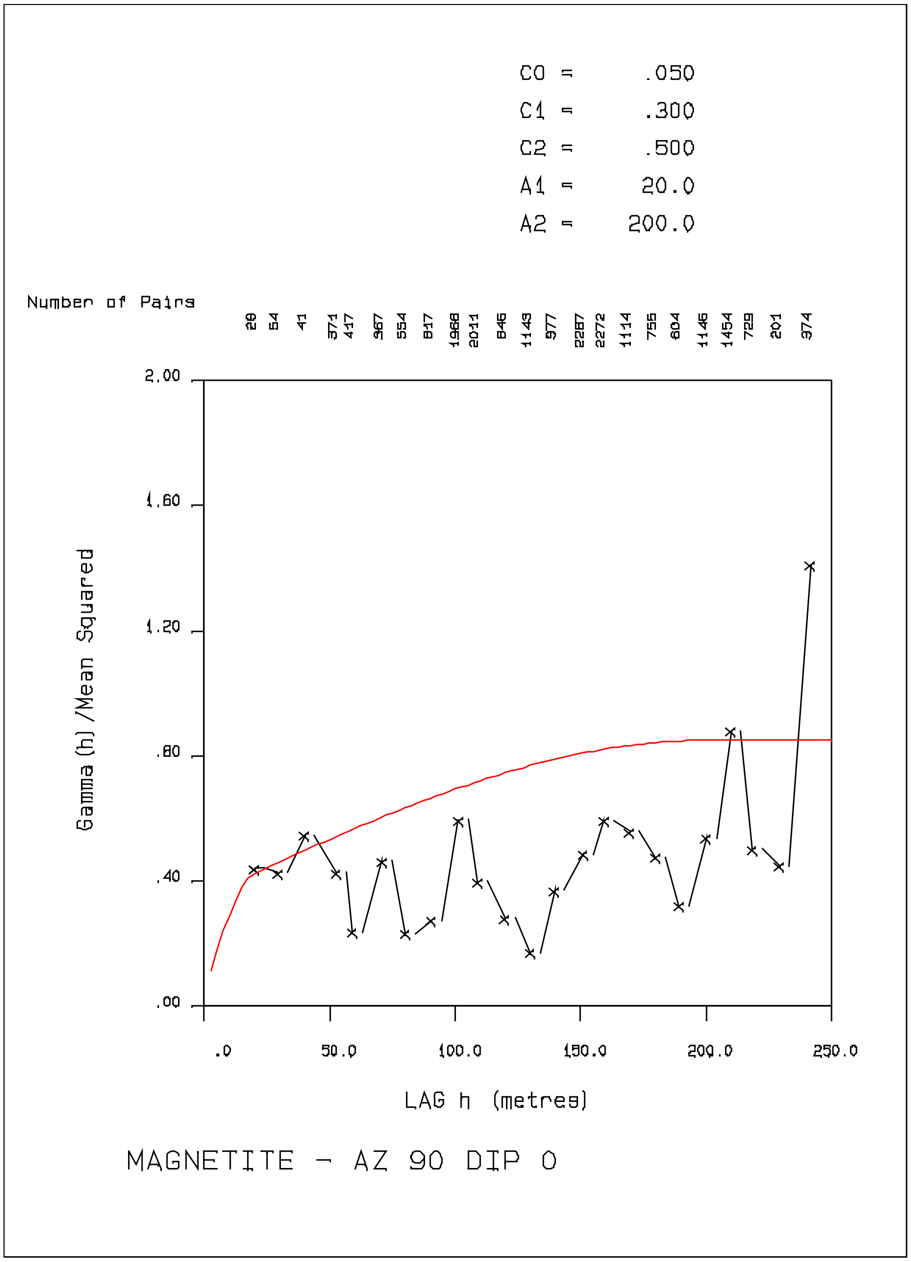


FIGURE 17-2
SEMIVARIOGRAM FOR MAGNETITE ALONG AZIMUTH 90 DIP 0

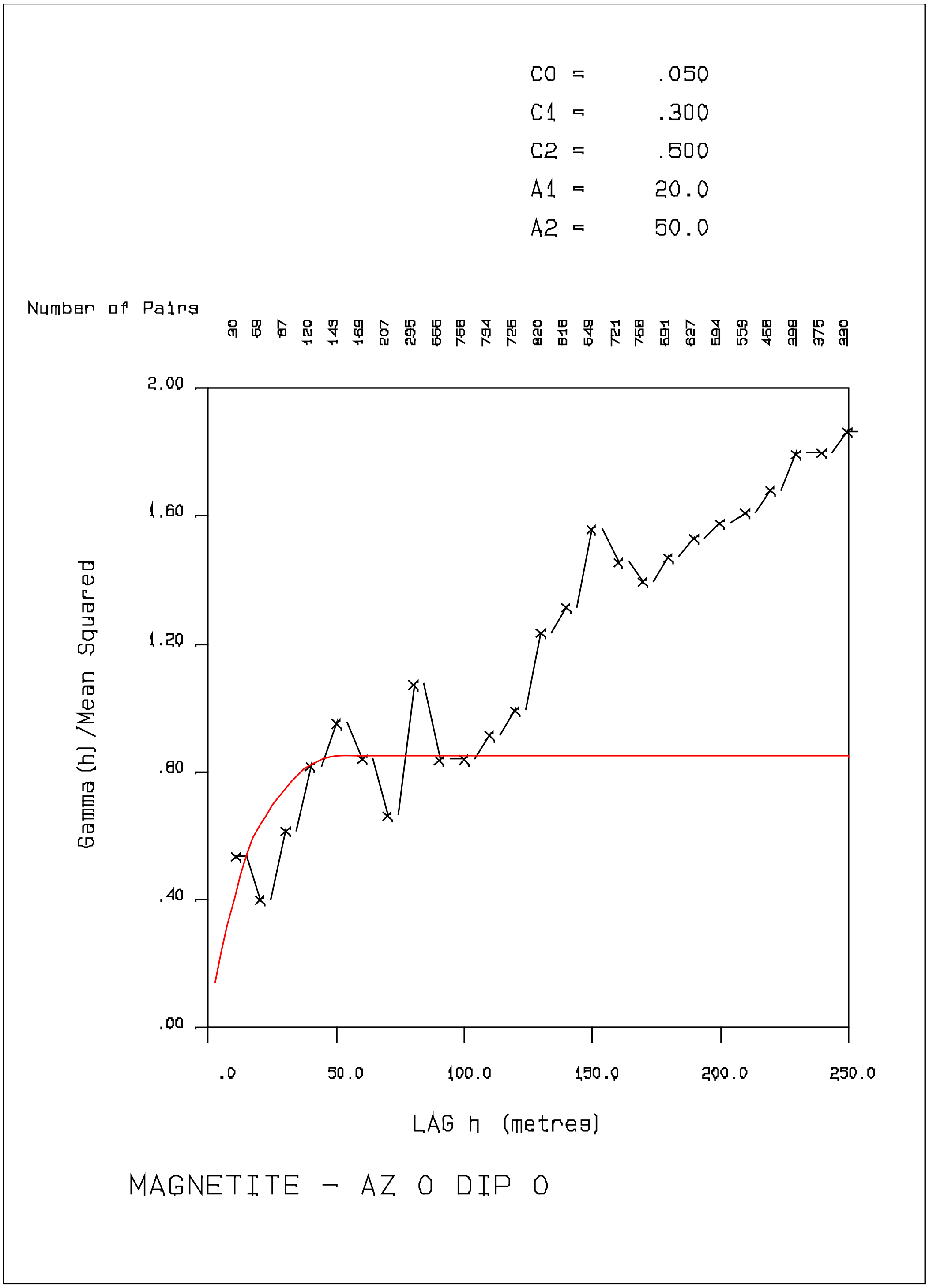


FIGURE 17-3
SEMIVARIOGRAM FOR MAGNETITE ALONG AZIMUTH 0 DIP 0

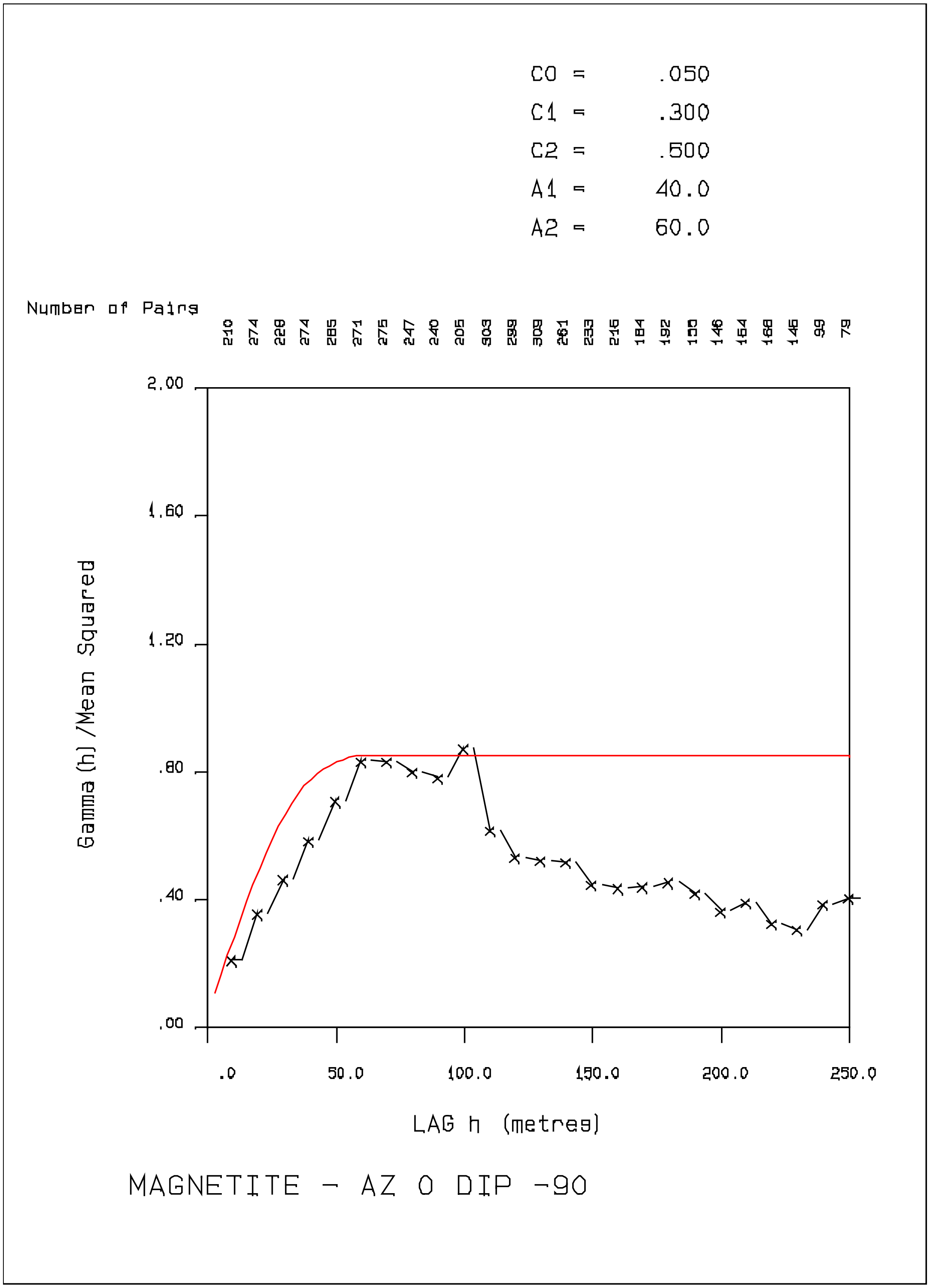


FIGURE 17-4
SEMIVARIOGRAM FOR MAGNETITE ALONG AZIMUTH 0 DIP -90

17.4 Bulk Density

A total of 88 specific gravity measurements have been made on crushed core at Bronson Slope by Acme Analytical Laboratories. The results are presented in **Table 17-6.** Three of the five geologic domains were sampled US, PPY and QM. Average values for these three domains are 2.74, 2.76 and 2.77 respectively. The average of these three or 2.76 is used for the other two Domains not sampled, namely HW and LS.

TABLE 17-4
Summary of Specific Gravity Determinations

Domain	Number	Minimum SG	Maximum SG	Average SG
US	13	2.65	2.85	2.74
PPY	3	2.75	2.77	2.76
QM	72	2.67	2.89	2.77
TOTAL	88	2.65	2.89	2.76

17.5 Block Model

A geologic model was completed by Skyline geologists using Surpac software. Five geologic solids were created based on sectional interpretations. A block model of 10 x 10 x 10 m blocks was superimposed over these solids. For each block the percentage below topography and inside the respective solids was recorded. The origin of the block model is as follows:

Lower Left Corner	24900 E	10 m wide	160 columns
	11300 N	10 m long	115 rows
Top of Model	895	10 m high	80 levels
No rotation			

17.6 Grade Interpolation

Magnetite grades were interpolated into blocks containing some percentage of QM, PPY, US or HW domains using ordinary kriging. The kriging was done first for blocks containing some percentage of QM using only QM composites. A second kriging run was completed for blocks containing some percentage of PPY and only PPY composites. Finally a third kriging run was completed for blocks containing some percentage of US or HW using composites from within these two domains.

In all runs the kriging was completed in four passes with the search ellipse for each pass a function of the semivariogram ranges. For Pass 1 a minimum of 4 composites were required within a search ellipse with dimensions equal to ¼ the semivariogram range. For blocks not estimated a second pass using search ellipse dimension equal to ½ the range were used. A third pass using the full range and a fourth pass using twice the range completed the exercise. In all cases a maximum of 12 composites were used and if more than 12 were found within any search, the closest 12 were used. In all cases a maximum of 3 composites from any single hole were allowed insuring each block was estimated with at least two drill holes.

17.7 Results

Blocks were classified during the resource estimation for Au and Cu completed in **Item 17.7** of Burgoyne and Giroux (2008) found at www.sedar.com The tonnage was established for each block during this estimation. For the magnetite estimation the block classifications and tonnages were taken from the 2008 block model. The results are tabulated below.

TABLE 17-5
MEASURED MAGNETITE GLOBAL RESOURCE

Magnetite Cut-off (%)	Tonnes > Cut-off (tonnes)	Grade > Cut-off Magnetite (%)	Contained Tonnes Magnetite
1.00	71,280,000	7.15	5,100,000
2.00	66,210,000	7.58	5,020,000
3.00	62,900,000	7.86	4,940,000
4.00	59,550,000	8.10	4,820,000
5.00	55,680,000	8.35	4,650,000
6.00	51,020,000	8.61	4,390,000
7.00	43,570,000	8.97	3,910,000
8.00	32,790,000	9.44	3,100,000
9.00	20,300,000	10.01	2,030,000
10.00	8,730,000	10.74	940,000

TABLE 17-6
INDICATED MAGNETITE GLOBAL RESOURCE

Magnetite Cut-off (%)	Tonnes > Cut-off (tonnes)	Grade > Cut-off Magnetite (%)	Contained Tonnes Magnetite
1.00	108,680,000	6.47	7,030,000
2.00	96,950,000	7.08	6,860,000
3.00	88,500,000	7.52	6,660,000
4.00	83,620,000	7.76	6,490,000
5.00	76,160,000	8.07	6,150,000
6.00	67,200,000	8.42	5,660,000
7.00	57,080,000	8.75	4,990,000
8.00	39,890,000	9.26	3,690,000
9.00	22,580,000	9.84	2,220,000
10.00	7,230,000	10.71	770,000

TABLE 17-7
MEASURED PLUS INDICATED MAGNETITE GLOBAL RESOURCE

Magnetite Cut-off (%)	Tonnes > Cut-off (tonnes)	Grade > Cut-off Magnetite (%)	Contained Tonnes Magnetite
1.00	179,960,000	6.74	12,130,000
2.00	163,160,000	7.28	11,880,000
3.00	151,400,000	7.66	11,600,000
4.00	143,170,000	7.90	11,310,000
5.00	131,840,000	8.19	10,800,000
6.00	118,220,000	8.50	10,050,000
7.00	100,640,000	8.84	8,900,000
8.00	72,680,000	9.34	6,790,000
9.00	42,880,000	9.92	4,250,000
10.00	15,960,000	10.73	1,710,000

TABLE 17-8
INFERRED MAGNETITE GLOBAL RESOURCE

Magnetite Cut-off (%)	Tonnes > Cut-off (tonnes)	Grade > Cut-off Magnetite (%)	Contained Tonnes Magnetite
1.00	13,040,000	4.01	520,000
2.00	6,300,000	6.92	440,000
3.00	5,710,000	7.38	420,000
4.00	5,320,000	7.66	410,000
5.00	4,980,000	7.88	390,000
6.00	4,390,000	8.21	360,000
7.00	3,500,000	8.60	300,000
8.00	2,510,000	9.00	230,000
9.00	1,110,000	9.58	110,000
10.00	240,000	10.40	20,000

It should be noted that when this global magnetite resource is compared to the preliminary open pit designed for the Preliminary Economic Assessment completed by Asia Leighton (Lawrence and Seen, 2009) in March 2009 that 44% of the measured and indicated magnetite tonnage, at a 2% cut-off is within the pit. The remainder sits below and to the west. As a result it is our recommendation that a new PEA be completed using the magnetite results to demonstrate the changes in project economics along with magnetite marketing considerations as noted below.

Since magnetite is a speciality industrial mineral, the amount that can be marketed and its price per metric tonne can only be determined by definition of sales agreements and marketing studies. Consequently the actual economic cut off for magnetite at the Bronson Slope cannot quantitatively be defined at this time. In the marketing study by Klein (2008), he reports that magnetite for one operation, Craigmont, was sold at $211 per tonne delivered to coal operations at Elkford, BC. Klein further indicates that the net cost of magnetite, less freight delivery costs, is in the order of $127 per tonne. Klein also notes that magnetite prices, as iron ore, have been up to $200 per tonne.

The 2% magnetite cut off highlighted in the above tables and used as a base case for resource estimation is based on flotation milling of tails from the Bronson Slope copper-gold-silver operation and truck transportation cost information supplied by Skyline Gold (Jensen 2010a) balanced against what is believed projected conservative sale price of $130 per tonne net of milling and transportation charges. This price is based upon a western Canada magnetite market analysis (Klein 2008) – as discussions with Craigmont Mines that produces magnetite powder for dense media separation coal cleaning. The estimated break-even cut-off grade is less than 2% magnetite on a by-product basis. It must be stressed that the economics are also dependent on the ability to market and sell magnetite. No metallurgical recoveries have been applied to the resource.

Skyline Gold's internal analysis (Jensen, 2010b) estimate that a 7% weight magnetite cut-off based on the 2009 Bronson slope PEA (Lawrence and Seen 2009) and the 2008 magnetite study (Klein 2008) is potentially viable on a stand-alone production basis and assuming that magnetite is the only mineral produced at Bronson Slope. At this cut-off Bronson Slope Measured and Indicated magnetite resource is 100,640,000 tonnes grading 8.8% magnetite for a total Measured and Indicated estimate of 8,900,000 tonnes of contained magnetite. It is reasonably expected that, on a by-product production basis, the magnetite economic cut-off grade would be lower and the magnetite resource estimate at lower cut-off grades is shown in the above tables.

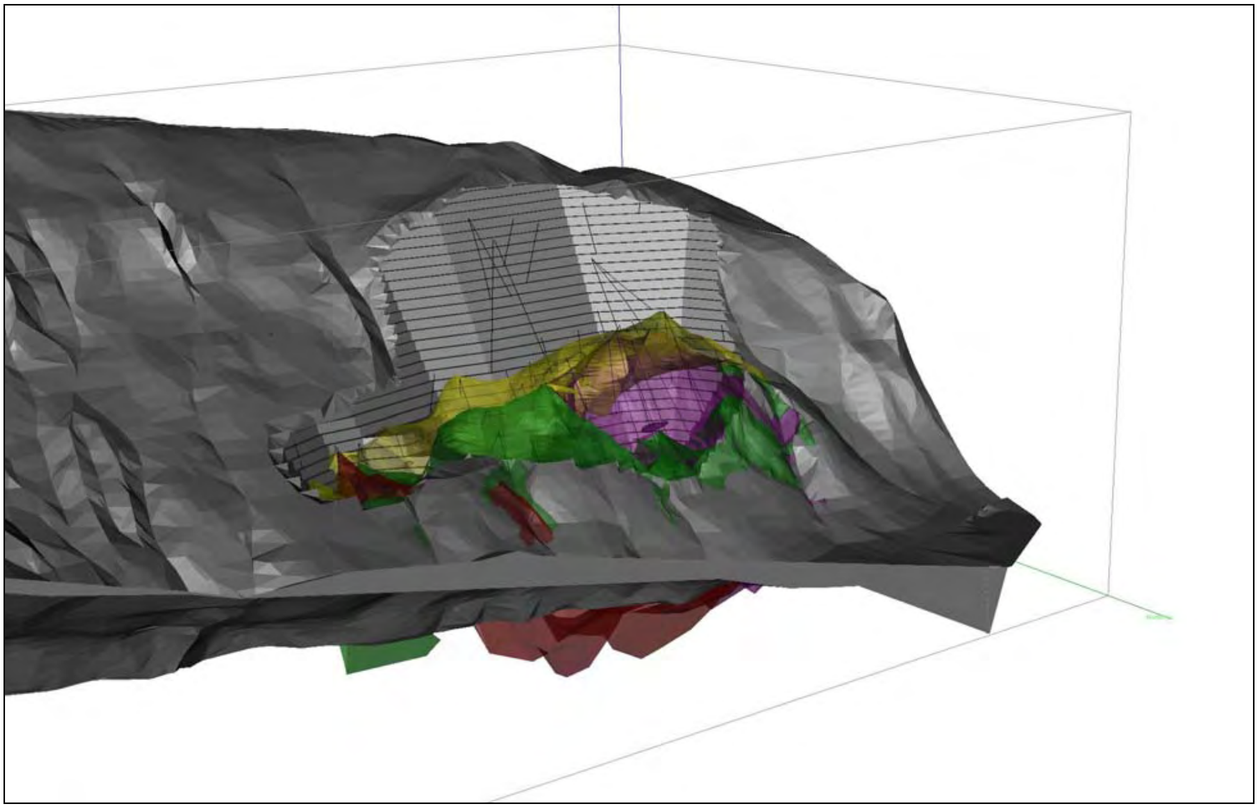


Figure 17-5
Isometric View Looking Southwest Showing Topography and Proposed Open Pit as Designed by Leighton Asia (Lawrence and Seen 2009) – Note **Figure 17-1** for Rock Codes

The relative proportions of the total magnetite resource present within the various rock domains is tabulated below In **Table 17-9** at a 2.0% magnetite cut-off for measured plus indicated blocks.

TABLE 17-9
GLOBAL MAGNETITE RESOURCE (M + IND) IN VARIOUS ROCK DOMAINS

Domain	Classification	Magnetite Cut-off %	Tonnes above Cut-off	% Magnetite	Tonnes* Magnetite	% of Total Magnetite
QM	M+I	2.00	72,240,000	8.45	6,100,000	51.52
PPY	M+I	2.00	81,830,000	6.71	5,490,000	46.37
US	M+I	2.00	6,120,000	3.39	210,000	1.77
HW	M+I	2.00	1,520,000	2.57	40,000	0.34

*Rounding has been applied to the measured plus indicated resource tonnages; consequently the total of all Domain types does not equal the measured plus indicated resource of **Table 17-7**

17.8 Bronson Slope 2008 Copper-Gold-Silver-Molybdenum Resource Estimate

The Bronson Slope Property hosts a porphyry gold-copper-silver-molybdenum deposit. The deposit resource estimate has previously been completed by G. H Giroux, P. Eng., of Giroux Consultants Ltd and A. A. Burgoyne, P.Eng., of Burgoyne Geological Inc., based exploration and drill hole work, completed by Skyline Gold and considered to be of good quality that meets industry standards. The current mineral resource has been estimated for the Bronson Slope deposit that meets CIMM resource standards and classifications and is reported in Burgoyne and

Giroux (2008).

The resource estimate, based on block modeling and kriging is given below. The resource estimate is presented based on two separate cases of metal prices. Case 1 used $1.50/lb Cu, $525/oz Au, $8/oz Ag, and $10/lb Mo. Case 2 used $2.00/lb Cu, $650/oz Au, $10/oz Ag, and $12/lb Mo.

Case 1 metal prices are based on the values used in the 2007 resource estimate by Burgoyne and Giroux (2007). The resource estimate for this case has been completed to provide a direct comparison between the 2007 resource estimate and the 2008 resource estimate. Case 2 metal prices are considered to be potentially more realistic and therefore a second resource estimate has been provided based on these revised metal prices. The metal prices were used along with block based metallurgical recoveries to determine individual block values. The mineral resources presented in the tables below were then determined based on a cut off of US $ 9.00 per tonne net recoverable value for Case 1 and Case 2, respectively.

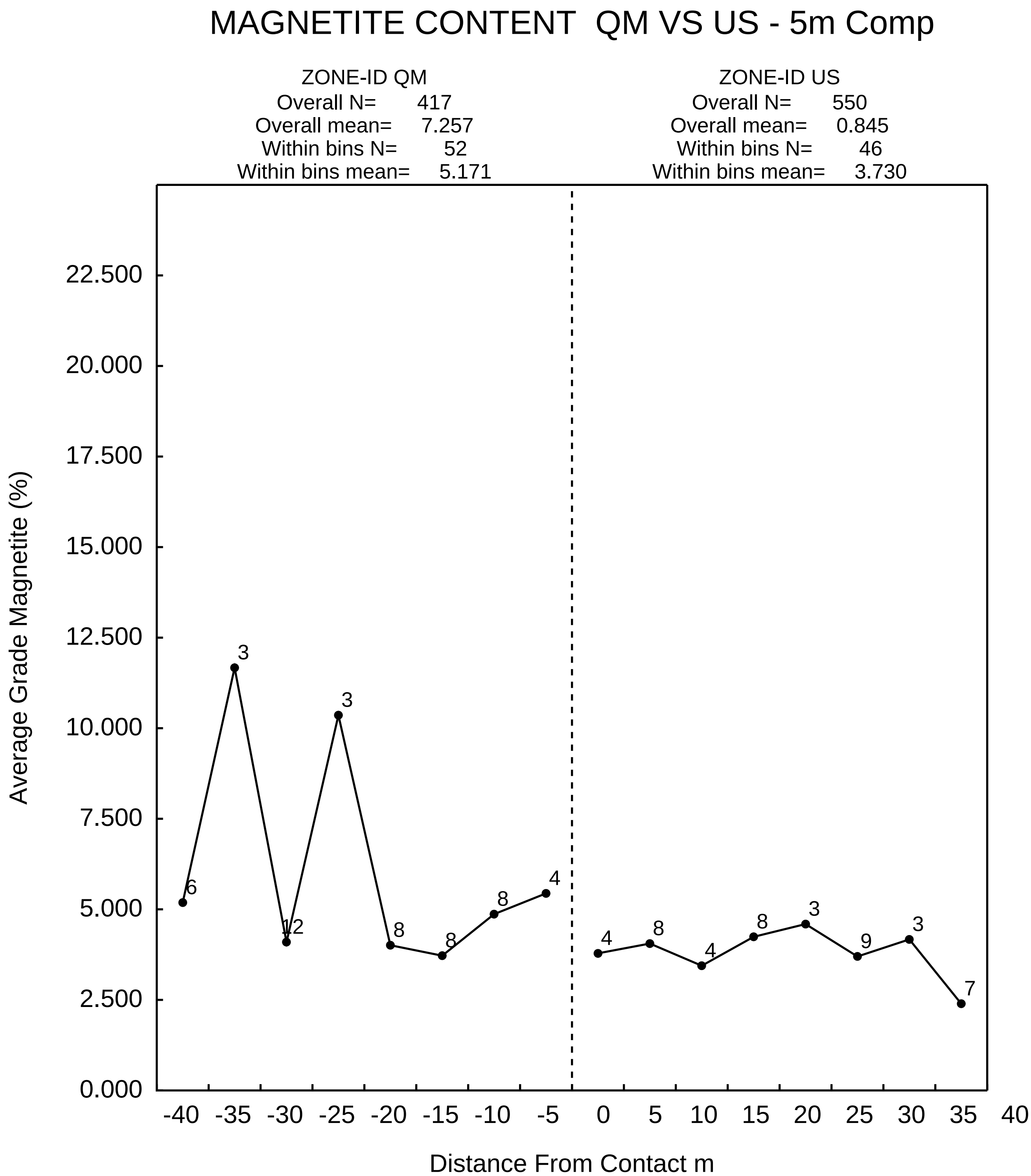
Case 1 2008 Bronson Slope Resource Estimate

Category	Metric Tonnes	Au g/t	Ag g/t	Cu %	Mo %
Measured	58,700,000	0.50	2.45	0.18	0.0058
Indicated	80,800,000	0.36	2.38	0.15	0.0094
Total Measured & Indicated	139,500,000	0.42	2.41	0.17	0.0070
Inferred	30,200,000	0.34	1.89	0.15	0.0070

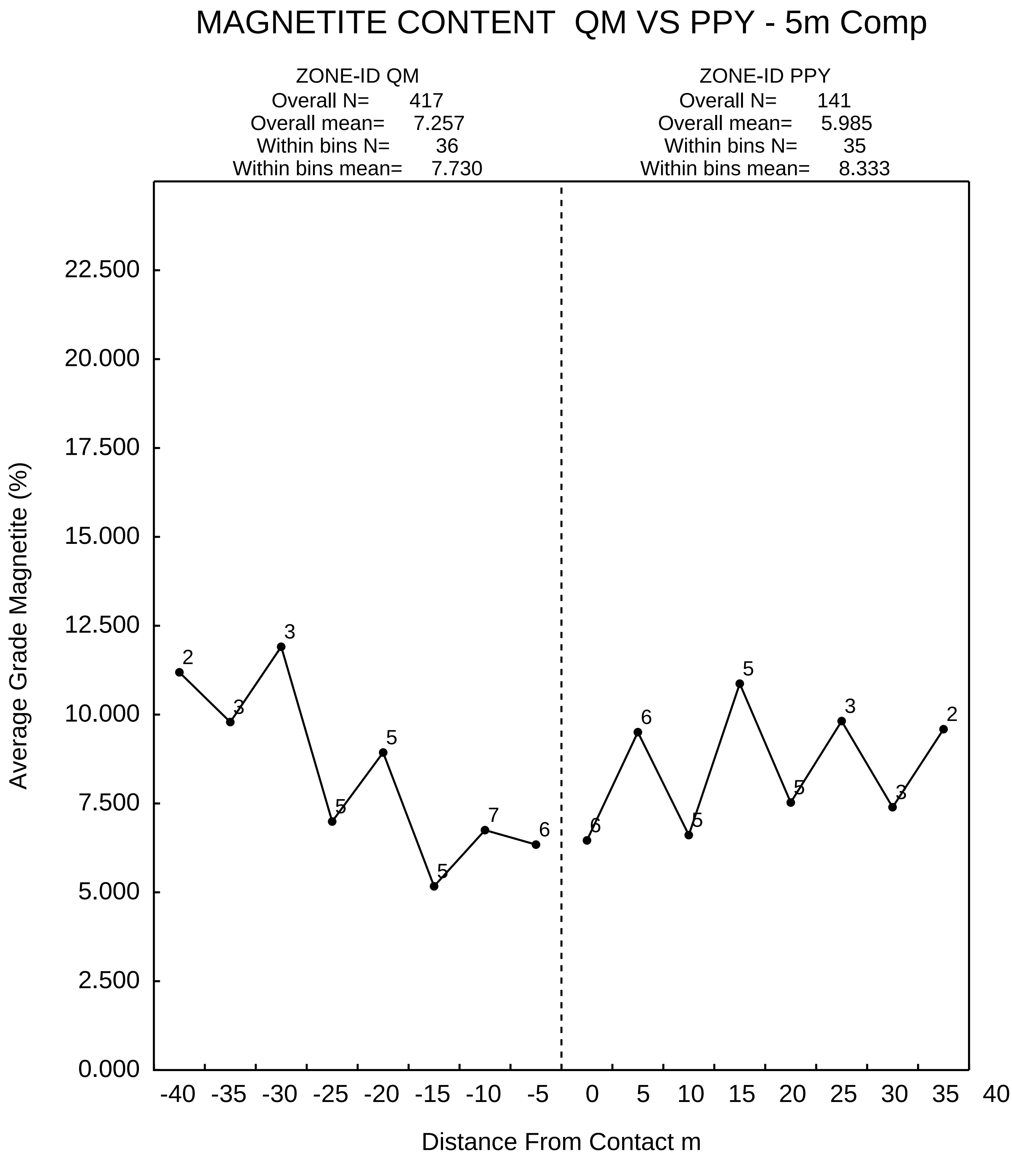
Case 2 2008 Bronson Slope Resource Estimate

Category	Metric Tonnes	Au g/t	Ag g/t	Cu %	Mo %
Measured	74,800,000	0.45	2.31	0.17	0.0059
Indicated	150,300,000	0.31	2.17	0.13	0.0087
Total Measured & Indicated	225,100,000	0.36	2.22	0.14	0.0077
Inferred	91,600,000	0.27	1.76	0.13	0.0080

For further details of on mineral resource calculations refer to “Mineral Resource Estimate – Bronson Slope Deposit”, dated April 30, 2008, authored by G. H Giroux, P. Eng., from Giroux Consultants Ltd and A. A. Burgoyne, P.Eng., M.Sc. from Burgoyne Geological Inc., and posted on SEDAR(www.sedar.com).



MAGNETITE CONTENT QM VS US - 5m Comp
ZONE-ID QM
Overall N= 417
Overall mean= 7.257
Within bins N= 52
Within bins mean= 5.171
ZONE-ID US
Overall N= 550
Overall mean= 0.845
Within bins N= 46
Within bins mean= 3.730
Average Grade Magnetite (%)
Distance From Contact m


MAGNETITE CONTENT QM VS PPY - 5m Comp
ZONE-ID QM
Overall N= 417
Overall mean= 7.257
Within bins N= 36
Within bins mean= 7.730
ZONE-ID PPY
Overall N= 141
Overall mean= 5.985
Within bins N= 35
Within bins mean= 8.333
Average Grade Magnetite (%)
22.500
20.000
17.500
15.000
12.500
10.000
7.500
5.000
2.500
0.000
2
3
3
5
5
5
7
6
6
6
5
5
5
3
3
2
-40 -35 -30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30 35 40
Distance From Contact m

18.0 Other Relevant Data and Information

18.1 Current (2008-2009) Mine Development Studies

During 2008 and 2009 several mine engineering and mine development studies were initiated and completed. In **Items 19** and **20** conclusions and recommendations are put forward for their continuance and completion. During December 2009 Skyline (Skyline Gold Press Release December 2, 2009) announced that they have retained SRK Consulting (Canada) Inc. to prepare a study identifying the required project elements, cost, and timing to complete a feasibility study technical report for the Bronson slope project. These studies, including the 2009 Bronson Preliminary Economic Assessment Technical Report (note below) completed by Leighton Asia, will be reviewed by SRK and compared to feasibility requirements through a matrix analyses to provide an estimate of the current project baseline status and also timeline, budget and project elements to complete the feasibility study phase.

The singly most important study completed was the Preliminary Economic Assessment (PEA) report on Bronson Slope by Leighton Asia (Lawrence and Seen, 2009) in March 2009. A summary of the results of this study are reported below:

Preliminary Economic Assessment (Scoping Study) by Leighton Asia

The Preliminary Assessment completed in March 2009 (Lawrence and Seen 2009) and Skyline Gold Press Release February 19, 2009) is intended to investigate conceptual plans and costing for the development of infrastructure, and the mining and processing of the resource considered to be economical. The report comprises an economic analysis of the deposit and includes a mine plan and project cost estimate showing positive economics and a basis for further advancement of the project. An economic analysis of the Bronson Slope project is based upon an open pit operation with in-pit crushing and an electrically powered conveyor system descending approximately 500 m from the pit to a 15,000 tonne per day (5.1 million tonnes per year) copper flotation and gravity gold separation processing plant. Tailings will be carried to the tailings facility by tailing pipeline. The PA mine plan and economic model for the base case includes a Life of Mine (LOM) mine production schedule of 93.5 million tonnes of mill feed that averages 0.155% copper, 0.446 g/t gold, 2.34 g/t silver and 0,0058% molybdenum, 78.5 million tonnes of waste and an average strip ratio of 0.83 over an 18.4 year mine life. It should be noted that mineral resources that are not mineral reserves do not have demonstrated economic viability. Metal recoveries from mill feed utilized in the PA are based upon prior metallurgical studies of the Bronson Slope deposit and are Gold: 85.4%, Copper: 86.6%, Silver: 63.7%.

Power costs are based on grid tariff power prices and set at CAD 0.055 per kilowatt-hour. Power is assumed to be supplied at Highway 37 from the proposed Northern Transmission Line for which the environmental permitting process is underway. Skyline Gold has also submitted hydro license applications in 7 regional catchments with a total potential generation capacity of 72 MW of power. Preliminary hydro-generation studies on two sites covered by the applications, which are within 10 km of the Bronson Slope deposit, have indicated the two sites have the potential capacity to generate a combined total of 29 MW of power. These sites have been further studied to determine the potential amount of electrical generation with storage added and indicate, on a preliminary basis, an ability to provide the power required by the Bronson Slope project. Further detailed technical studies and a feasibility study are required to confirm capacity and viability of these projects.

It is estimated that the Bronson Slope project will provide 201 jobs during years 1 to 8 of operation and 184 jobs during years 9 to 18. The base case project annual and total metal production is estimated at:

	Year 1 – 8 Average Production	**Year 9 – 18 Average Production**	**Life of Mine Yearly Average**	**Total Production**
Gold	73,400 oz.	54,400 oz.	62,800 oz.	1.13 million oz.
Copper	13.1 million lb.	14.4 million lb.	14.1 million lb.	254 million lb.
Silver	272,800 oz.	224,300 oz.	245,800 oz.	4.43 million oz.

The project economic model utilizes base case life-of-mine (LOM) average metal prices of (USD) $ 700/oz. gold, $ 2.00/lb. copper, and $ 15/oz. silver and an exchange rate of 0.85 USD/CAD.

Life of Mine (LOM) gold cash cost, net of byproduct credits using base case metal prices, is (USD) $232/oz. With production costs distributed pro-rata by revenue generated by each metal produced, LOM average cash costs of production are:

	Gold [USD /oz.]	**Copper** [USD /lb.]	**Silver** [USD /oz.]
Project Cash Costs	$428	$1.24	$9.28
Cash cost net of copper and silver credits	$232		

LOM average operating costs are:

	CAD / tonne Milled	**USD / tonne Milled**
Direct Mining Costs	$ 3.14	$ 2.67
Overhead and Administration	$ 0.98	$ 0.83
Processing Costs	$ 5.23	$ 4.45
Total:	**$ 9.34**	**$ 7.94**

Base case estimated project construction capital costs of CAD $237 million (USD $201.5 million) include a 15% contingency and with CAD $14 million in working capital give a total initial capital (peak investment) requirement of CAD $251 million (USD $213 million). Estimated life-of-mine sustaining capital is CAD $21.3 million excluding reclamation costs and salvage recovery of capital. Including reclamation costs (CAD $10 million) and salvage recovery of capital at closure, the life-of-mine sustaining capital requirement is CAD $15.7 million. The financial model is:

Project economic measures are:

Project IRR (before tax):	11 %
Project IRR (after tax):	10 %
Project NPV @ 7.5% discount (before tax):	CAD $59.3 million
Project NPV @ 7.5% discount (after tax):	CAD $38.3 million
Project NPV @ 0 % discount (before tax):	CAD $351.1 million
Project NPV @ 0 % discount (after tax):	CAD $279.4 million
Project Payback:	8.2 years
Mine life:	18.4 years

The report contains recommendations to advance the project and increase the project's economic return:

1. Re-optimizing the open-pit "Whittle" model utilizing operating and capital cost details and an optimized mine plan generated during this PA of the Bronson Slope results in enhanced returns. Increased potential returns (increased IRR) and faster payback of a smaller, higher grade mined resource (reduction of waste: ore ratio) and/or increased mine/mill throughput per year were identified by the Whittle model using updated inputs from the base case PA. Further work is recommended.

2. Development of a magnetite resource component in the Bronson Slope N.I. 43-101 compliant mineral resource estimate. The ability to produce a magnetite product from Bronson Slope mill feed offers the potential to increase the project's estimated economic returns.

Metallurgical Studies

- The metallurgical study and metal recoveries by BC Mining Research Limited on the High Wall Zone of gold mineralization (Klein 2008) were completed and are noted in **Item 16**.
- A study by BC Mining Research Ltd. to assess the amenability of Bronson Slope Cu-Au-Ag-Mo mineralization to pre-concentration and to assess the economic impacts (scoping study) on the Bronson Slope was undertaken during 2008 and 2009
- The completion of an Iron Magnetite Study by BC Mining Research Limited, **as** detailed in **Item 16.**

Road Construction Studies

Note Item 5.2. A comprehensive report entitled "Bronson Creek Access Road, Bridges and Environmental Considerations, Schedule K SUP Application" prepared by Forsite Engineering (2008) was completed and a Special Use Permit (SUP) Application was made to the BC Government to construct an access road from the Forest Kerr access road to the Bronson Slope deposit. Skyline is also working with AltaGas to define a mutual Road Use Agreement between the companies.

Hydroelectric Power
A summary discussion of Skyline Gold progress is outline **in Item 5.3**.

Other Project Development Work

- Skyline Gold has submitted its Bronson Slope Project Description to the BC Environmental Assessment Office and the federal Canadian Environmental Assessment Agency.
- Skyline Gold is working with the Tahltan and Iskut First Nations Chief and Tahltan Central Council and communities near the Bronson Slope project to develop strong and productive relations during the consultation process and during the development, operation and reclamation phases of the project.

18.2 Historical Mine Development Studies

Skyline previously completed a substantial amount of engineering scoping, environmental, cash flow, metallurgical, capital and operating costs, geotechnical, infrastructure and access, and other pre-feasibility studies on the Bronson Slope deposit from 1995 through 1997. The studies are referred to as feasibility studies in the Skyline correspondence of the day – they are, however, today better considered as historical pre-feasibility and engineering /development studies. Yeager (2006) reports that in the order of $3.5 million in 2006 dollars, similar to that spent on mineral exploration, was spent on development and pre-feasibility studies. **Table 18-1,** modified from Yeager (1998a) lists the studies completed and should be used in conjunction with **Item 21, References.** The writers have not made an extensive review of these historical development studies other than the resource and metallurgical/mill reports which are detailed in **Items 6** and **16**, respectively.

The environmental studies provide useful environmental background and monitoring studies for any future development work. The hydroelectric power and road studies, of course, are useful for future development/production but are now historical in nature and have been updated by Skyline, in part, as discussed in **Item 18.1**.

The mine studies including Acid Rock Drainage (ARD), mine design, geotechnical assessment and open pit slope design, tailings and water management illustrated that an open pit mining operation at Bronson Slope is feasible and positive from a technical perspective; however, the criteria and parameters developed from these studies are, at this point, historical in nature and are being confirmed by Skyline with updated studies.

It is cautioned that as future development occurs at Bronson Slope, all of the above studies will need to be revisited and, in light of their historical nature, will probably require substantial up dating to current engineering practise and methods and economics. These reports are of limited relevance today and are reported in **Table 18-1** for information purposes only.

TABLE 18-1
HISTORICAL DEVELOPMENT STUDIES ON BRONSON SLOPE DEPOSIT

Author	Date	Subject Report
		ENVIRONMENTAL
Bronson Slope Environmental Assessment Committee	June 18, 1996	Bronson Slope Mine Project Final Report Specifications
Keystone Wildlife Research	Oct. 10, 1996	Wildlife Habitat Evaluation for the Bronson Slope Mine
Norecol, Dames and Moore Inc.	Oct. 31, 1997	Bronson Slope Project Aquatic Environmental Impact Assessment
Woznow, D.P.	March 1997	Bronson Slope Mine Baseline Environmental Monitoring Protocols
		FINANCIAL & OPERATING COSTS
Ganshorn, J.A.	May 1, 1997	Bronson Slope Project Copper (Au+Ag), Molybdenum, Magnetite Marketing Reports
International Skyline Gold Corporation	December 11, 1997	Bronson Slope Project, (Cash Flow) Case Studies
Moore, M.	December 8, 1997	Bronson Slope Project Capital Cost Estimates Based on Amendments of Rescan Draft
		INFRASTRUCTURE & POWER
Brazier-Vera Associates	July 1995	Bronson Slope Project Power Supply Options
Klohn Leonoff Consulting Engineers Ltd.	March 1991	Iskut Road Study, Vol. IV Engineering Studies
Sigma Engineering Ltd.	January 1997	Bronson Slope Project Iskut Hydro Study
		MINE
International Skyline Gold Corporation	May 15, 1997	Summary of ARD Characterization of Bronson Slope Rock Samples
International Skyline Gold Corporation	June 1998	Interpretation of Results of ARD Kinetic Testing of Bronson Slope Rock Samples
International Skyline Gold Corporation	July 1998	Compilation of Draft Submissions of the Bronson Slope Feasibility Study from Rescan Engineering Ltd.
International Skyline Gold Corporation / Azimuth Management Consulting	January 1998	Bronson Slope Mine Project Report (Draft)
Piteau Associates	March 1997	Bronson Slope Project Preliminary Geotechnical Assessments and Slope Design Studies for the Bronson Slope Open Pit
Process Research Associates	April 29, 1997	Acid Base Accounting Test Results Bronson Slope Project
Steffen, Robertson and Kirsten Consulting Eng	August 13, 1997	Bronson Slope High Wall – Revised ARD Modelling
		METALLURGY & MILL FACILITIES
Process Research Associates	Jul 18, 1997	Bronson Slope Project Metallurgy Study on the Bronson Slope Samples
Rescan Engineering Ltd.	March 1995	Preliminary Feasibility Study Mill Facilities
		RESOURCE
International Skyline Gold Corporation	July 11,1996	Mineral Resource Inventory, 250 m Search Radius Model, Corrected Topography
Giroux, G.H.	1996 & 1997	Resource Estimates **- Note Items 17 & 21 in this Report**
Raymond, G.P.	July 15, 1997	Geostatistical Study of Drilling to May, 1997 and Recommended Drill Spacing, Bronson Slope Deposit
		TAILINGS
Agra Earth & Environmental Ltd	April 15, 1997	Tailings & Water Management System on Feasibility Design Bronson Slope Project
Agra Earth & Environmental Ltd	May 1997	Seismic Refraction Investigation, Bronson Slope Project
Dick, R.C.	February 25, 1997	Bronson Slope Project Site Investigations, Discussion of Results
Piteau Engineering Ltd.	January 1997	Conceptual Design (and Costs) of Tailings Facility

19.0 Interpretation & Conclusions

1. The authors have completed a detailed technical review and a mineral resource estimate of the magnetite content of the Bronson Slope Au-Cu-Ag-Mo deposit. The preparation of this technical report included certain due diligence procedures. It is concluded that the technical fieldwork, and office data compilation, including historical exploration surveys and procedures, diamond core drilling, analyses, and reporting of data, completed by Skyline, is of good quality and meets good practice industry standards.

2. Historical exploration programs, included drilling, geological mapping, and induced polarization surveys, undertaken by Skyline in the period of 1988 through 1997, was to outline, define, and expand bulk tonnage porphyry style gold-copper-silver-molybdenum mineralization found in the Red Bluff Porphyry and intruded feldspathic greywackes of the Stuhini Group of Upper Triassic age. Secondary historical objectives included completion of resource evaluation and mine engineering and development studies.

3. The porphyry copper-gold-silver-molybdenum deposit, hosting magnetite mineralization, occurs over a 1.5 km long northwest-southeast stratigraphic trend and is in the order of 0.6 km thick. The magnetite mineralization is mostly restricted to the Quartz Magnetite and Red Bluff Porphyry Units although significant magnetite can be found in Upper Sediments adjacent to these above Units.

4. A current mineral resource for magnetite has been estimated for the Bronson Slope deposit that meets CIMM resource standards and classifications. The resource estimate, based on block modelling and kriging is considered reliable and relevant.

BRONSON SLOPE – GLOBAL MAGNETITE MINERAL RESOURCE

Cut Off 2% Magnetite

Category	Metric Tonnes	% Magnetite	Contained Tonnes Magnetite
Measured	66,210,000	7.58	5,020,000
Indicated	96,950,000	7.08	6,860.000
Total Measured + Indicated	**163,160,000**	**7.28**	**11,880,000**
Inferred	6,300,000	6.92	440,000

5. The 2% magnetite cut off used as a base case for resource estimation is based on milling and truck transportation cost information supplied by Skyline Gold (Jensen 2010a) which yielded a price of $130 per tonne net of milling and transportation charges. This price is based on market analysis (Klein 2008) – see Appendix D and as well as discussions with Craigmont Mines that produces magnetite powder for dense media separation coal cleaning. The estimated break-even cut-off grade is less than 2% on a by-product basis. It must be stressed that the economics are also dependent on the ability to market and sell magnetite.

6 It should be noted that when this global magnetite resource is compared to the preliminary open pit designed for the Preliminary Economic Assessment completed by Leighton Asia (Lawrence and Seen, 2009) in March 2009 that 44% of the measured and indicated magnetite tonnage, above a 2% cut-off, is within the pit. The remainder sits below and to the west. As a result it is our recommendation that a new PEA be completed using the magnetite results to demonstrate the changes in project economics as noted below.

7. Skyline Gold's internal studies (Jensen, 2010b) indicate that at a 7% magnetite by weight economic cut-off based upon the 2009 Bronson Slope PEA (Lawrence and Seen 2009) and the 2008 magnetite study by Klein (2008) is potentially viable on a stand-alone production basis and assuming that magnetite is the only mineral produced at Bronson Slope. At this cut-off Bronson Slope Measured and Indicated magnetite resource is 100,640,000 tonnes grading 8.8% magnetite for a total Measured and Indicated estimate of 8,900,000 tonnes of contained magnetite. It is reasonably expected that, on a by-product production basis, the magnetite economic cut-off grade would be lower and the magnetite resource estimate at lower cut-off grades is shown in the above tables.

8. Klein (2008) completed metallurgical testing from bulk samples obtained from drill core from the Quartz Magnetite Unit of the Bronson Slope deposit. The testing confirmed the metallurgical process, determined the grinding work index from regrinding and characterized the magnetite product with respect to the specifications. The testing involved grinding and flotation to recover copper sulphides. The flotation tailings were used for magnetic separation testing. Klein (2008) also completed metallurgical and marketing studies with respect magnetite that could be recovered from the Bronson Slope deposit. The market study estimated the amount of magnetite used for BC and Alberta Coal industries for dense media separation and the metallurgical study assessed the properties of the Bronson Slope magnetite use in dense media. Dense media separation is a process in which finely ground magnetite is mixed with water to create a medium that has properties of a dense liquid.

9. Resource estimation to date has largely focussed on the Quartz Magnetite Unit and the Red Bluff Porphyry for definition of magnetite mineralization. There is excellent potential for defining addition magnetite mineralization and resource along the trend extension of the Quartz Magnetite unit and Red Bluff Porphyry unit to the west, east and to depth.

10. During 2009 work focussed primarily on completion of drill hole sampling and analyses to estimate a magnetite resource, the drilling of two drill holes over 729 meters on the Snip 1 claim 900 m east of Bronson Slope deposit, and completion of a Preliminary Economic Assessment Study (PEA), and other mine development studies. SRK Consulting Inc. was engaged to complete a gap study, identifying the required project elements, cost, and timing to complete a feasibility study, for the Bronson Slope project.

11. The primary objective for 2010 should include:

- A revised preliminary economic assessment (PEA) report including a review and revision of the open pit design model, that includes the evaluation of the magnetite resource; this will determine what amount of the magnetite resource can be included and extracted, subject to marketing considerations and studies, in a revised preliminary open pit design.
- Since magnetite is an industrial mineral, the amount that can be marketed and its price per metric tonne can only be determined by definition of sales agreements and marketing studies.
- Complete the SRK gap study that is currently underway such that all aspects necessary for a full feasibility study can be commenced. Confirm the SRK gap study, as part of the PEA update, to include magnetite.

12. Future development work on Bronson Slope deposit is subject to the recommendations of the on going SRK study and Skyline should now focus primarily on continuation of further mine and development studies as outlined in **Item 20**.

20.0 Recommendations

The Bronson Slope deposit and property should be advanced through further mine development programs. It is the opinion of the authors that the character of the defined porphyry copper-gold-silver-molybdenum deposit, with the associated magnetite content, when considered in terms of current relatively high precious and base metal prices, are of sufficient merit to warrant the following programs as detailed below.

The Preliminary Economic Assessment Study (PEA) and pit design study, initiated in mid 2007, and completed in early 2009 has defined the economic potential of the deposit and the property and this is discussed in **Item 18.** The PEA has yielded a potential economic rate of return and has given several recommendations to enhance the economics of the property, of which the estimation of a magnetite resource, and completion of a gap analysis to identify specific data requirements and level of effort to advance the project to a pre or feasibility level, have been undertaken or are underway. Skyline should now focus primarily on future mine and development studies. The recently discovered and defined zone of gold-silver mineralization on the Snip 1 mineral tenure some 900 meters east of the most easternmost drill holes on Bronson Slope deposit is significant but requires the completion of a technical report by Equity Engineering such that the appropriate recommendations can be made. The objective of the below mine development programs is for Skyline to initiate and complete an Environment Assessment Report (EAR) for submission to the BC Government and the Ministries of Environment and Energy, Mines and Petroleum Resources. The following recommendations, as initially proposed in the PEA, are warranted and include:

- A revised preliminary economic assessment report including a review and revision of the open pit design model, that includes the evaluation of the magnetite resource, should be completed; this will determine what amount of magnetite can be included in a revised preliminary open pit design along with magnetite marketing considerations. This is estimated to cost from $100,000 to $150,000;

- Since magnetite is an industrial mineral, the amount that can be marketed and its price per metric tonne can only be determined by definition of sales agreements and marketing studies;

- Further metallurgical work should be completed on the magnetite mineralization to define metallurgical recoveries in the different rock units;

- Continuation of mine development studies recommended by the gap study currently being undertaken by SRK;

- Depending on the gap analysis study results by SRK, initiate a Pre-Feasibility or Feasibility Study. Such study to include magnetite and molybdenum recovery;

- Implement project changes requested on Environmental Assessment (EA) permitting process by BC EAO on previously submitted project description and advance EA process with BC EAO and CEAA.

- Negotiate a Participation Agreement with the Tahltan Band and Iskut First Nation;

- Prepare a Feasibility Study for Skyline Gold's local hydro license applications for self-generation hydropower for the Bronson Slope project.

21.0 References

The following references have been used in preparing the Technical Report. Skyline completed a substantial amount of engineering scoping, environmental, cash flow, metallurgical, capital and operating costs, geotechnical, infrastructure and access, and other pre-feasibility studies on the Bronson Slope deposit from 1995 - 1997 and these are listed in **Table 18-1** in **Item 18.**

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22.0 Signature Page

The report titled “Technical Report – Magnetite Mineral Resource Estimate for Skyline Gold Corporation On The Bronson Slope on the Property, North Western British Columbia, Canada” dated January 15, 2010 was prepared and signed by the following authors.

“A.A. Burgoyne” {Signed and Sealed}

Dated at North Saanich, British Columbia
January 28, 2010

A. A. Burgoyne, P.Eng., M.Sc.,

Burgoyne Geological Inc.

“Arnd Burgert” {Signed and Sealed}

Dated at North Saanich, British Columbia
January 28, 2010

Arnd Burgert, P.Geo., B.Sc.,

Arnd Burgert Consulting Ltd.

“*G.H. Giroux” {Signed and Sealed*}

Dated at Vancouver, British Columbia
January 28, 2010

G.H. Giroux, P.Eng., M.ASc.,

Giroux Consultants Ltd.

23.0 Certificate - Statement Of Qualified Persons

BURGOYNE GEOLOGICAL INC.
Consulting Geologists & Engineers

548 Lands End Road
North Saanich, BC, Canada
V8L 5K9
TEL / FAX (250) 656 3950

A.A. (Al) Burgoyne, M.Sc., P.Eng.

I Alfred A. Burgoyne hereby certifies:

1. I am an independent consulting Geologist employed by Burgoyne Geological Inc. with residence and office at 548 Lands End Road, North Saanich, BC, CANADA, V8L 5K9.
2. I graduated from the University of British Columbia in 1962 with a Bachelor of Science Degree in Geology and from the University of New Mexico in 1967 with a Master of Science Degree in Geology.
3. I am a registered Professional Engineer in the Association of Professional Engineers and Geoscientists for the Province of British Columbia and am registered as a Fellow of the Geological Association of Canada.
4. I have practiced my profession for 45 years and have been involved in mineral exploration and development in Canada, USA, Latin America, Southeast and Central Asia, and Eastern Europe.
5. During this period of professional practice I have been extensively involved in the exploration, discovery, definition, and development phases of no less than five major porphyry copper-gold deposits in British Columbia.
6. Prior to establishing Burgoyne Geological Inc. in 1991 I held several successive positions from 1980 to 1991 as Vice President-Exploration for Breakwater Resources Ltd., Western Canadian Mining Corporation, Cassiar Mining Corporation and Bethlehem Copper Corporation. From 1970 to 1979, I was Exploration Manager of Western Canada for UMEX Corp.
7. During my tenure with the above companies I have been intimately involved in the drilling definition and evaluation of all styles of porphyry style mineralization having been responsible for exploring and discovering and/or extending five major deposits of which two attained production.
8. I have read the definition of “qualified person” set out in National Instrument 43-101 and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a “qualified person” for the purposes of NI 43-101.
9. The report dated January 28, 2010 and titled “Technical Report – Magnetite Mineral Resource Estimate for Skyline Gold Corporation On The Bronson Slope Property, North Western British Columbia, Canada” is based on about five weeks of technical evaluation in September 2009 through January 2010. The writer has written Items 2 through 10, 15, 16, 18, and 21. Items 1, 19, and 20 have been jointly written.
10. Site examinations and evaluations, on the Bronson Property, were made on October 1 to 3, 2009, October 13 and 14, 2007 and September 11, and October 14 to 16, 2006. The writer evaluated the property with respect to drill hole locations, geology, mineralization, and general infrastructure was reviewed. The sources of all information not based on personal examination are quoted in the report. The information provided by the various parties is to the best of my knowledge and experience correct.

11. That as of the date of this certificate, to the best of the qualified person's knowledge, information and belief, the technical report contains all scientific and technical information that is required to be disclosed to make the technical report not misleading.
12. Numerous maps and sections, especially in respect to mineral resource were supplied by Skyline Gold Corporation and reviewed.
13. I am independent of the issuer applying all the tests in section 1.4 of National Instrument 43-101
14. I have read National Instrument 43-101 and Form 43-101Fl and the Technical Report has been prepared in compliance with that instrument and form.

Dated at North Saanich, British Columbia this 28 th day of January, 2010.

"A.A. Burgoyne" {signed and sealed}

A.A. Burgoyne, P.Eng.

Independent Qualified Person

CERTIFICATE G.H. Giroux

I, G.H. Giroux, of 982 Broadview Drive, North Vancouver, British Columbia, do hereby certify that:

1) I am a consulting geological engineer with an office at #1215 - 675 West Hastings Street, Vancouver, British Columbia.
2) I am a graduate of the University of British Columbia in 1970 with a B.A. Sc. and in 1984 with a M.A. Sc., both in Geological Engineering.
3) I am a member in good standing of the Association of Professional Engineers and Geoscientists of the Province of British Columbia.
4) I have practised my profession continuously since 1970. I have had over 30 years experience calculating mineral resources. I have previously completed resource estimations on a wide variety of deposits many similar to Bronson Slope.
5) I have read the definition of "qualified person" set out in National Instrument 43-101 and certify that by reason of education, experience, independence and affiliation with a professional association, I meet the requirements of an Independent Qualified Person as defined in National Policy 43-101.
6) This report titled "Technical Report – Magnetite Mineral Resource Estimate for Skyline Gold Corporation On The Bronson Slope Property, North Western British Columbia, Canada" dated January 28, 2010, is based on a study of the data and literature available on the Bronson Slope Property. I am responsible for the Item 17. I have not visited the property.
7) I have previously completed resource estimates on this property in 1996 and 2007 and 2008.
8) As of the date of this certificate, to the best of my knowledge, information and belief, the technical report contains all scientific and technical information that is required to be disclosed to make the technical report not misleading.
9) I am independent of the issuer applying all of the tests in section 1.4 of National Instrument 43-101.
10) I have read National Instrument 43-101 and Form 43-101F1, and the Technical Report has been prepared in compliance with that instrument and form.

Dated this 28 th day of January 2010.

"G. H. Giroux" {Signed and Sealed}

G. H. Giroux, P.Eng., MASc.

ARND BURGERT CONSULTING LTD.

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Ladysmith, BC, Canada
V9G 1N9
TEL (250) 245 9712

Arnd Burgert, P.Geo.

I Arnd Burgert hereby certify that:

1. I am an independent consulting Geologist employed by Arnd Burgert Consulting Ltd. with residence and office at 921 Colonia Drive, Ladysmith, BC, Canada, V9G 1N9.
2. I graduated from the University of British Columbia in 1995 with a Bachelor of Science Degree in Geology.
3. I am a registered Professional Geoscientist in the Association of Professional Engineers and Geoscientists for the Province of British Columbia.
4. I have practiced my profession for 19 years and have been involved in mineral exploration and development in western and northern Canada.
5. I have read the definition of "qualified person" set out in National Instrument 43-101 and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
6. This report titled "Technical Report – Magnetite Mineral Resource Estimate for Skyline Gold Corporation On The Bronson Slope Property, North Western British Columbia, Canada" dated January 28, 2010, is based on a study of the data and literature available on the Bronson Slope Property. I am responsible for Items 11 through 14 and have jointly authored Items 1, 19 and 20.
7. That as of the date of this certificate, to the best of the qualified person's knowledge, information and belief, the technical report contains all scientific and technical information that is required to be disclosed to make the technical report not misleading.
8. I have read National Instrument 43-101 and Form 43-101Fl and the Technical Report has been prepared in compliance with that instrument and form.
9. During the period of October 1 through 21, I was Project Geologist and Manager at the Bronson Slope Campsite and supervised the core splitting and sampling program described in this report for magnetite analysis described in this report.

Dated at Ladysmith, British Columbia this 28 th day of January 2010.

"Arnd Burgert" {signed and sealed}

Arnd Burgert, P.Geo., B.Sc.

APPENDIX A
BRONSON SLOPE DIAMOND DRILL HOLE DATA
THOSE USED IN MAGNETITE RESOURCE ESTIMATE HIGHLIGHTED IN BLUE

Hole	Total Depth	Easting**	Northing**	Elevation	Azimuth**	Dip
	(metres)	(metres)	(metres)	(metres)	(degrees)	(degrees)
944	206.3	25569.6	11909.7	513.9	342	-50
945	48.0	25569.6	11909.7	513.9	342	-75
946	121.6	25569.3	11948.9	507.0	296	-45
947	78.9	25637.8	12174.5	315.0	270	-90
948	66.8	25637.8	12174.5	315.0	086	-70
949	123.4	25637.8	12174.5	315.0	266	-60
954	100.0	25064.3	12299.1	222.0	122	-46
955	91.1	25064.3	12299.1	222.0	112	-60
956	88.1	25015.0	12056.0	425.0	074	-60
957	118.6	25625.6	12044.9	403.0	287	-45
958	127.1	25064.3	12299.1	222.0	247	-45
959	108.8	26012.0	12237.0	261.0	107	-68
960	185.6	26160.2	12030.2	373.0	270	-90
961	133.2	25569.3	11948.9	507.0	296	-65
962	117.3	25569.3	11948.9	507.0	274	-46
963	115.5	24956.0	12316.0	196.0	270	-90
964	109.4	24956.0	12316.0	196.0	089	-44
1198	69.5	25700.0	11965.0	422.0	180	-55
1199	169.2	25700.0	11965.0	422.0	360	-69
1200	166.7	25700.0	12160.0	317.0	180	-45
1201	130.1	25700.0	12160.0	317.0	360	-59
1202	108.8	26100.0	12112.0	322.0	180	-45
1203	120.1	26100.0	12112.0	322.0	360	-55
1204	105.8	26100.0	12206.0	282.0	360	-55
1208	182.6	25430.3	11882.7	587.3	343	-84
1209	169.2	25417.6	11980.7	584.7	360	-82
1210	124.1	25208.4	11975.5	551.8	002	-74
1211	165.5	25208.6	11907.7	601.3	351	-82
1212	135.3	25049.4	11916.8	546.0	360	-75
1213	84.7	26500.0	11820.0	466.0	360	-79
1214	89.9	26350.0	11840.0	465.0	360	-75
1215	342.4	25311.6	11922.6	597.4	348	-54
1216	256.7	25208.8	11906.3	601.5	349	-60
1217	423.4	25367.0	11869.1	603.5	004	-59
1218	408.1	25367.0	11981.7	597.9	359	-56
1219	452.9	25500.0	11838.2	572.5	0	-63
1220	369.1	25600.8	11842.9	513.0	0	-55
1221	312.1	25117.2	11978.5	506.5	0	-54
1222	199.0	25367.0	11981.7	597.9	180	-54
1223	264.0	25015.0	12056.0	425.0	0	-60
1224	27.0	25064.3	12299.1	222.0	122	-46
1225	299.9	25260.2	12013.5	566.9	0	-57

1226	275.4	25500.0	11940.0	543.1	0	-55
1227	243.2	25700.0	11810.0	507.4	358	-60
1228	200.0	25900.0	11870.0	432.1	0	-55
1229	450.2	25299.7	11752.7	714.1	356	-59
1230	40.2	25700.0	11810.0	507.4	0	-90
1231	46.0	26048.5	11875.1	438.0	0	-82
1232	219.6	25550.0	11862.0	531.8	0	-83
1233	219.5	25793.0	11839.0	465.0	0	-60
1234	327.7	25300.0	11753.0	714.1	301	-54
1235	402.0	25884.0	11583.0	642.0	005	-59
1236	236.8	25884.0	11583.0	642.0	275	-47
1237	446.5	25300.0	11753.0	714.1	275	-45
1238	61.0	26042.0	11595.0	625.0	005	-50
1239	36.0	26042.0	11595.0	625.0	005	-60
1240	28.0	26050.4	11888.9	437.0	002	-82
1241	150.3	26050.0	11888.6	437.0	025	-89
1242	199.6	25994.1	11877.6	430.4	035	-49
1243	169.5	25993.0	11878.8	432.0	002	-54
1244	249.1	26133.3	11860.1	457.1	001	-59
1245	493.0	25487.0	11636.1	764.0	346	-61
1246	545.7	25490.9	11636.2	765.3	037	-61
S-06	107.6	24964.1	11662.6	775.0	0	-45
S-101	314.8	24943.5	11501.1	811.9	0	-45
S-125	404.0	24919.0	11555.2	798.9	0	-47
S-126	425.3	24919.0	11554.0	798.9	0	-75
S-127	461.9	25194.2	11570.1	804.7	0	-67
S-129	382.6	25502.3	11549.8	804.0	358	-60
S-130	233.2	25502.1	11550.7	804.2	357	-44
*BS0601	31.0	25348.906	11926.4	594.2	3.5	-60
*BS0602	138.6	25391.117	11974.0	598.6	0.5	-70
*BS0603	270.0	25355.665	11929.8	590.4	1.5	-59
*BS0604	122.0	25502.743	11938.7	545.5	0.5	-55
BS0701	466.3	25257.353	11945.09	585.7	186.2	-53.5
BS0702	393.2	25309.002	11988.067	591.2	174,7	-46.5
BS0703	295.7	25697,373	11912.865	457.8	170.6	-62.9
BS0704	360.6	25599.286	11904.387	497.6	236.5	-58.3
BS0705	429.8	25549.787	11931.24	524.3	169	59.4
BS0706	274.6	26050.062	11962.919	400.0	242.5	-64.5
BS0708	360.6	25352,538	11615.737	783.9	72.6	-69.5
BS0709	390.9	25399.105	11581.136	793.3	75.8	-63.5
BS0710	365.8	25355.031	11929.152	590.5	180.9	-50.0
BS0711	300.0	25053.848	11610.379	795.4	61.5	-76.0
BS0712	298.7	25747.113	11782.198	518.2	56.3	-69.0

* Holes also reported as 200601 to 200604

**** The Northing, Easting, and Azimuth values are based on Grid North which is 025° 12’ 22”**

* Year of Assay * Also know as 200601 through 200604

APPENDIX B

DRILL HOLE ANALYSIS FOR MAGNETITE

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 6-Nov-09
File Number: **A718180**

Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)
G1/ P.1	1.1		430468	BDL		430492	BDL			
430447	0.2		430469	BDL		430493	BDL			
430448	0.2		430470	BDL		430494	BDL			
G022505	1.3		G022506	0.6		430495	BDL			
430450	0.1		430472	BDL		430496	BDL			
430451	BDL		430473	BDL		430497	BDL			
430452	BDL		430474	BDL		430498	BDL			
430453	0.2		430475	BDL		430499	BDL			
430454	BDL		430476	BDL		430500	BDL			
430455	BDL		430477	BDL		430701	BDL			
430455	BDL	Repeat	430478	BDL		430702	BDL			
Standard	8.8	Standard	430479	BDL		430703	BDL			
430456	BDL		430480	BDL		430704	BDL			
430457	BDL		430481	BDL		430705	BDL			
430458	0.1		430482	0.1						
430459	BDL		430483	BDL						
RRE430459	BDL	Duplicate	430484	BDL						
430460	BDL		430485	BDL						
430461	BDL		RRE430485	BDL	Duplicate					
430462	0.1		430486	BDL						
430463	0.1		430487	BDL						
430464	BDL		430488	BDL						
430465	BDL		G022507	0.9						
430466	BDL		430490	BDL						
430467	0.1		430491	BDL						

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by: ______________________
Ishwinder Grewal, M.A.Sc. P.Er

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 6-Nov-09
File Number: A718162
Page 1 of 1

Sample Number	Magnetite (%)	Note
430363	6.1	
430364	6.8	
430365	5.2	
G022501	1.5	
430367	5.5	
430368	3.9	
430369	0.2	
430370	3.9	
430371	4.3	
430372	BDL	
430373	4.7	
430374	6.0	
430375	0.3	
RRE430375	BDL	Duplicate
430376	2.2	
430377	6.0	
430378	10.2	
430379	4.1	
430380	6.6	
430381	1.9	
430382	2.5	
430383	3.6	
430384	2.3	
430385	7.7	
G022502	1.0	

Sample Number	Magnetite (%)	Note
430387	3.8	
430388	1.9	
430389	3.7	
430390	1.9	
430391	6.5	
430392	4.5	
430393	1.7	
430394	2.5	
G-1**/P.2	0.9	
430395	4.7	
430396	7.9	
430397	4.3	
430398	6.7	
430399	6.8	
430400	3.0	
430401	5.7	
430402	6.9	
430403	8.8	
430404	3.1	
430405	4.1	
RRE430405	4.2	Duplicate
430406	6.8	
G1	0.9	
G022503	0.3	
430408	10.6	

Sample Number	Magnetite (%)	Note
430409	5.6	
430410	1.3	
430411	0.2	
430412	2.3	
430413	4.5	
430414	3.6	
430415	0.3	
430416	0.4	
430417	0.3	
430418	1.7	
430419	0.9	
430420	3.0	
430421	6.5	
430422	4.0	
430423	0.5	
430424	1.3	
RRE430424	1.9	Duplicate
430425	3.5	
G022504	2.1	
430427	2.9	
430428	5.2	
430429	2.7	
430430	2.1	
G-1** /P.3	1.0	
430431	2.4	

Sample Number	Magnetite (%)
430432	3.8
430433	1.6
430434	0.2
430435	BDL
430436	0.1
430437	0.1
430438	0.1
430439	0.1
430440	BDL
430441	0.1
430442	BDL
430443	BDL
430444	BDL
430445	0.2
430446	0.2

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

Davis Tube Magnetite Analysis Report

MET-SOLVE LABORATORIES INC.

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 10-Nov-09
File Number: A718183

Sample Number	Magnetite (%)	Note
G1/P.1	1.1	
430706	0.2	
430707	0.3	
430708	0.2	
430709	0.3	
430710	1.0	
430711	5.2	
430712	1.4	
430713	0.3	
430714	BDL	
430715	0.2	
430716	0.2	
430717	0.2	
430718	0.1	
430719	0.6	
430720	0.2	
430721	0.2	
430722	0.2	
430723	0.2	
430724	BDL	
430725	0.2	
RRE 430725	0.2	Duplicate
430726	0.2	
430727	0.2	
430728	0.2	

Sample Number	Magnetite (%)	Note
430729	0.1	
430730	0.1	
430731	BDL	
430732	1.4	
430733	BDL	
430734	0.1	
430735	0.2	
430736	0.1	
430737	BDL	
G-1**/P.2	1.0	
G022508	1.4	
430739	0.2	
430740	BDL	
430741	BDL	
430742	BDL	
430743	BDL	
430744	BDL	
RRE 430744	BDL	Duplicate
430745	BDL	
430746	0.2	
430747	BDL	
430748	BDL	
430749	BDL	
430749	BDL	Repeat
Standard	8.4	Standard

Sample Number	Magnetite (%)	Note
430750	BDL	
430751	BDL	
430752	BDL	
430753	BDL	
430754	BDL	
430755	0.1	
430756	BDL	
430757	BDL	
430758	BDL	
G022509	0.8	
430760	0.2	
430761	BDL	
430762	BDL	
430763	BDL	
430764	BDL	
430765	BDL	
430766	0.1	
430767	BDL	
430768	BDL	
430769	0.1	
G-1**/P.3	0.9	
430770	BDL	
430771	0.1	
430772	0.1	
430773	BDL	
430774	BDL	

Sample Number	Magnetite (%)
430775	0.3
430776	0.1
RRE 430776	BDL
430777	BDL
G022510	1.9
430779	BDL
430780	BDL
430781	BDL
430782	BDL
430783	BDL
430784	0.1
430785	BDL
430786	0.2
430787	BDL
430788	BDL
430789	BDL
430790	0.1
430791	BDL
430792	0.2
430793	0.1
430794	0.2
430795	BDL
430796	0.3
430797	0.2
430798	BDL
430799	0.1
G022511	1.3
430801	0.2

BDL: Below Detection Limit

ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by: ____________

Ishwinder Grewal, M.A.Sc. P.Eng.

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 16-Nov-09
File Number: A706608

Sample Number	Magnetite (%)	Note
G-1**/ P.1	0.9	
431084	0.2	
431085	0.4	
431086	0.2	
431087	0.2	
431088	0.6	
431089	0.2	
431090	BDL	
431092	BDL	
431093	0.2	
431094	0.2	
431095	0.4	
DUP 431095	0.2	Duplicate
431096	0.6	
431097	0.2	
RRE 431097	0.2	Duplicate
431098	0.6	
431099	0.1	
G022512	2.0	
431101	0.1	
431102	0.2	
431103	BDL	
431104	0.4	
431105	0.1	
431106	0.2	

Sample Number	Magnetite (%)	Note
431107	0.1	
431108	0.2	
431109	BDL	
431110	0.2	
431111	BDL	
DUP 431111	BDL	Duplicate
431112	0.8	
431113	0.2	
431114	BDL	
G-1**/ P.2	0.9	
431115	BDL	
431116	BDL	
431117	BDL	
431118	BDL	
431119	BDL	
431120	BDL	
431121	BDL	
G022513	0.8	
431123	BDL	
431124	BDL	
431125	BDL	
RRE 431125	BDL	
RRE 431125	0.2	Repeat
Standard	8.4	Standard
431126	0.6	

Sample Number	Magnetite (%)	Note
431127	BDL	
431128	1.3	
431129	BDL	
431130	BDL	
431131	BDL	
DUP. 431131	BDL	Duplicate
431132	BDL	
431133	BDL	
431134	BDL	
431135	BDL	
431136	0.1	
431137	BDL	
431138	BDL	
431139	0.1	
431140	BDL	
431141	0.2	
G022514	1.2	
431143	0.4	
431144	0.1	
431145	BDL	
G1/P.3	0.8	
431146	BDL	
431147	BDL	
RRE 431147	BDL	Duplicate
431148	0.2	

Sample Number	Magnetite (%)
431149	BDL
431150	BDL
431151	0.1
431152	BDL
431153	0.2
431154	BDL
DUP 431154	BDL
431155	BDL
431156	0.2
431157	BDL
431158	0.3
431159	BDL
431160	BDL
431161	BDL
431162	BDL
431163	BDL
G022515	2.0
431165	0.1
431166	0.1
431167	0.1
431168	BDL
431169	BDL
431170	0.1
431171	BDL
431172	BDL

BDL: Below Detection Limit

ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 16-Nov-09
File Number: A706608

Sample Number	Magnetite (%)	Note
431173	BDL	
431174	BDL	
DUP 431174	BDL	Duplicate
431175	BDL	
G1/P.4	0.7	
431176	BDL	
431177	BDL	
431178	0.1	
431179	BDL	
431180	BDL	
431181	BDL	
431182	BDL	
431183	BDL	
431184	0.1	
G022516	0.6	
431186	BDL	
DUP 431186	BDL	
431187	BDL	
431188	0.1	
431189	BDL	
431190	BDL	
431191	BDL	
431192	BDL	
431193	0.4	
431194	BDL	

Sample Number	Magnetite (%)	Note
431195	BDL	
431196	BDL	
DUP 431196	BDL	
431197	0.2	
431198	BDL	
431199	BDL	
431200	1.5	
431201	0.4	
431202	0.7	
431203	0.3	
431204	1.0	iss (10 g)
G022517	1.3	
431206	0.6	
G1/P.5	0.9	
431207	0.1	
431208	4.1	
431209	0.1	
431210	0.7	
431211	BDL	
431212	BDL	
431213	0.2	
431214	0.6	
DUP 431214	0.6	
431215	BDL	
431215	0.1	Repeat

Sample Number	Magnetite (%)	Note
Standard	8.5	Standard
RRE 431215	BDL	
431216	0.5	
431217	0.2	
431218	0.5	

Sample Number	Magnetite (%)

BDL: Below Detection Limit

ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Nov-09
File Number: SMI0700000(

Sample Number	Magnetite (%)	Note
G1/P.1	1.1	
430929	BDL	
430930	4.3	
430931	2.9	
430932	1.0	
430933	-	ISS
430934	4.5	
430935	1.5	
430936	2.0	
430937	1.8	
430938	0.9	
430939	4.1	
430940	1.6	
430941	2.1	
430942	0.6	
430943	1.4	
430944	1.2	
RRE430944	1.3	Duplicate
430945	0.6	
430946	0.7	
430947	0.6	
430948	0.6	
430949	0.2	
430950	0.8	
430951	0.2	

Sample Number	Magnetite (%)	Note
G022518	2.0	
430953	2.1	
430954	1.9	
430955	0.6	
430956	0.3	
430957	0.4	
430958	0.2	
430959	BDL	
430960	0.3	
430961	0.2	
430962	0.7	
430963	0.9	
430964	0.2	
430965	0.3	
430966	BDL	
430967	0.1	ISS (15 g)
430968	0.2	
430969	1.1	
430970	0.7	
G022519	1.3	
430972	0.4	
430973	1.6	
430974	BDL	
430975	BDL	
430976	BDL	

Sample Number	Magnetite (%)	Note
DUP 430976	0.1	Duplicate
430977	0.1	
430978	0.2	
430979	BDL	
430980	BDL	
430981	0.1	
430982	0.2	
430983	0.1	
430984	BDL	
430985	BDL	
430986	0.1	
430987	BDL	
430988	BDL	
G022520	1.9	
430990	BDL	
430991	BDL	
430992	BDL	
430993	BDL	
430994	0.2	
430995	0.1	
430996	BDL	
430997	BDL	
430998	0.1	
430999	BDL	
431000	BDL	

Sample Number	Magnetite (%)
DUP 431000	BDL
431001	BDL
431002	BDL
431003	0.2
431004	BDL
431005	BDL
431006	BDL
431007	BDL
431009	BDL
431010	BDL
431011	BDL
431012	BDL
431013	BDL
431014	BDL
431015	BDL
431016	BDL
431017	BDL
431018	BDL
431019	BDL
431020	BDL
431020	BDL
Standard	8.3
431021	BDL
431022	BDL
431023	BDL

BDL: Below Detection Limit

ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

Davis Tube Magnetite Analysis Report

MET-SOLVE LABORATORIES INC.

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Nov-09
File Number: SMI0700000(

Sample Number	Magnetite (%)	Note
431024	BDL	
431025	BDL	
431026	0.1	
431027	BDL	
431028	BDL	
G022521	1.3	
G022522	0.7	
431030	BDL	
431031	BDL	
431032	BDL	
431033	0.1	
431034	0.1	
431035	BDL	
431036	BDL	
431037	BDL	
431038	0.2	
431039	BDL	
DUP 431039	BDL	Duplicate
431040	BDL	
431041	BDL	
431042	BDL	
431043	BDL	
431044	BDL	
431045	BDL	
431046	BDL	

Sample Number	Magnetite (%)	Note
431047	BDL	
431048	BDL	
431049	BDL	
G022523	1.8	
431051	BDL	
431052	BDL	
431053	0.1	
431054	BDL	
431055	BDL	
431056	BDL	
431057	BDL	
431058	0.2	
431059	0.1	
431060	0.1	
431061	BDL	
431062	BDL	
431063	BDL	
431064	BDL	
431065	0.2	
431066	0.2	
431067	0.1	
431068	BDL	
G022524	1.1	
431070	BDL	
G022525	0.8	

Sample Number	Magnetite (%)	Note
431071	BDL	
431072	0.3	
431073	0.2	
431074	0.1	
431075	BDL	
431076	0.2	
431077	0.1	
431078	0.1	
431079	0.1	
431080	BDL	
DUP 431080	0.1	Duplicate
431081	0.1	
431082	BDL	
431083	BDL	

Sample Number	Magnetite (%)

BDL: Below Detection Limit

ISS: Insufficient Sample (amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

Davis Tube Magnetite Analysis Report

MET-SOLVE LABORATORIES INC.

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 23-Nov-09
File Number: A718214

Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)
G1/P.1	1.1		430826	0.1		430847	BDL		430870	BDL
430802	0.1		DUP 430826	0.1	Duplicate	430848	0.1		430871	BDL
430803	0.2		430827	BDL		430849	BDL		430872	BDL
430804	0.1		430828	BDL		430850	BDL		430873	BDL
430805	BDL		430829	BDL		430851	BDL		430874	BDL
430806	BDL		430830	0.1		430852	BDL		G022531	1.6
430807	BDL		430831	BDL		430853	BDL		430876	BDL
430808	0.2		430832	BDL		430854	BDL		430877	BDL
430809	0.3		430832	BDL	Repeat	430855	BDL		430878	BDL
430810	0.1		430834	8.3	Standard	430856	0.1		430879	BDL
430811	BDL		430833	1.3		430857	BDL		430880	BDL
430812	BDL		G-1**/P.2	1.0		G022530	1.2		430881	BDL
430813	BDL		430834	BDL		430859	BDL		430882	BDL
430814	0.2		430835	BDL		430860	BDL		430883	BDL
430815	BDL		430836	BDL		430861	BDL		RRE 430883	BDL
430816	BDL		430837	0.1		430862	0.2		430884	BDL
430817	BDL		430838	0.1		430863	BDL		430885	0.1
430818	0.5	ISS (15 g)	G022529	1.9		DUP 430863	BDL	Duplicate	430886	BDL
430819	BDL		430840	0.1		430864	BDL		430887	BDL
430820	BDL		430841	BDL		430865	BDL		430888	BDL
430821	0.2		430842	0.1		G-1**/P.3	0.9		430889	BDL
430822	0.1		430843	BDL		430866	BDL		430890	BDL
430823	0.3		430844	BDL		430867	BDL		430891	BDL
430824	0.3		430845	BDL		430868	BDL		430892	0.1
430825	BDL		430846	BDL		430869	BDL		430893	0.1

BDL: Below Detection Limit

ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 23-Nov-09
File Number: A718214

Sample Number	Magnetite (%)	Note
430894	BDL	
430895	BDL	
G022532	0.5	
430897	BDL	
G-1**/P.4	0.9	
430898	BDL	
430899	BDL	
430900	BDL	
430901	BDL	
430902	BDL	
430903	BDL	
430904	BDL	
430905	BDL	
430906	BDL	
430907	BDL	
430908	BDL	
430909	BDL	
430910	BDL	
430911	BDL	
430912	BDL	
430913	BDL	
430914	BDL	
G022533	1.2	
430916	BDL	
430917	BDL	

Sample Number	Magnetite (%)	Note
DUP 430917	BDL	Duplicate
430918	BDL	
430919	0.1	
430920	BDL	
430921	BDL	
430922	BDL	
430923	BDL	
430924	BDL	
430925	BDL	
430926	BDL	
430926	BDL	Repeat
430928	8.4	Standard
430927	BDL	
430928	BDL	

Sample Number	Magnetite (%)	Note

Sample Number	Magnetite (%)

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:
Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 24-Nov-09
File Number: 9S0049RA

Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)
126501	BDL		126525	0.3		126549	10.4			
126502	BDL		126526	1.6		126550	10.5			
126503	BDL		126527	1.2		126551	9.4			
126504	BDL		126528	1.5		126552	8.7			
126505	BDL		126529	4.1		126553	12.2			
126506	BDL		126530	1.9		126554	10.8			
126507	BDL		126531	1.4		126555	11.3			
126508	BDL		126532	3.6		126556	10.6			
126509	BDL		126533	4.2						
126510	0.1		126534	1.9						
126511	BDL		126535	2.9						
126512	BDL		126536	4.7						
126513	BDL		126537	3.1						
126514	BDL		126538	3.6						
126515	BDL		126539	4.8						
126516	BDL		126540	11.7						
126517	BDL		126540-DP	11.9						
126518	BDL		126541	14.6						
126519	BDL		126542	11.5						
126520	BDL		126543	10.3						
126520-DP	BDL		126544	10.3						
126521	BDL		126545	9.0						
126522	BDL		126546	9.4						
126523	BDL		126547	BDL						
126524	BDL		126548	13.4						

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 1-Dec-09
File Number: 9S0050RA

Sample Number	Magnetite (%)	Note
126713	0.2	
126714	BDL	
126715	BDL	
126716	BDL	
126716-DP	BDL	Duplicate
126717	BDL	
126718	BDL	
126719	BDL	
126720	BDL	
126721	BDL	
126722	0.2	
126723	BDL	
126724	BDL	
126725	0.1	
126726	BDL	
126727	BDL	
126728	BDL	
126729	0.2	
126730	0.1	
126731	0.8	
126732	BDL	
126733	BDL	
126734	BDL	
126735	BDL	
126736	BDL	

Sample Number	Magnetite (%)	Note
126736-DP	BDL	Duplicate
126737	BDL	
126738	0.7	
126739	1.7	
126740	1.6	
126741	1.5	
126742	0.8	
126743	2.5	
126744	BDL	
126745	2.7	
126746	8.1	
126747	6.9	
126748	6.6	
126749	4.3	
126750	5.5	
126750	5.6	Repeat
Standard	8.1	Standard
126751	5.2	
126752	5.1	
126753	2.5	
126754	3.1	
126755	3.9	
126756	3.2	
126756-DP	3.2	Duplicate
126757	5.6	

Sample Number	Magnetite (%)	Note
126758	6.6	
126759	11.9	
126760	10.2	
126761	11.5	
126762	13.0	
126763	9.8	
126764	11.1	
126765	0.7	
126766	9.1	
126767	6.6	
126768	5.6	
126769	11.8	
126770	10.4	
126771	5.3	
126772	9.5	
126773	10.6	
126774	11.5	
126775	10.1	
126776	12.7	
126776-DP	12.7	Duplicate
126777	10.0	
126778	12.0	
126779	10.8	
126780	4.5	
126781	4.0	

Sample Number	Magnetite (%)
126782	13.3
126783	11.1
126784	9.8
126785	8.6
126786	9.1
126787	11.1
126788	13.5
126789	10.0
126790	12.5
126791	BDL
126792	12.8
126793	12.5
126794	10.8
126795	1.6
126796	12.3
126796-DP	12.5
126797	14.2
126798	13.0
126799	12.9

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 1-Dec-09
File Number: 9S0051RA

Sample Number	Magnetite (%)	Note
126563	2.8	
126564	5.0	
126565	5.2	
126566	10.2	
126567	4.6	
126568	5.6	
126569	7.8	
126570	5.1	
126571	5.5	
126572	4.8	
126573	4.4	
126574	5.0	
126575	3.1	
126576	5.5	
126577	4.5	
126578	0.0	
126579	4.7	
126579-DP	4.7	Duplicate
126580	4.8	
126581	1.7	
126582	7.4	
126583	5.0	
126584	8.0	
126585	6.1	
126586	3.4	

Sample Number	Magnetite (%)	Note
126587	3.3	
126588	11.0	
126589	9.2	
126590	5.0	
126591	4.1	
126592	5.4	
126593	3.9	
126594	6.9	
126595	3.9	
126596	5.0	
126597	5.9	
126598	5.3	
126599	2.7	
126599-DP	2.7	Duplicate
126600	3.9	
126601	9.7	
126602	5.1	
126603	5.1	
126604	8.4	
126605	6.6	
126606	5.5	
126607	10.8	
126608	15.0	
126608	15.0	Repeat
Standard	8.4	Standard

Sample Number	Magnetite (%)	Note
126609	16.5	
126610	10.7	
126611	1.9	
126612	9.6	
126613	11.2	
126614	11.2	
126615	11.5	
126616	8.8	
126617	4.4	
126618	6.8	

Sample Number	Magnetite (%)

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by: ____________________
Ishwinder Grewal, M.A.Sc. P.Er

Davis Tube Magnetite Analysis Report

MET-SOLVE LABORATORIES INC.

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 1-Dec-09
File Number: 9S0052RA

Sample Number	Magnetite (%)	Note
126801	BDL	
126801-DP	BDL	Duplicate
126802	BDL	
126803	BDL	
126804	BDL	
126805	BDL	
126806	0.3	
126807	BDL	
126808	0.9	
126809	0.3	
126810	0.9	
126811	1.3	
126812	0.4	
126813	0.6	
126814	0.4	
126815	1.3	
126816	BDL	
126817	5.5	
126818	6.6	
126819	6.3	
126820	7.8	
126821	8.7	
126821-DP	8.6	Duplicate
126822	0.9	
126823	8.6	

Sample Number	Magnetite (%)	Note
126824	9.0	
126825	7.7	
126826	8.8	
126827	9.2	
126828	9.9	
126829	9.7	
126830	8.0	
126831	8.0	
126832	11.7	
126833	13.0	
126834	11.7	
126835	11.4	
126836	12.7	
126837	10.7	
126838	9.6	
126839	9.5	
126840	4.2	
126841	8.1	
126841-DP	8.2	Duplicate
126842	10.4	
126843	10.1	
126931	1.5	
126932	3.6	
126933	3.1	
126934	2.3	

Sample Number	Magnetite (%)	Note
126935	4.7	
126936	4.8	
126937	8.9	
126938	7.0	
126939	5.9	
126940	9.9	
126941	7.7	
126942	8.7	
126943	8.3	
126944	7.2	
126945	6.8	
126946	9.7	
126947	4.6	
126948	5.2	
126948-DP	5.0	Duplicate
126949	8.8	
126950	9.1	
126951	10.6	
126952	7.9	
126953	8.0	
126954	10.5	
126955	9.9	
126956	8.5	
126957	7.7	
126958	8.8	

Sample Number	Magnetite (%)
126959	9.7
126960	13.5
127030	1.0
127031	BDL
127032	1.0
127033	5.6
127034	4.3
127035	2.5
127036	2.3
127037	1.1
127037-DP	1.4
127038	0.2
127039	1.7
127040	5.6
127041	4.2
127041	4.2
Standard	8.3
127042	4.9
127043	2.5
127044	3.2

BDL: Below Detection Limit

ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 1-Dec-09
File Number: 9S0053RA

Sample Number	Magnetite (%)	Note
126619	10.1	
126620	10.4	
126621	8.7	
126622	6.7	
126623	5.8	
126624	8.3	
126625	7.9	
126626	5.6	
126627	6.7	
126628	BDL	
126629	9.5	
126630	8.4	
126631	7.6	
126632	9.8	
126633	10.7	
126634	10.5	
126635	9.8	
126636	8.9	
126637	8.4	
126638	10.6	
126638-DP	10.8	Duplicate
126639	11.0	
126640	9.3	
126641	11.2	
126642	9.9	

Sample Number	Magnetite (%)	Note
126643	13.1	
126644	8.7	
126645	10.2	
126646	9.5	
126647	8.0	
126648	5.6	
126649	3.4	
126650	7.2	
126651	7.1	
126652	10.1	
126653	8.5	
126654	9.1	
126655	8.9	
126656	7.5	
126657	10.2	
126658	9.8	
126658-DP	10.6	Duplicate
126659	10.8	
126660	10.0	
126661	0.7	
126662	8.5	
126663	7.6	
126664	16.0	
126665	8.4	
126666	10.7	

Sample Number	Magnetite (%)	Note
126667	6.1	
126668	4.0	
126669	11.0	
126670	9.7	
126671	6.3	
126672	5.9	
126673	9.2	
126674	4.9	
126675	8.3	
126676	11.5	
126677	10.8	
126678	BDL	
126679	8.3	
126679-DP	8.1	Duplicate
126680	7.1	
126681	4.1	
126682	0.8	
126683	0.6	
126684	4.6	
126685	5.6	
126686	5.9	
126687	7.3	
126688	6.4	
126689	7.4	
126690	5.5	

Sample Number	Magnetite (%)
126691	6.1
126692	3.1
126693	4.3
126694	4.6
126695	4.6
126696	6.1
126697	4.5
126698	0.8
126699	3.2
126699-DP	3.3
126700	2.4
126701	8.0
126702	8.6
126703	8.5
126704	9.5

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 3-Dec-09
File Number: 9S0054RA

Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)
126844	12.7		126866	BDL		126890	12.9		126914	9.3
126845	12.5		126867	14.1		126891	2.0		126915	8.6
126846	9.7		126868	10.8		126892	8.0		126916	BDL
126847	10.4		126869	10.3		126893	9.3		126917	10.1
126848	4.8		126870	9.9		126894	6.9		126918	12.2
126849	5.6		126871	7.6		126895	16.0		126918-DP	12.6
126850	4.9		126872	9.2		126896	9.6		126919	12.2
126850	4.8	Repeat	126873	9.9		126897	7.6		126920	13.0
STANDARD	8.3	Standard	126874	7.7		126898	6.6		126921	12.1
126851	6.7		126875	9.8		126898-DP	6.7	Duplicate	126922	6.4
126852	2.2		126876	8.1		126899	7.5		126923	12.0
126853	0.6		126877	10.8		126900	14.0		126924	10.5
126854	5.6		126878	12.1		126901	12.7		126925	13.0
126855	8.8		126878-DP	12.2	Duplicate	126902	8.1		126926	11.4
126856	4.2		126879	11.8		126903	8.9		126927	8.1
126857	9.7		126880	13.0		126904	12.0		126928	10.5
126858	8.5		126881	12.2		126905	9.5		126929	12.4
126858-DP	8.4	Duplicate	126882	1.8		126906	11.0		126930	11.8
126859	8.4		126883	9.5		126907	11.9			
126860	10.1		126884	13.1		126908	10.7			
126861	10.1		126885	9.4		126909	5.5			
126862	9.5		126886	9.8		126910	0.7			
126863	10.5		126887	9.3		126911	2.1			
126864	11.1		126888	13.0		126912	8.3			
126865	11.3		126889	9.8		126913	9.2			

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:
Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 4-Dec-09
File Number: 9S0055RA
Page 1 of 1

Sample Number	Magnetite (%)	Note
126961	12.1	
126962	8.1	
126963	16.5	
126964	12.7	
126965	8.9	
126966	9.1	
126967	9.9	
126968	13.8	
126968-DP	12.9	Duplicate
126969	11.6	
126970	1.8	
126971	13.7	
126972	12.2	
126973	9.6	
126974	10.0	
126975	10.4	
126975	10.4	Repeat
Standard	8.3	Standard
126976	9.7	
126977	8.8	
126978	10.6	
126979	3.3	
126980	2.2	
126981	0.1	
126982	1.2	

Sample Number	Magnetite (%)	Note
126983	5.7	
126984	6.7	
126985	10.3	
126986	10.4	
126987	10.1	
126988	8.8	
126988-DP	9.8	Duplicate
126989	11.2	
126990	1.9	
126991	5.8	
126992	6.7	
126993	8.1	
126994	11.5	
126995	13.0	
126996	10.7	
126997	11.5	
126998	9.7	
126999	4.5	
127000	5.6	
127001	10.5	
127002	7.5	
127003	15.5	
127004	9.7	
127005	14.7	
127006	1.6	

Sample Number	Magnetite (%)	Note
127007	10.1	
127008	8.4	
127008-DP	9.2	Duplicate
127009	10.3	
127010	8.6	
127011	11.0	
127012	8.1	
127013	6.8	
127014	10.8	
127015	12.7	
127016	7.7	
127017	12.6	
127018	0.7	
127019	BDL	
127020	9.5	
127021	8.8	
127022	10.0	
127023	9.1	
127024	1.4	
127025	1.1	
127026	0.8	
127027	10.1	
127028	11.7	
127028-DP	12.1	Duplicate
127029	13.3	

Sample Number	Magnetite (%)
127220	10.9
127221	15.4
127222	13.6
127223	11.1
127224	12.1
127225	10.5
127226	0.9
127227	15.7
127228	10.9
127229	11.4

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

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MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 4-Dec-09
File Number: 9S0056RA

Sample Number	Magnetite (%)	Note
127045	7.3	
127046	0.3	
127047	3.1	
127048	3.2	
127049	BDL	
127050	5.6	
127051	7.0	
127052	7.7	
127053	3.8	
127053-DP	4.0	Duplicate
127054	4.8	
127055	0.2	
127056	0.1	
127057	3.0	
127058	10.3	
127059	5.8	
127060	5.8	
127061	10.3	
127062	17.9	
127063	11.1	
127064	7.3	
127065	5.9	
127066	7.8	
127067	6.8	
127068	4.0	

Sample Number	Magnetite (%)	Note
127069	8.0	
127070	9.2	
127071	10.8	
127072	2.0	
127073	10.2	
127073-DP	11.5	Duplicate
127074	7.8	
127075	8.9	
127075	8.8	Repeat
Standard	8.6	Standard
127076	9.2	
127077	10.9	
127078	7.8	
127079	2.4	
127080	2.5	
127081	0.9	
127082	5.1	
127083	3.8	
127084	7.0	
127085	8.8	
127086	8.9	
127087	2.8	
127088	11.1	
127089	BDL	
127090	10.9	

Sample Number	Magnetite (%)	Note
127091	9.1	
127092	8.5	
127093	8.1	
127093-DP	8.9	Duplicate
127094	9.5	
127095	7.5	
127096	3.4	
127097	5.0	
127098	9.8	
127099	4.6	
127101	11.9	
127102	4.0	
127103	9.5	
127104	8.9	
127105	7.5	
127106	6.1	
127107	9.3	
127108	3.8	
127109	5.6	
127110	5.8	
127111	7.0	
127112	1.9	
127113	2.5	
127114	6.5	
127114-DP	6.6	Duplicate

Sample Number	Magnetite (%)
127115	8.4
127116	5.8
127117	5.5
127118	10.8
127119	11.9
127120	12.8
127121	11.8
127122	11.8
127123	12.5

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Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 6-Dec-09
File Number: 9S0058RA

Sample Number	Magnetite (%)	Note
127240	0.6	
127241	0.2	
127242	2.7	
127243	2.2	
127244	3.3	
127245	5.5	
127246	1.6	
127247	1.4	
127248	2.0	
127249	5.8	
127250	BDL	
127251	9.0	
127251-DP	8.2	Duplicate
127252	3.7	
127253	9.6	
127254	6.4	
127255	5.5	
127256	1.7	
127257	8.4	
127258	11.0	
127259	13.2	
127260	10.3	
127261	12.3	
127262	12.4	
127263	8.2	

Sample Number	Magnetite (%)	Note
127264	7.8	
127265	5.6	
127266	4.2	
127267	0.9	
127268	1.9	
127269	5.3	
127270	5.6	
127270-DP	5.6	Duplicate
127271	5.6	
127272	7.0	
127273	3.1	
127274	2.8	
127275	8.4	
127276	2.8	
127277	3.3	
127278	2.8	
127279	4.3	
127280	6.4	
127281	0.5	
127282	8.5	
127283	8.0	
127284	6.7	
127285	5.2	
127286	7.0	
127287	6.6	

Sample Number	Magnetite (%)	Note
127288	5.8	
127288	5.7	Duplicate
Standard	8.1	Standard
127289	11.5	
127290	BDL	
127291	11.1	
127291-DP	11.4	Duplicate
127292	7.9	
127293	7.5	
127294	6.9	
127295	10.6	
127296	9.8	
127297	10.8	
127298	5.7	
127299	10.4	
127300	7.9	
127301	6.7	
127302	8.9	
127303	11.8	
127304	6.7	
127305	10.6	
127306	9.7	
127307	3.0	
127308	4.4	
127309	9.0	

Sample Number	Magnetite (%)
127310	10.2
127311	9.1
127311-DP	9.6
127312	10.5
127313	9.4
127314	11.4
127315	2.1
127316	10.7
127317	11.2
127318	7.0
127319	11.7
127320	11.4
127321	7.3
127322	6.9
127323	7.8
127324	6.7
127325	7.5
127326	9.4
127327	8.2
127328	4.7
127329	4.8
127330	BDL
127331	6.0
127331-DP	6.3
127332	7.9

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MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 6-Dec-09
File Number: 9S0058RA

Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)
127333	5.9									
127334	4.5									
127335	5.3									
127336	3.1									
127337	11.0									
127338	0.8									
127339	10.2									

BDL: Below Detection Limit
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Approved by: ____________________
Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 9-Dec-09
File Number: 9S0059RA

Sample Number	Magnetite (%)	Note
127351	BDL	
127352	BDL	
127353	0.2	
127354	0.2	
127355	BDL	
127356	0.2	
127357	BDL	
127358	0.2	
127359	0.9	
127360	0.3	
127361	0.6	
127362	BDL	
127362-DP	BDL	Duplicate
127363	0.5	
127364	1.1	
127365	1.3	
127366	4.7	
127367	3.0	
127368	2.8	
127369	5.2	
127370	3.8	
127371	2.7	
127372	5.3	
127373	3.4	
127374	7.8	

Sample Number	Magnetite (%)	Note
127375	7.5	
127376	BDL	
127377	8.8	
127378	2.6	
127379	7.3	
127380	10.7	
127381	9.8	
127382	14.6	
127382-DP	14.7	Duplicate
127383	12.3	
127384	0.5	
127385	10.3	
127386	10.4	
127387	11.6	
127388	10.0	
127389	12.3	
127390	7.2	
127391	8.8	
127392	4.1	
127393	7.2	
127394	9.4	
127394	9.1	
Standard	8.3	
127395	8.1	
127396	7.2	

Sample Number	Magnetite (%)	Note
127397	3.5	
127398	7.2	
127399	8.3	
127400	7.3	
127401	7.5	
127402	9.8	
127402-DP	9.9	Duplicate
127403	9.1	
127404	11.7	
127405	10.9	
127406	9.6	
127407	10.8	
127408	11.7	
127409	10.9	
127410	10.9	
127411	12.8	
127412	4.2	
127413	7.2	
127414	2.1	
127415	10.8	
127416	BDL	
127417	14.7	
127418	12.2	
127419	14.5	
127420	9.3	

Sample Number	Magnetite (%)
127421	12.8
127422	11.4
127422-DP	11.9
127423	14.5
127424	10.0
127425	16.0
127426	10.9
127427	8.9
127428	7.8
127429	11.0
127430	4.4
127431	8.0
127432	6.0
127433	6.2
127434	6.3
127435	7.3
127436	8.8

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Davis Tube Magnetite Analysis Report

MET-SOLVE LABORATORIES INC.

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: 9S0060RA

Sample Number	Magnetite (%)	Note
127451	BDL	
127452	0.7	
127453	BDL	
127454	BDL	
127455	BDL	
127456	BDL	
127456-DP	BDL	Duplicate
127457	BDL	
127458	BDL	
127459	BDL	
127460	BDL	
127461	BDL	
127462	0.1	
127463	BDL	
127464	BDL	
127465	BDL	
127466	BDL	
127467	BDL	
127468	BDL	
127469	0.1	
127470	BDL	
127471	0.1	
127472	BDL	
127473	BDL	
127474	BDL	

Sample Number	Magnetite (%)	Note
127475	BDL	
127476	BDL	
127476-DP	BDL	Duplicate
127477	BDL	
127478	BDL	
127479	BDL	
127480	1.6	
127481	BDL	
127482	BDL	
127483	BDL	
127484	BDL	
127485	0.1	
127486	BDL	
127487	BDL	
127488	BDL	
127489	BDL	
127490	BDL	
127491	0.2	
127492	BDL	
127493	0.1	
127494	0.2	
127495	0.2	
127496	0.2	
127496-DP	BDL	Duplicate
127497	0.1	

Sample Number	Magnetite (%)	Note
127498	BDL	
127499	BDL	
127500	BDL	
127501	BDL	
127502	BDL	
127503	BDL	
127503	BDL	Repeat
Standard	8.4	Standard
127504	BDL	
127505	1.8	
127506	0.1	
127507	0.2	
127508	BDL	
127509	BDL	

Sample Number	Magnetite (%)

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MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: 9S0061RA

Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)
127910	0.4		127935	2.4		127959	BDL			
127911	BDL		127936	3.1		127960	BDL			
127912	BDL		127937	0.5		127961	BDL			
127913	0.3		127938	0.2		127962	BDL			
127914	BDL		127939	1.3		127963	BDL			
127915	BDL		127940	0.5		127964	BDL			
127916	0.1		127941	BDL		127965	BDL			
127917	BDL		127942	0.1		127966	BDL			
127918	0.1		127943	0.6		127967	BDL			
127919	BDL		127944	0.1		127968	0.2			
127920	0.1		127945	2.7		127969	0.2			
127921	BDL		127945-DP	2.7	Duplicate	127970	BDL			
127922	BDL		127946	0.5		127971	0.1			
127923	BDL		127947	2.3		127972	0.1			
127924	BDL		127948	0.1		127973	1.7			
127925	BDL		127949	BDL		127974	BDL			
127926	BDL		127950	0.2		127975	0.2			
127927	BDL		127951	BDL		127976	0.1			
127928	BDL		127952	0.2		127977	BDL			
127929	BDL		127953	BDL		127978	BDL			
127930	BDL		127954	BDL		127979	BDL			
127931	BDL		127955	BDL		127980	BDL			
127932	BDL		127956	BDL		127981	BDL			
127933	0.1		127957	0.1		127982	0.2			
127934	0.2		127958	BDL		127983	BDL			

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MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: 9S0062RA

Sample Number	Magnetite (%)	Note
127124	11.6	
127125	12.7	
127125-DP	13.5	Duplicate
127126	8.5	
127127	10.4	
127128	BDL	
127129	13.0	
127130	12.9	
127131	12.4	
127132	12.3	
127133	8.9	
127134	0.3	
127135	10.2	
127136	1.1	
127137	BDL	
127138	2.4	
127139	11.3	
127140	8.0	
127141	8.0	
127141	7.9	Repeat
Standard	8.3	Standard
127142	9.5	
127143	6.3	
127144	11.3	
127145	13.0	

Sample Number	Magnetite (%)	Note
127146	12.9	
127147	6.1	
127148	12.4	
127149	13.2	
127150	10.9	
127151	11.7	
127152	8.6	
127153	4.6	
127154	2.8	
127155	10.3	
127156	1.7	
127157	7.8	
127158	10.3	
127159	12.1	
127160	6.1	
127161	11.0	
127162	7.3	
127163	14.7	
127164	12.7	
127165	13.3	
127165-DP	11.3	Duplicate
127166	10.9	
127167	13.5	
127168	13.2	
127169	8.8	

Sample Number	Magnetite (%)	Note
127170	5.6	
127171	7.8	
127172	1.3	
127173	5.8	
127174	13.5	
127175	6.1	
127176	5.3	
127177	5.9	
127178	BDL	
127520	BDL	
127521	2.0	
127522	BDL	
127523	BDL	
127524	BDL	
127525	BDL	
127526	BDL	
127527	BDL	
127528	0.1	
127529	BDL	
127530	BDL	
127531	BDL	
127532	BDL	
127533	BDL	
127534	0.2	
127535	BDL	

Sample Number	Magnetite (%)
127536	BDL
127537	BDL
127538	BDL
127539	BDL
127540	BDL
127541	BDL
127542	BDL
127543	BDL
127544	BDL
127545	BDL
127546	0.7
127547	BDL
127547-DP	BDL
127548	BDL
127549	BDL
127550	BDL
127551	BDL
127552	0.2
127553	BDL
127554	BDL
127555	BDL
127556	BDL
127557	BDL
127558	BDL
127559	BDL

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MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: 9S0062RA

Sample Number	Magnetite (%)	Note
127560	0.1	
127561	BDL	
127562	BDL	
127563	0.2	
127564	BDL	
127565	0.1	
127566	BDL	
127567	0.1	
127568	0.9	
127569	BDL	
127570	0.1	
127571	BDL	
127572	BDL	
127573	BDL	
127574	BDL	

Sample Number	Magnetite (%)	Note

Sample Number	Magnetite (%)	Note

Sample Number	Magnetite (%)

BDL: Below Detection Limit
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Davis Tube Magnetite Analysis Report

MET-SOLVE LABORATORIES INC.

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: 9S0063RA

Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)
127581	BDL		127603	BDL		127803	BDL		127827	BDL
127582	0.1		127604	BDL		127804	BDL		127828	BDL
127582	BDL	Repeat	127605	BDL		127805	0.1		127829	0.5
Standard	8.3	Standard	127606	BDL		127806	BDL		127830	0.1
127583	BDL		127607	BDL		127807	BDL		127831	BDL
127584	BDL		127608	BDL		127808	BDL		127832	BDL
127585	BDL		127609	BDL		127808-DP	BDL	Duplicate	127833	BDL
127586	0.1		127610	BDL		127809	0.4		127834	BDL
127587	0.1		127611	BDL		127810	1.0		127835	0.5
127588	BDL		127612	BDL		127811	BDL		127836	0.3
127589	BDL		127613	BDL		127812	BDL		127837	0.4
127590	BDL		127614	BDL		127813	BDL		127838	0.8
127591	1.8		127615	BDL		127814	BDL		127839	0.7
127592	BDL		127616	BDL		127815	0.1		127840	1.2
127593	BDL		127617	BDL		127816	0.2		127841	0.1
127593-DP	0.1	Duplicate	127618	BDL		127817	BDL		127842	0.4
127594	BDL		127619	BDL		127818	1.4		127843	1.5
127595	BDL		127620	BDL		127819	1.4		127844	2.3
127596	BDL		127621	BDL		127820	BDL		127845	2.4
127597	BDL		127622	0.7		127821	1.8		127846	2.5
127598	BDL		127623	5.0		127822	BDL		127847	3.2
127599	BDL		127624	3.8		127823	0.2		127848	3.5
127600	BDL		127625	5.5		127824	BDL		127848-DP	3.2
127601	BDL		127801	BDL		127825	0.7		127849	2.8
127602	BDL		127802	BDL		127826	0.7		127850	3.9

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MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: 9S0063RA

Sample Number	Magnetite (%)	Note
127851	3.6	
127852	5.2	
127853	3.3	
127854	BDL	
127854	0.1	Repeat
Standard	8.3	Standard
127855	3.4	
127856	4.4	
127857	5.3	
127858	4.4	
127859	2.0	
127860	3.5	
127861	1.0	
127862	2.0	
127863	2.8	
127864	4.2	
127865	2.3	
127866	3.5	
127867	4.9	
127868	3.7	
127869	2.5	
127870	3.5	
127871	2.3	
127872	2.6	
127873	4.7	

Sample Number	Magnetite (%)	Note
127874	4.6	
127875	5.5	
127876	5.6	
127877	2.3	
127878	3.0	
127879	3.9	
127880	4.5	
127881	3.2	
127882	1.6	
127883	2.0	
127884	2.3	
127885	2.7	
127886	2.3	
127887	4.7	
127888	3.8	
127888-DP	3.3	Duplicate
127889	0.8	
127890	8.1	
127891	6.8	
127892	0.8	
127893	0.5	
127894	BDL	
127895	1.2	
127896	0.8	
127897	1.1	

Sample Number	Magnetite (%)	Note
127898	1.1	
127899	1.2	
127900	0.8	
127901	0.7	

Sample Number	Magnetite (%)

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:
Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: **9S0065RA**

Sample Number	Magnetite (%)	Note
127630	BDL	
127631	BDL	
127632	BDL	
127633	0.1	
127634	BDL	
127635	BDL	
127636	BDL	
127637	BDL	
127638	BDL	
127639	BDL	
127640	BDL	
127640-DP	BDL	Duplicate
127641	0.8	
127642	1.8	
127643	0.3	
127644	BDL	
127645	BDL	
127646	BDL	
127647	BDL	
127648	BDL	
127649	BDL	
127650	BDL	
127651	BDL	
127652	BDL	
127653	BDL	

Sample Number	Magnetite (%)	Note
127654	BDL	
127655	BDL	
127656	BDL	
127657	3.6	
127658	0.2	
127659	BDL	
127660	BDL	
127661	BDL	
127662	0.1	
127663	BDL	
127664	BDL	
127665	0.6	
127666	0.5	
127667	0.3	
127668	1.3	
127669	2.2	
127670	1.0	
127671	1.1	
127672	0.2	
127673	0.5	
127674	BDL	
127675	0.4	
127676	1.3	
127677	4.0	
127678	2.6	

Sample Number	Magnetite (%)	Note
127679	2.8	
127680	2.0	
127680	1.9	Repeat
Standard	8.3	Standard
127680-DP	2.0	Duplicate
127681	1.1	
127682	1.4	
127683	1.7	
127684	2.7	
127685	2.7	
127686	5.1	
127687	6.8	
127688	2.3	
127689	5.0	
127690	5.8	
127691	5.3	
127692	2.2	
127693	1.8	
127694	1.7	
127695	BDL	
127696	0.3	
127697	4.0	
127698	3.2	
127699	6.4	
127700	9.7	

Sample Number	Magnetite (%)
127701	16.3
127702	1.4
127703	14.7
127704	12.1
127705	11.7
127706	8.8
127707	9.4
127708	7.5
127709	8.3
127710	5.8
127711	4.2
127712	2.3
127713	5.8
127714	BDL
127715	9.0
127716	8.8
127717	10.7
127718	5.5
127719	5.6
127720	8.6
127720-DP	8.6
127721	9.7
127722	8.8
127723	8.3
127724	6.1

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Approved by:
Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: **9S0065RA**

Sample Number	Magnetite (%)	Note
127725	8.1	
127726	5.6	
127727	6.3	
127728	5.6	
127729	6.0	
127730	3.6	
127731	7.7	
127732	1.0	
127733	6.1	
127734	5.8	
127735	8.1	
127736	7.5	
127737	9.6	
127738	4.6	
127739	1.7	
127740	6.4	
127741	6.4	
127742	4.4	
127743	4.5	
127744	4.1	
127745	2.8	
127746	6.1	
127747	7.4	
127748	4.4	
127749	5.2	

Sample Number	Magnetite (%)	Note
127750	4.7	
127751	2.7	
127752	2.1	
127753	5.9	
127754	BDL	
127755	2.6	
127756	4.7	
127757	4.7	
127758	4.3	
127759	3.0	
127760	4.3	
127760-DP	4.2	Duplicate
127761	3.0	
127762	0.2	
127763	4.2	
127764	4.2	
127765	4.1	
127766	1.7	
127767	2.6	
127768	0.3	
127769	0.1	
127770	2.4	
127771	BDL	
127772	4.6	
127773	3.4	

Sample Number	Magnetite (%)	Note
127774	3.4	
127775	2.7	
127776	0.8	
127777	0.2	
127777	0.2	Repeat
Standard	8.3	Standard
127778	5.3	
127779	4.5	
127780	2.7	
127781	4.1	

Sample Number	Magnetite (%)

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:
Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: A608403

Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)
430101	8.3									
430102	7.5									
430103	5.5									
430104	7.0									
430105	5.9									
430106	7.1									
430107	7.8									
430108	11.3									
430109	7.2									

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: A607570

Sample Number	Magnetite (%)	Note
430011	2.9	
430012	3.8	
430013	2.5	
430014	6.2	
430015	4.0	
430016	8.6	
430018	8.8	
430019	10.0	
430021	8.5	
430022	5.6	
430023	3.5	
430024	7.2	
430025	2.0	
430026	8.2	
430027	9.2	
430028	1.1	ISS (2.63g)
430029	8.0	
430030	9.1	
430031	9.1	
430032	3.3	
430034	4.8	
430035	5.9	
430037	5.7	
430038	3.9	
430039	5.5	
430040	3.8	
430041	3.8	
430042	6.0	
430043	4.0	
430044	5.5	
430045	6.6	
430046	8.0	
430047	7.3	
430048	1.7	

BDL: Below Detection Limit

ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:

Ishwinder Grewal, M.A.Sc. P.Er

MET-SOLVE LABORATORIES INC.

Davis Tube Magnetite Analysis Report

Project Name: Skyline Gold Corp.
Project Number: MS1203

Date: 22-Dec-09
File Number: A718161

Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)	Note	Sample Number	Magnetite (%)
430277	BDL		430303	0.1		430329	BDL		430354	BDL
430278	BDL		430304	0.1		430330	BDL		430355	BDL
430279	BDL		430305	BDL		430332	BDL		430356	BDL
430280	BDL		430306	BDL		430332	BDL	Repeat	430357	BDL
430281	BDL		430307	BDL		Standard	7.9	Standard	430358	BDL
430282	BDL		430308	BDL		430333	BDL		430359	BDL
430283	0.3		430310	BDL		430334	BDL		430360	BDL
430284	BDL		430311	BDL		430335	BDL		430361	BDL
430285	BDL		430312	BDL		430336	BDL		430362	BDL
430286	BDL		430313	BDL		430337	0.1			
430287	BDL		430314	BDL		430338	0.2			
430288	BDL		430315	BDL		430339	0.1			
430289	BDL		430316	BDL		430340	3.7			
430291	BDL		430317	BDL		430341	BDL			
430292	BDL		430318	BDL		430342	BDL			
430293	BDL		430319	BDL	ISS (3.49g)	430343	BDL			
430294	BDL		430320	0.2		430344	BDL			
430295	BDL		430321	BDL		430345	BDL			
430296	BDL		430322	BDL		430346	BDL			
430297	BDL		430323	BDL		430347	BDL			
430298	BDL		430324	BDL		430349	BDL			
430299	BDL		430325	BDL		430350	BDL			
430300	BDL		430326	0.1		430351	BDL			
430301	BDL		430327	BDL		430352	BDL			
430302	0.1		430328	BDL		430353	BDL			

BDL: Below Detection Limit
ISS: Insufficient Sample (where possible, amount of sample available shown in brackets)

Approved by:
Ishwinder Grewal, M.A.Sc. P.Er

3.3

Hole	Sample ID	Depth From (m)	Depth To (m)	Interval (m)	Magnetite Analysis %	Numerical Magnetite Analysis %
1211	126501	5.2	8.5	3.3	BDL	0.05
1211	126502	8.5	11.6	3.1	BDL	0.05
1211	126503	11.6	14.6	3.0	BDL	0.05
1211	126504	14.6	17.7	3.1	BDL	0.05
1211	126505	17.7	20.7	3.0	BDL	0.05
1211	126506	20.7	23.8	3.1	BDL	0.05
1211	126507	23.8	26.8	3.0	BDL	0.05
1211	126508	26.8	29.9	3.1	BDL	0.05
1211	126509	29.9	32.9	3.0	BDL	0.05
1211	126510	32.9	35.9	3.0	0.1	0.10
1211	126511	35.9	39.0	3.0	BDL	0.05
1211	126512	39.0	42.1	3.1	BDL	0.05
1211	126513	42.1	45.1	3.0	BDL	0.05
1211	126514	45.1	48.1	3.0	BDL	0.05
1211	126515	48.1	51.2	3.0	BDL	0.05
1211	126516	51.2	54.2	3.0	BDL	0.05
1211	126517	54.2	57.3	3.0	BDL	0.05
1211	126518	57.3	60.3	3.0	BDL	0.05
1211	126519	60.3	63.4	3.0	BDL	0.05
1211	126520	63.4	66.4	3.0	BDL	0.05
1211	126521	66.4	69.5	3.0	BDL	0.05
1211	126522	69.5	72.5	3.0	BDL	0.05
1211	126523	72.5	75.6	3.0	BDL	0.05
1211	126524	75.6	78.6	3.0	BDL	0.05
1211	126525	78.6	81.7	3.0	0.3	0.30
1211	126526	81.7	84.7	3.0	1.65	1.65
1211	126527	84.7	87.7	3.0	1.15	1.15
1211	126528	87.7	90.8	3.0	1.5	1.50
1211	126529	90.8	93.8	3.0	4.05	4.05
1211	126531	93.8	96.8	3.0	1.4	1.40
1211	126532	96.8	99.9	3.0	3.6	3.60
1211	126533	99.9	102.9	3.0	4.25	4.25
1211	126534	102.9	106.0	3.0	1.85	1.85
1211	126535	106.0	109.0	3.0	2.9	2.90
1211	126536	109.0	112.1	3.0	4.7	4.70
1211	126537	112.1	115.1	3.0	3.05	3.05
1211	126538	115.1	118.2	3.0	3.6	3.60
1211	126539	118.2	121.2	3.0	4.8	4.80
1211	126540	121.2	124.2	3.0	11.7	11.70
1211	126541	124.2	127.3	3.0	14.55	14.55
1211	126542	127.3	130.3	3.0	11.45	11.45
1211	126543	130.3	133.4	3.0	10.3	10.30

1211	126544	133.4	136.4	3.0	10.25	10.25
1211	126545	136.4	139.5	3.0	9	9.00
1211	126546	139.5	142.6	3.1	9.4	9.40
1211	126548	142.6	145.6	3.0	13.4	13.40
1211	126549	145.6	148.7	3.0	10.35	10.35
1211	126550	148.7	151.7	3.0	10.55	10.55
1211	126551	151.7	154.8	3.0	9.35	9.35
1211	126552	154.8	157.8	3.0	8.7	8.70
1211	126553	157.8	160.9	3.0	12.15	12.15
1211	126555	160.9	163.9	3.0	11.3	11.30
1211	126556	163.9	165.5	1.6	10.6	10.60
1212	127581	13.1	14.6	1.5	BDL	0.05
1212	127582	14.6	17.6	3.0	0.1	0.10
1212	127583	17.6	20.7	3.0	BDL	0.05
1212	127584	20.7	23.7	3.0	BDL	0.05
1212	127585	23.7	26.8	3.0	BDL	0.05
1212	127586	26.8	29.8	3.0	0.1	0.10
1212	127587	29.8	32.9	3.0	0.1	0.10
1212	127588	32.9	35.9	3.0	BDL	0.05
1212	127589	35.9	39.0	3.0	BDL	0.05
1212	127590	39.0	42.0	3.0	BDL	0.05
1212	127592	42.0	45.1	3.0	BDL	0.05
1212	127593	45.1	48.1	3.0	BDL	0.05
1212	127594	48.1	51.2	3.0	BDL	0.05
1212	127595	51.2	54.2	3.0	BDL	0.05
1212	127596	54.2	57.3	3.0	BDL	0.05
1212	127597	57.3	60.3	3.0	BDL	0.05
1212	127598	60.3	63.4	3.0	BDL	0.05
1212	127599	63.4	66.4	3.0	BDL	0.05
1212	127600	66.4	69.5	3.0	BDL	0.05
1212	127601	69.5	72.5	3.0	BDL	0.05
1212	127603	72.5	75.6	3.0	BDL	0.05
1212	127604	75.6	78.6	3.0	BDL	0.05
1212	127605	78.6	81.7	3.0	BDL	0.05
1212	127606	81.7	84.7	3.0	BDL	0.05
1212	127607	84.7	87.8	3.0	BDL	0.05
1212	127608	87.8	90.8	3.0	BDL	0.05
1212	127609	90.8	93.8	3.0	BDL	0.05
1212	127610	93.8	96.9	3.0	BDL	0.05
1212	127611	96.9	99.9	3.0	BDL	0.05
1212	127612	99.9	103.0	3.0	BDL	0.05
1212	127614	103.0	106.0	3.0	BDL	0.05
1212	127615	106.0	109.1	3.0	BDL	0.05
1212	127616	109.1	112.1	3.0	BDL	0.05
1212	127617	112.1	115.2	3.0	BDL	0.05
1212	127618	115.2	118.2	3.0	BDL	0.05

1212	127619	118.2	121.3	3.0	BDL	0.05
1212	127620	121.3	124.3	3.0	BDL	0.05
1212	127621	124.3	127.4	3.0	BDL	0.05
1212	127623	127.4	130.4	3.0	5.05	5.05
1212	127624	130.4	133.5	3.0	3.8	3.80
1212	127625	133.5	135.3	1.8	5.45	5.45
1216	126713	9.0	12.2	3.2	0.2	0.20
1216	126714	12.2	15.2	3.0	BDL	0.05
1216	126715	15.2	18.3	3.0	BDL	0.05
1216	126716	18.3	21.3	3.0	BDL	0.05
1216	126717	21.3	24.4	3.0	BDL	0.05
1216	126718	24.4	27.4	3.0	BDL	0.05
1216	126719	27.4	30.5	3.0	BDL	0.05
1216	126720	30.5	33.5	3.0	BDL	0.05
1216	126721	33.5	36.6	3.0	BDL	0.05
1216	126722	36.6	39.6	3.0	0.2	0.20
1216	126723	39.6	42.7	3.0	BDL	0.05
1216	126724	42.7	45.7	3.0	BDL	0.05
1216	126725	45.7	48.8	3.0	0.1	0.10
1216	126726	48.8	51.8	3.0	BDL	0.05
1216	126727	51.8	54.9	3.0	BDL	0.05
1216	126728	54.9	57.9	3.0	BDL	0.05
1216	126729	57.9	61.0	3.0	0.15	0.15
1216	126730	61.0	64.0	3.0	0.1	0.10
1216	126732	64.0	67.1	3.0	BDL	0.05
1216	126733	67.1	70.1	3.0	BDL	0.05
1216	126734	70.1	73.2	3.0	BDL	0.05
1216	126735	73.2	76.2	3.0	BDL	0.05
1216	126736	76.2	79.3	3.0	BDL	0.05
1216	126737	79.3	82.3	3.0	BDL	0.05
1216	126738	82.3	85.4	3.0	0.75	0.75
1216	126739	85.4	88.4	3.0	1.65	1.65
1216	126740	88.4	91.4	3.0	1.6	1.60
1216	126741	91.4	94.5	3.0	1.45	1.45
1216	126742	94.5	97.2	2.7	0.85	0.85
1216	126743	97.2	100.2	3.0	2.45	2.45
1216	126745	100.2	103.3	3.0	2.7	2.70
1216	126746	103.3	106.4	3.1	8.15	8.15
1216	126747	106.4	109.7	3.3	6.9	6.90
1216	126748	109.7	112.7	3.0	6.65	6.65
1216	126749	112.7	115.8	3.0	4.25	4.25
1216	126750	115.8	118.8	3.0	5.5	5.50
1216	126751	118.8	121.9	3.0	5.25	5.25
1216	126752	121.9	124.9	3.0	5.1	5.10
1216	126753	124.9	128.0	3.0	2.55	2.55
1216	126754	128.0	131.0	3.0	3.15	3.15

1216	126755	131.0	134.1	3.0	3.95	3.95
1216	126756	134.1	137.1	3.0	3.15	3.15
1216	126757	137.1	140.2	3.0	5.6	5.60
1216	126758	140.2	143.2	3.0	6.6	6.60
1216	126759	143.2	146.3	3.0	11.85	11.85
1216	126760	146.3	149.3	3.0	10.25	10.25
1216	126761	149.3	152.4	3.0	11.45	11.45
1216	126763	152.4	155.4	3.0	9.75	9.75
1216	126764	155.4	158.5	3.0	11.1	11.10
1216	126766	158.5	161.5	3.0	9.15	9.15
1216	126767	161.5	164.6	3.0	6.65	6.65
1216	126768	164.6	167.6	3.0	5.65	5.65
1216	126769	167.6	170.7	3.0	11.85	11.85
1216	126770	170.7	173.7	3.0	10.35	10.35
1216	126771	173.7	176.8	3.0	5.3	5.30
1216	126772	176.8	179.8	3.0	9.55	9.55
1216	126773	179.8	182.9	3.0	10.6	10.60
1216	126774	182.9	185.9	3.0	11.5	11.50
1216	126775	185.9	188.9	3.0	10.05	10.05
1216	126776	188.9	192.0	3.0	12.65	12.65
1216	126777	192.0	195.0	3.0	10	10.00
1216	126778	195.0	198.1	3.0	12	12.00
1216	126779	198.1	201.1	3.0	10.8	10.80
1216	126780	201.1	204.2	3.0	4.55	4.55
1216	126781	204.2	207.2	3.0	4.05	4.05
1216	126782	207.2	210.3	3.0	13.3	13.30
1216	126783	210.3	213.3	3.0	11.1	11.10
1216	126784	213.3	216.4	3.0	9.75	9.75
1216	126785	216.4	219.4	3.0	8.65	8.65
1216	126786	219.4	222.5	3.0	9.05	9.05
1216	126787	222.5	225.5	3.0	11.05	11.05
1216	126788	225.5	228.6	3.0	13.5	13.50
1216	126789	228.6	231.6	3.0	9.95	9.95
1216	126790	231.6	234.7	3.0	12.5	12.50
1216	126790	234.7	237.7	3.0	12.5	12.50
1216	126792	237.7	240.8	3.0	12.8	12.80
1216	126793	240.8	243.8	3.0	12.5	12.50
1216	126794	243.8	246.9	3.0	10.85	10.85
1216	126796	246.9	249.9	3.0	12.3	12.30
1216	126797	249.9	253.0	3.0	14.15	14.15
1216	126798	253.0	256.0	3.0	13	13.00
1216	126799	256.0	256.7	0.7	12.85	12.85
1217	126801	60.0	63.0	3.0	BDL	0.05
1217	126802	63.0	66.1	3.1	BDL	0.05
1217	126803	66.1	69.1	3.0	BDL	0.05
1217	126804	69.1	72.2	3.0	BDL	0.05

1217	126805	72.2	75.2	3.0	BDL	0.05
1217	126806	75.2	78.3	3.0	0.25	0.25
1217	126807	78.3	81.3	3.0	BDL	0.05
1217	126808	81.3	84.4	3.0	0.9	0.90
1217	126809	84.4	87.4	3.0	0.25	0.25
1217	126810	87.4	90.5	3.0	0.9	0.90
1217	126811	90.5	93.5	3.0	1.3	1.30
1217	126812	93.5	96.6	3.0	0.4	0.40
1217	126813	96.6	99.6	3.0	0.55	0.55
1217	126814	99.6	102.7	3.0	0.4	0.40
1217	126815	102.7	105.7	3.0	1.3	1.30
1217	126817	105.7	108.7	3.0	5.5	5.50
1217	126818	108.7	111.8	3.0	6.55	6.55
1217	126819	111.8	114.8	3.0	6.25	6.25
1217	126820	114.8	117.9	3.0	7.75	7.75
1217	126821	117.9	120.9	3.0	8.65	8.65
1217	126823	120.9	123.9	3.0	8.6	8.60
1217	126824	123.9	127.0	3.0	9	9.00
1217	126825	127.0	130.0	3.0	7.7	7.70
1217	126826	130.0	133.1	3.0	8.75	8.75
1217	126827	133.1	136.1	3.0	9.15	9.15
1217	126828	136.1	139.2	3.0	9.95	9.95
1217	126829	139.2	142.2	3.0	9.65	9.65
1217	126830	142.2	145.3	3.0	8	8.00
1217	126832	145.3	148.3	3.0	11.7	11.70
1217	126833	148.3	151.4	3.0	12.95	12.95
1217	126834	151.4	154.4	3.0	11.7	11.70
1217	126835	154.4	157.5	3.0	11.4	11.40
1217	126836	157.5	160.5	3.0	12.75	12.75
1217	126837	160.5	163.6	3.0	10.7	10.70
1217	126838	163.6	166.6	3.0	9.65	9.65
1217	126839	166.6	169.7	3.0	9.55	9.55
1217	126840	169.7	172.7	3.0	4.2	4.20
1217	126841	172.7	175.8	3.0	8.1	8.10
1217	126842	175.8	178.8	3.0	10.4	10.40
1217	126843	178.8	181.9	3.0	10.1	10.10
1217	126844	181.9	184.9	3.0	12.7	12.70
1217	126845	184.9	188.0	3.0	12.45	12.45
1217	126846	188.0	191.0	3.0	9.65	9.65
1217	126847	191.0	194.1	3.0	10.35	10.35
1217	126848	194.1	197.1	3.0	4.85	4.85
1217	126849	197.1	200.1	3.0	5.6	5.60
1217	126850	200.1	203.2	3.0	4.9	4.90
1217	126851	203.2	206.2	3.0	6.7	6.70
1217	126853	206.2	209.3	3.0	0.65	0.65
1217	126854	209.3	212.3	3.0	5.65	5.65

1217	126855	212.3	215.4	3.0	8.75	8.75
1217	126856	215.4	218.4	3.0	4.2	4.20
1217	126857	218.4	221.5	3.0	9.65	9.65
1217	126858	221.5	224.5	3.0	8.5	8.50
1217	126859	224.5	227.6	3.0	8.45	8.45
1217	126860	227.6	230.6	3.0	10.1	10.10
1217	126861	230.6	233.7	3.0	10.05	10.05
1217	126862	233.7	236.7	3.0	9.45	9.45
1217	126863	236.7	239.8	3.0	10.45	10.45
1217	126864	239.8	242.8	3.0	11.1	11.10
1217	126865	242.8	245.9	3.0	11.25	11.25
1217	126867	245.9	248.9	3.0	14.05	14.05
1217	126868	248.9	252.0	3.0	10.8	10.80
1217	126869	252.0	255.0	3.0	10.25	10.25
1217	126870	255.0	258.1	3.0	9.85	9.85
1217	126871	258.1	261.1	3.0	7.6	7.60
1217	126872	261.1	264.2	3.0	9.25	9.25
1217	126873	264.2	267.2	3.0	9.9	9.90
1217	126874	267.2	270.3	3.0	7.7	7.70
1217	126875	270.3	273.3	3.0	9.75	9.75
1217	126876	273.3	276.3	3.0	8.1	8.10
1217	126877	276.3	279.4	3.0	10.85	10.85
1217	126878	279.4	282.4	3.0	12.1	12.10
1217	126880	282.4	285.5	3.0	13.05	13.05
1217	126881	285.5	288.5	3.0	12.25	12.25
1217	126883	288.5	291.6	3.0	9.45	9.45
1217	126884	291.6	294.6	3.0	13.1	13.10
1217	126885	294.6	297.7	3.0	9.35	9.35
1217	126886	297.7	300.7	3.0	9.8	9.80
1217	126887	300.7	303.8	3.0	9.3	9.30
1217	126888	303.8	306.8	3.0	13.05	13.05
1217	126889	306.8	309.9	3.0	9.8	9.80
1217	126890	309.9	312.9	3.0	12.9	12.90
1217	126891	312.9	316.0	3.0	2.05	2.05
1217	126892	316.0	319.0	3.0	7.95	7.95
1217	126893	319.0	322.1	3.0	9.3	9.30
1217	126894	322.1	325.1	3.0	6.85	6.85
1217	126895	325.1	328.2	3.0	15.95	15.95
1217	126896	328.2	331.2	3.0	9.6	9.60
1217	126897	331.2	334.3	3.0	7.55	7.55
1217	126898	334.3	337.3	3.0	6.55	6.55
1217	126899	337.3	340.4	3.0	7.55	7.55
1217	126900	340.4	343.4	3.0	13.95	13.95
1217	126901	343.4	346.5	3.0	12.75	12.75
1217	126902	346.5	349.5	3.0	8.1	8.10
1217	126903	349.5	352.5	3.0	8.85	8.85

1217	126904	352.5	355.6	3.0	11.95	11.95
1217	126905	355.6	358.6	3.0	9.55	9.55
1217	126906	358.6	361.7	3.0	11	11.00
1217	126907	361.7	364.7	3.0	11.9	11.90
1217	126908	364.7	367.8	3.0	10.7	10.70
1217	126909	367.8	370.8	3.0	5.45	5.45
1217	126911	370.8	373.9	3.0	2.15	2.15
1217	126912	373.9	376.9	3.0	8.25	8.25
1217	126913	376.9	380.0	3.0	9.2	9.20
1217	126914	380.0	383.0	3.0	9.3	9.30
1217	126915	383.0	386.1	3.0	8.6	8.60
1217	126917	386.1	389.1	3.0	10.05	10.05
1217	126918	389.1	392.2	3.0	12.15	12.15
1217	126919	392.2	395.2	3.0	12.2	12.20
1217	126920	395.2	398.3	3.0	12.95	12.95
1217	126921	398.3	401.3	3.0	12.05	12.05
1217	126922	401.3	404.4	3.0	6.35	6.35
1217	126923	404.4	407.4	3.0	11.95	11.95
1217	126924	407.4	410.5	3.0	10.45	10.45
1217	126925	410.5	413.5	3.0	13	13.00
1217	126927	413.5	416.6	3.0	8.15	8.15
1217	126928	416.6	419.6	3.0	10.45	10.45
1217	126929	419.6	422.7	3.0	12.35	12.35
1217	126930	422.7	423.4	0.7	11.8	11.80
1218	126563	3.0	7.0	4.0	2.8	2.80
1218	126564	7.0	10.0	3.0	4.95	4.95
1218	126565	10.0	13.1	3.0	5.2	5.20
1218	126566	13.1	16.1	3.0	10.25	10.25
1218	126567	16.1	19.2	3.0	4.6	4.60
1218	126568	19.2	22.2	3.0	5.6	5.60
1218	126569	22.2	25.3	3.0	7.85	7.85
1218	126570	25.3	28.3	3.0	5.1	5.10
1218	126571	28.3	31.4	3.0	5.5	5.50
1218	126572	31.4	34.4	3.0	4.85	4.85
1218	126573	34.4	37.5	3.0	4.4	4.40
1218	126574	37.5	40.5	3.0	5.05	5.05
1218	126575	40.5	43.6	3.0	3.15	3.15
1218	126576	43.6	46.6	3.0	5.55	5.55
1218	126577	46.6	49.7	3.0	4.5	4.50
1218	126579	49.7	52.7	3.0	4.7	4.70
1218	126580	52.7	55.8	3.0	4.75	4.75
1218	126582	55.8	58.8	3.0	7.4	7.40
1218	126583	58.8	61.9	3.0	4.95	4.95
1218	126584	61.9	64.9	3.0	8	8.00
1218	126585	64.9	68.0	3.0	6.1	6.10
1218	126586	68.0	71.0	3.0	3.4	3.40

1218	126587	71.0	74.1	3.0	3.25	3.25
1218	126588	74.1	77.1	3.0	10.95	10.95
1218	126589	77.1	80.2	3.0	9.2	9.20
1218	126590	80.2	83.2	3.0	4.95	4.95
1218	126591	83.2	86.2	3.0	4.05	4.05
1218	126592	86.2	89.3	3.0	5.4	5.40
1218	126593	89.3	92.3	3.0	3.85	3.85
1218	126594	92.3	95.4	3.0	6.9	6.90
1218	126595	95.4	98.4	3.0	3.95	3.95
1218	126597	98.4	101.5	3.0	5.9	5.90
1218	126598	101.5	104.5	3.0	5.3	5.30
1218	126599	104.5	107.6	3.0	2.7	2.70
1218	126600	107.6	110.6	3.0	3.95	3.95
1218	126601	110.6	113.7	3.0	9.65	9.65
1218	126602	113.7	116.7	3.0	5.1	5.10
1218	126603	116.7	119.8	3.0	5.1	5.10
1218	126604	119.8	122.8	3.0	8.4	8.40
1218	126605	122.8	125.9	3.0	6.6	6.60
1218	126606	125.9	128.9	3.0	5.55	5.55
1218	126607	128.9	132.0	3.0	10.8	10.80
1218	126608	132.0	135.0	3.0	15	15.00
1218	126609	135.0	138.1	3.0	16.45	16.45
1218	126610	138.1	141.1	3.0	10.65	10.65
1218	126612	141.1	144.2	3.0	9.6	9.60
1218	126613	144.2	147.2	3.0	11.2	11.20
1218	126614	147.2	150.3	3.0	11.2	11.20
1218	126615	150.3	153.3	3.0	11.5	11.50
1218	126616	153.3	156.4	3.0	8.8	8.80
1218	126617	156.4	159.4	3.0	4.45	4.45
1218	126618	159.4	162.4	3.0	6.8	6.80
1218	126619	162.4	165.5	3.0	10.1	10.10
1218	126620	165.5	168.5	3.0	10.4	10.40
1218	126621	168.5	171.6	3.0	8.65	8.65
1218	126622	171.6	174.6	3.0	8.7	8.70
1218	126623	174.6	177.7	3.0	5.8	5.80
1218	126624	177.7	180.7	3.0	8.3	8.30
1218	126625	180.7	183.8	3.0	7.9	7.90
1218	126626	183.8	186.8	3.0	5.55	5.55
1218	126627	186.8	189.9	3.0	6.7	6.70
1218	126629	189.9	192.9	3.0	9.45	9.45
1218	126630	192.9	196.0	3.0	8.45	8.45
1218	126631	196.0	199.0	3.0	7.60	7.60
1218	126632	199.0	202.1	3.0	9.85	9.85
1218	126633	202.1	205.1	3.0	10.65	10.65
1218	126634	205.1	208.2	3.0	10.45	10.45
1218	126635	208.2	211.2	3.0	9.85	9.85

1218	126636	211.2	214.3	3.0	8.9	8.90
1218	126637	214.3	217.3	3.0	8.4	8.40
1218	126638	217.3	220.4	3.0	10.6	10.60
1218	126639	220.4	223.4	3.0	10.95	10.95
1218	126640	223.4	226.5	3.0	9.3	9.30
1218	126641	226.5	229.5	3.0	11.2	11.20
1218	126642	229.5	232.6	3.0	9.9	9.90
1218	126643	232.6	235.6	3.0	13.1	13.10
1218	126644	235.6	238.6	3.0	8.7	8.70
1218	126645	238.6	241.7	3.0	10.25	10.25
1218	126647	241.7	244.7	3.0	8.05	8.05
1218	126648	244.7	247.8	3.0	5.65	5.65
1218	126649	247.8	250.8	3.0	3.45	3.45
1218	126650	250.8	253.9	3.0	7.15	7.15
1218	126651	253.9	256.9	3.0	7.1	7.10
1218	126652	256.9	260.0	3.0	10.1	10.10
1218	126653	260.0	263.0	3.0	8.5	8.50
1218	126654	263.0	266.1	3.0	9.05	9.05
1218	126655	266.1	269.1	3.0	8.9	8.90
1218	126656	269.1	272.2	3.0	7.55	7.55
1218	126657	272.2	275.2	3.0	10.2	10.20
1218	126658	275.2	278.3	3.0	9.85	9.85
1218	126659	278.3	281.3	3.0	10.85	10.85
1218	126660	281.3	284.4	3.0	10	10.00
1218	126662	284.4	287.4	3.0	8.5	8.50
1218	126663	287.4	290.5	3.0	7.6	7.60
1218	126664	290.5	293.5	3.0	16	16.00
1218	126665	293.5	296.6	3.0	8.35	8.35
1218	126666	296.6	299.6	3.0	10.65	10.65
1218	126667	299.6	302.7	3.0	6.05	6.05
1218	126668	302.7	305.7	3.0	4	4.00
1218	126669	305.7	308.8	3.0	10.95	10.95
1218	126670	308.8	311.8	3.0	9.65	9.65
1218	126671	311.8	314.8	3.0	6.3	6.30
1218	126672	314.8	317.9	3.0	5.9	5.90
1218	126673	317.9	320.9	3.0	9.2	9.20
1218	126674	320.9	324.0	3.0	4.9	4.90
1218	126675	324.0	327.0	3.0	8.3	8.30
1218	126676	327.0	330.1	3.0	11.45	11.45
1218	126677	330.1	333.1	3.0	10.8	10.80
1218	126679	333.1	336.2	3.0	8.3	8.30
1218	126680	336.2	339.2	3.0	7.05	7.05
1218	126681	339.2	342.3	3.0	4.05	4.05
1218	126682	342.3	345.3	3.0	0.75	0.75
1218	126683	345.3	348.4	3.0	0.55	0.55
1218	126684	348.4	351.4	3.0	4.6	4.60

1218	126685	351.4	354.5	3.0	5.6	5.60
1218	126686	354.5	357.5	3.0	5.95	5.95
1218	126687	357.5	360.6	3.0	7.35	7.35
1218	126688	360.6	363.6	3.0	6.45	6.45
1218	126689	363.6	366.7	3.0	7.4	7.40
1218	126690	366.7	369.7	3.0	5.55	5.55
1218	126691	369.7	372.8	3.0	6.1	6.10
1218	126692	372.8	375.8	3.0	3.1	3.10
1218	126693	375.8	378.9	3.0	4.3	4.30
1218	126694	378.9	381.9	3.0	4.6	4.60
1218	126696	381.9	385.0	3.0	6.15	6.15
1218	126697	385.0	388.0	3.0	4.5	4.50
1218	126699	388.0	391.0	3.0	3.2	3.20
1218	126700	391.0	394.1	3.0	2.4	2.40
1218	126701	394.1	397.1	3.0	8	8.00
1218	126702	397.1	399.6	2.5	8.6	8.60
1218	126703	399.6	402.6	3.0	8.5	8.50
1218	126704	402.6	405.6	3.0	9.5	9.50
1219	127630	20.2	23.2	3.0	BDL	0.05
1219	127631	23.2	26.2	3.0	BDL	0.05
1219	127632	26.2	29.3	3.0	BDL	0.05
1219	127633	29.3	32.3	3.0	0.1	0.10
1219	127635	32.3	35.4	3.0	BDL	0.05
1219	127636	35.4	38.4	3.0	BDL	0.05
1219	127637	38.4	41.5	3.0	BDL	0.05
1219	127638	41.5	44.5	3.0	BDL	0.05
1219	127639	44.5	47.6	3.0	BDL	0.05
1219	127640	47.6	50.6	3.0	BDL	0.05
1219	127641	50.6	53.7	3.0	0.8	0.80
1219	127643	53.7	56.7	3.0	0.3	0.30
1219	127644	56.7	59.8	3.0	BDL	0.05
1219	127645	59.8	62.8	3.0	BDL	0.05
1219	127646	62.8	65.9	3.0	BDL	0.05
1219	127647	65.9	68.9	3.0	BDL	0.05
1219	127648	68.9	72.0	3.0	BDL	0.05
1219	127649	72.0	75.0	3.0	BDL	0.05
1219	127650	75.0	78.1	3.0	BDL	0.05
1219	127651	78.1	81.1	3.0	BDL	0.05
1219	127652	81.1	84.2	3.0	BDL	0.05
1219	127653	84.2	87.2	3.0	BDL	0.05
1219	127655	87.2	90.3	3.0	BDL	0.05
1219	127656	90.3	93.3	3.0	BDL	0.05
1219	127657	93.3	96.4	3.0	3.6	3.60
1219	127658	96.4	99.4	3.0	0.15	0.15
1219	127659	99.4	102.4	3.0	BDL	0.05
1219	127660	102.4	105.5	3.0	BDL	0.05

1219	127661	105.5	108.5	3.0	BDL	0.05
1219	127662	108.5	111.6	3.0	0.1	0.10
1219	127663	111.6	114.6	3.0	BDL	0.05
1219	127664	114.6	117.7	3.0	BDL	0.05
1219	127665	117.7	120.7	3.0	0.55	0.55
1219	127666	120.7	123.8	3.0	0.45	0.45
1219	127667	123.8	126.8	3.0	0.35	0.35
1219	127668	126.8	129.9	3.0	1.35	1.35
1219	127669	129.9	132.9	3.0	2.15	2.15
1219	127670	132.9	136.0	3.0	1	1.00
1219	127671	136.0	139.0	3.0	1.15	1.15
1219	127673	139.0	142.1	3.0	0.45	0.45
1219	127675	142.1	145.1	3.0	0.4	0.40
1219	127676	145.1	148.2	3.0	1.3	1.30
1219	127677	148.2	151.2	3.0	3.95	3.95
1219	127678	151.2	154.3	3.0	2.55	2.55
1219	127679	154.3	157.3	3.0	2.85	2.85
1219	127680	157.3	160.4	3.0	1.95	1.95
1219	127681	160.4	163.4	3.0	1.05	1.05
1219	127682	163.4	166.5	3.0	1.45	1.45
1219	127683	166.5	169.5	3.0	1.75	1.75
1219	127684	169.5	172.6	3.0	2.65	2.65
1219	127685	172.6	175.6	3.0	2.7	2.70
1219	127686	175.6	178.6	3.0	5.1	5.10
1219	127687	178.6	181.7	3.0	6.8	6.80
1219	127688	181.7	184.7	3.0	2.3	2.30
1219	127689	184.7	187.8	3.0	5	5.00
1219	127690	187.8	190.8	3.0	5.8	5.80
1219	127691	190.8	193.9	3.0	5.3	5.30
1219	127692	193.9	196.9	3.0	2.2	2.20
1219	127693	196.9	200.0	3.0	1.75	1.75
1219	127695	200.0	203.0	3.0	BDL	0.05
1219	127696	203.0	206.1	3.0	0.25	0.25
1219	127697	206.1	209.1	3.0	4	4.00
1219	127698	209.1	212.2	3.0	3.15	3.15
1219	127699	212.2	215.2	3.0	6.45	6.45
1219	127700	215.2	218.3	3.0	9.75	9.75
1219	127701	218.3	221.3	3.0	16.3	16.30
1219	127703	221.3	224.4	3.0	14.65	14.65
1219	127704	224.4	227.4	3.0	12.05	12.05
1219	127705	227.4	230.5	3.0	11.65	11.65
1219	127706	230.5	233.5	3.0	8.8	8.80
1219	127707	233.5	236.6	3.0	9.35	9.35
1219	127708	236.6	239.6	3.0	7.5	7.50
1219	127709	239.6	242.7	3.0	8.25	8.25
1219	127710	242.7	245.7	3.0	5.8	5.80

1219	127711	245.7	248.8	3.0	4.15	4.15
1219	127712	248.8	251.8	3.0	2.25	2.25
1219	127713	251.8	254.8	3.0	5.75	5.75
1219	127715	254.8	257.9	3.0	9	9.00
1219	127716	257.9	260.9	3.0	8.85	8.85
1219	127717	260.9	264.0	3.0	10.7	10.70
1219	127718	264.0	267.0	3.0	5.45	5.45
1219	127719	267.0	270.1	3.0	5.6	5.60
1219	127720	270.1	273.1	3.0	8.55	8.55
1219	127721	273.1	276.2	3.0	9.7	9.70
1219	127722	276.2	279.2	3.0	8.8	8.80
1219	127723	279.2	282.3	3.0	8.3	8.30
1219	127724	282.3	285.3	3.0	6.05	6.05
1219	127725	285.3	288.4	3.0	8.1	8.10
1219	127726	288.4	291.4	3.0	5.6	5.60
1219	127727	291.4	294.5	3.0	6.3	6.30
1219	127728	294.5	297.5	3.0	5.6	5.60
1219	127729	297.5	300.6	3.0	6.05	6.05
1219	127730	300.6	303.6	3.0	3.65	3.65
1219	127731	303.6	306.7	3.0	7.65	7.65
1219	127733	306.7	309.7	3.0	6.05	6.05
1219	127735	309.7	312.8	3.0	8.15	8.15
1219	127736	312.8	315.8	3.0	7.5	7.50
1219	127737	315.8	318.9	3.0	9.6	9.60
1219	127738	318.9	321.9	3.0	4.6	4.60
1219	127739	321.9	325.0	3.0	1.7	1.70
1219	127740	325.0	328.0	3.0	6.4	6.40
1219	127741	328.0	331.0	3.0	6.4	6.40
1219	127742	331.0	334.1	3.0	4.45	4.45
1219	127743	334.1	337.1	3.0	4.55	4.55
1219	127744	337.1	340.2	3.0	4.05	4.05
1219	127745	340.2	343.2	3.0	2.8	2.80
1219	127746	343.2	346.3	3.0	6.15	6.15
1219	127747	346.3	349.3	3.0	7.4	7.40
1219	127748	349.3	352.4	3.0	4.4	4.40
1219	127749	352.4	355.4	3.0	5.2	5.20
1219	127750	355.4	358.5	3.0	4.65	4.65
1219	127751	358.5	361.5	3.0	2.7	2.70
1219	127752	361.5	364.6	3.0	2.1	2.10
1219	127753	364.6	367.6	3.0	5.95	5.95
1219	127755	367.6	370.7	3.0	2.6	2.60
1219	127756	370.7	373.7	3.0	4.7	4.70
1219	127757	373.7	376.8	3.0	4.65	4.65
1219	127758	376.8	379.8	3.0	4.3	4.30
1219	127759	379.8	382.9	3.0	3	3.00
1219	127760	382.9	385.9	3.0	4.3	4.30

1219	127761	385.9	389.0	3.0	3	3.00
1219	127763	389.0	392.0	3.0	4.2	4.20
1219	127764	392.0	395.1	3.0	4.2	4.20
1219	127765	395.1	398.1	3.0	4.05	4.05
1219	127766	398.1	401.2	3.0	1.65	1.65
1219	127767	401.2	404.2	3.0	2.6	2.60
1219	127768	404.2	407.2	3.0	0.35	0.35
1219	127769	407.2	410.3	3.0	0.1	0.10
1219	127770	410.3	413.3	3.0	2.4	2.40
1219	127771	413.3	416.4	3.0	BDL	0.05
1219	127772	416.4	419.4	3.0	4.6	4.60
1219	127773	419.4	422.5	3.0	3.4	3.40
1219	127775	422.5	425.5	3.0	2.7	2.70
1219	127776	425.5	428.6	3.0	0.8	0.80
1219	127777	428.6	431.6	3.0	0.2	0.20
1219	127778	431.6	434.7	3.0	5.35	5.35
1219	127779	434.7	437.7	3.0	4.55	4.55
1219	127780	437.7	440.8	3.0	2.7	2.70
1219	127781	440.8	444.2	3.4	4.05	4.05
1220	127801	25.6	27.7	2.1	BDL	0.05
1220	127802	27.7	30.7	3.0	BDL	0.05
1220	127803	30.7	33.8	3.0	BDL	0.05
1220	127804	33.8	36.8	3.0	BDL	0.05
1220	127806	36.8	39.9	3.0	BDL	0.05
1220	127807	39.9	42.9	3.0	BDL	0.05
1220	127808	42.9	46.0	3.0	BDL	0.05
1220	127809	46.0	49.0	3.0	0.4	0.40
1220	127810	49.0	52.1	3.0	1	1.00
1220	127811	52.1	55.1	3.0	BDL	0.05
1220	127812	55.1	58.2	3.0	BDL	0.05
1220	127813	58.2	61.2	3.0	BDL	0.05
1220	127815	61.2	64.3	3.0	0.1	0.10
1220	127816	64.3	67.3	3.0	0.15	0.15
1220	127817	67.3	70.4	3.0	BDL	0.05
1220	127818	70.4	73.4	3.0	1.4	1.40
1220	127819	73.4	76.5	3.0	1.45	1.45
1220	127820	76.5	79.5	3.0	BDL	0.05
1220	127821	79.5	82.6	3.0	1.75	1.75
1220	127822	82.6	85.6	3.0	BDL	0.05
1220	127823	85.6	88.7	3.0	0.2	0.20
1220	127824	88.7	91.7	3.0	BDL	0.05
1220	127825	91.7	94.8	3.0	0.7	0.70
1220	127826	94.8	97.8	3.0	0.75	0.75
1220	127827	97.8	100.9	3.0	BDL	0.05
1220	127828	100.9	103.9	3.0	BDL	0.05
1220	127830	103.9	106.9	3.0	0.1	0.10

1220	127831	106.9	110.0	3.0	BDL	0.05
1220	127832	110.0	113.0	3.0	BDL	0.05
1220	127833	113.0	116.1	3.0	BDL	0.05
1220	127834	116.1	119.1	3.0	BDL	0.05
1220	127835	119.1	122.2	3.0	0.45	0.45
1220	127836	122.2	125.2	3.0	0.3	0.30
1220	127837	125.2	128.3	3.0	0.4	0.40
1220	127838	128.3	131.3	3.0	0.75	0.75
1220	127839	131.3	134.4	3.0	0.7	0.70
1220	127840	134.4	137.4	3.0	1.2	1.20
1220	127841	137.4	140.5	3.0	0.1	0.10
1220	127842	140.5	143.5	3.0	0.4	0.40
1220	127843	143.5	146.6	3.0	1.5	1.50
1220	127844	146.6	149.6	3.0	2.35	2.35
1220	127846	149.6	152.7	3.0	2.5	2.50
1220	127847	152.7	155.7	3.0	3.15	3.15
1220	127848	155.7	158.8	3.0	3.5	3.50
1220	127849	158.8	161.8	3.0	2.8	2.80
1220	127850	161.8	164.9	3.0	3.85	3.85
1220	127851	164.9	167.9	3.0	3.55	3.55
1220	127852	167.9	171.0	3.0	5.15	5.15
1220	127853	171.0	174.0	3.0	3.35	3.35
1220	127855	174.0	177.1	3.0	3.45	3.45
1220	127856	177.1	180.1	3.0	4.45	4.45
1220	127857	180.1	183.1	3.0	5.35	5.35
1220	127858	183.1	186.2	3.0	4.35	4.35
1220	127860	186.2	189.2	3.0	3.5	3.50
1220	127861	189.2	192.3	3.0	1	1.00
1220	127862	192.3	195.3	3.0	2	2.00
1220	127863	195.3	198.4	3.0	2.75	2.75
1220	127864	198.4	201.4	3.0	4.2	4.20
1220	127865	201.4	204.5	3.0	2.35	2.35
1220	127866	204.5	207.5	3.0	3.5	3.50
1220	127867	207.5	210.6	3.0	4.95	4.95
1220	127868	210.6	213.6	3.0	3.7	3.70
1220	127869	213.6	216.7	3.0	2.55	2.55
1220	127870	216.7	219.7	3.0	3.5	3.50
1220	127871	219.7	222.8	3.0	2.3	2.30
1220	127872	222.8	225.8	3.0	2.6	2.60
1220	127873	225.8	228.9	3.0	4.65	4.65
1220	127874	228.9	231.9	3.0	4.65	4.65
1220	127875	231.9	235.0	3.0	5.45	5.45
1220	127876	235.0	238.0	3.0	5.55	5.55
1220	127877	238.0	241.1	3.0	2.3	2.30
1220	127878	241.1	244.1	3.0	3	3.00
1220	127879	244.1	247.2	3.0	3.95	3.95

1220	127880	247.2	250.2	3.0	4.55	4.55
1220	127881	250.2	253.3	3.0	3.2	3.20
1220	127882	253.3	256.3	3.0	1.6	1.60
1220	127883	256.3	259.3	3.0	2	2.00
1220	127884	259.3	262.4	3.0	2.35	2.35
1220	127886	262.4	265.4	3.0	2.35	2.35
1220	127887	265.4	268.5	3.0	4.75	4.75
1220	127888	268.5	271.5	3.0	3.8	3.80
1220	127890	271.5	274.6	3.0	8.15	8.15
1220	127891	274.6	277.6	3.0	6.8	6.80
1220	127892	277.6	280.7	3.0	0.85	0.85
1220	127893	280.7	283.7	3.0	0.45	0.45
1220	127895	283.7	286.8	3.0	1.2	1.20
1220	127896	286.8	289.8	3.0	0.75	0.75
1220	127897	289.8	292.9	3.0	1.1	1.10
1220	127898	292.9	295.9	3.0	1.1	1.10
1220	127899	295.9	299.0	3.0	1.2	1.20
1220	127900	299.0	302.0	3.0	0.75	0.75
1220	127901	302.0	306.4	4.4	0.7	0.70
1221	126931	9.1	10.4	1.3	1.5	1.50
1221	126932	10.4	13.4	3.0	3.65	3.65
1221	126933	13.4	16.5	3.0	3.1	3.10
1221	126934	16.5	19.5	3.0	2.35	2.35
1221	126935	19.5	22.6	3.0	4.65	4.65
1221	126936	22.6	25.6	3.0	4.85	4.85
1221	126937	25.6	27.1	1.5	8.95	8.95
1221	126938	27.1	28.7	1.6	7	7.00
1221	126939	28.7	31.7	3.0	5.9	5.90
1221	126940	31.7	34.8	3.0	9.9	9.90
1221	126941	34.8	37.8	3.0	7.75	7.75
1221	126942	37.8	41.8	4.0	8.7	8.70
1221	126943	41.8	43.9	2.1	8.3	8.30
1221	126944	43.9	47.9	4.0	7.15	7.15
1221	126945	47.9	50.0	2.1	6.8	6.80
1221	126946	50.0	53.0	3.0	9.65	9.65
1221	126947	53.0	56.1	3.0	4.6	4.60
1221	126948	56.1	59.1	3.0	5.15	5.15
1221	126949	59.1	62.2	3.0	8.85	8.85
1221	126951	62.2	65.2	3.0	10.6	10.60
1221	126952	65.2	68.3	3.0	7.85	7.85
1221	126953	68.3	71.3	3.0	8	8.00
1221	126954	71.3	74.4	3.0	10.5	10.50
1221	126955	74.4	77.4	3.0	9.95	9.95
1221	126956	77.4	80.5	3.0	8.5	8.50
1221	126957	80.5	83.5	3.0	7.7	7.70
1221	126958	83.5	86.6	3.0	8.8	8.80

1221	126959	86.6	89.6	3.0	9.7	9.70
1221	126960	89.6	92.7	3.0	13.45	13.45
1221	126961	92.7	95.7	3.0	12.05	12.05
1221	126962	95.7	98.8	3.0	8.1	8.10
1221	126963	98.8	101.8	3.0	16.55	16.55
1221	126964	101.8	104.9	3.0	12.7	12.70
1221	126965	104.9	107.9	3.0	8.9	8.90
1221	126966	107.9	111.0	3.0	9.1	9.10
1221	126967	111.0	114.0	3.0	9.9	9.90
1221	126968	114.0	117.1	3.0	13.75	13.75
1221	126969	117.1	120.1	3.0	11.6	11.60
1221	126971	120.1	123.2	3.0	13.7	13.70
1221	126972	123.2	126.2	3.0	12.25	12.25
1221	126973	126.2	129.2	3.0	9.6	9.60
1221	126974	129.2	132.3	3.0	10	10.00
1221	126975	132.3	135.3	3.0	10.35	10.35
1221	126976	135.3	138.4	3.0	9.7	9.70
1221	126977	138.4	141.4	3.0	8.8	8.80
1221	126978	141.4	144.5	3.0	10.55	10.55
1221	126979	144.5	146.4	1.9	3.25	3.25
1221	126980	146.4	149.4	3.0	2.15	2.15
1221	126982	149.4	150.5	1.1	1.2	1.20
1221	126983	150.5	153.5	3.0	5.7	5.70
1221	126984	153.5	156.6	3.0	6.65	6.65
1221	126985	156.6	159.6	3.0	10.3	10.30
1221	126986	159.6	162.7	3.0	10.35	10.35
1221	126987	162.7	165.7	3.0	10.1	10.10
1221	126988	165.7	168.8	3.0	8.75	8.75
1221	126989	168.8	171.8	3.0	11.15	11.15
1221	126991	171.8	174.9	3.0	5.85	5.85
1221	126992	174.9	177.9	3.0	6.75	6.75
1221	126993	177.9	181.0	3.0	8.15	8.15
1221	126994	181.0	184.0	3.0	11.45	11.45
1221	126996	184.0	187.1	3.0	10.7	10.70
1221	126997	187.1	190.1	3.0	11.45	11.45
1221	126998	190.1	193.2	3.0	9.65	9.65
1221	126999	193.2	196.2	3.0	4.55	4.55
1221	127000	196.2	199.3	3.0	5.55	5.55
1221	127001	199.3	202.3	3.0	10.45	10.45
1221	127002	202.3	205.4	3.0	7.5	7.50
1221	127003	205.4	208.4	3.0	15.45	15.45
1221	127004	208.4	211.5	3.0	9.75	9.75
1221	127005	211.5	214.5	3.0	14.75	14.75
1221	127006	214.5	217.6	3.0	1.6	1.60
1221	127007	217.6	220.6	3.0	10.05	10.05
1221	127008	220.6	223.7	3.0	8.4	8.40

1221	127009	223.7	226.7	3.0	10.25	10.25
1221	127010	226.7	229.7	3.0	8.6	8.60
1221	127011	229.7	232.8	3.0	10.95	10.95
1221	127012	232.8	235.8	3.0	8.15	8.15
1221	127013	235.8	238.9	3.0	6.85	6.85
1221	127014	238.9	241.9	3.0	10.85	10.85
1221	127015	241.9	245.0	3.0	12.75	12.75
1221	127016	245.0	248.0	3.0	7.65	7.65
1221	127017	248.0	251.1	3.0	12.6	12.60
1221	127020	251.1	254.1	3.0	9.5	9.50
1221	127021	254.1	257.2	3.0	8.75	8.75
1221	127022	257.2	260.2	3.0	9.95	9.95
1221	127023	260.2	263.3	3.0	9.1	9.10
1221	127024	263.3	266.3	3.0	1.4	1.40
1221	127025	266.3	269.4	3.0	1.05	1.05
1221	127026	269.4	272.4	3.0	0.8	0.80
1221	127027	272.4	275.5	3.0	10.05	10.05
1221	127028	275.5	278.5	3.0	11.7	11.70
1221	127029	278.5	281.6	3.0	13.25	13.25
1221	127220	281.6	284.6	3.0	10.9	10.90
1221	127221	284.6	287.7	3.0	15.35	15.35
1221	127222	287.7	290.7	3.0	13.6	13.60
1221	127223	290.7	293.8	3.0	11.1	11.10
1221	127224	293.8	296.8	3.0	12.05	12.05
1221	127225	296.8	299.9	3.0	10.5	10.50
1221	127226	299.9	302.9	3.0	0.85	0.85
1221	127227	302.9	305.9	3.0	15.7	15.70
1221	127228	305.9	309.0	3.0	10.85	10.85
1221	127229	309.0	312.1	3.1	11.35	11.35
1223	127030	7.0	11.0	4.0	1	1.00
1223	127031	11.0	14.0	3.0	BDL	0.05
1223	127032	14.0	17.1	3.0	1	1.00
1223	127033	17.1	20.1	3.0	5.65	5.65
1223	127034	20.1	23.2	3.0	4.25	4.25
1223	127035	23.2	26.2	3.0	2.5	2.50
1223	127037	26.2	29.3	3.0	1.05	1.05
1223	127038	29.3	32.3	3.0	0.15	0.15
1223	127039	32.3	35.4	3.0	1.65	1.65
1223	127040	35.4	38.4	3.0	5.6	5.60
1223	127041	38.4	41.5	3.0	4.25	4.25
1223	127042	41.5	44.5	3.0	4.95	4.95
1223	127043	44.5	47.6	3.0	2.55	2.55
1223	127044	47.6	50.6	3.0	3.2	3.20
1223	127045	50.6	53.7	3.0	7.3	7.30
1223	127046	53.7	56.7	3.0	0.3	0.30
1223	127047	56.7	59.8	3.0	3.1	3.10

1223	127048	59.8	62.8	3.0	3.2	3.20
1223	127050	62.8	65.9	3.0	5.55	5.55
1223	127051	65.9	68.9	3.0	6.95	6.95
1223	127052	68.9	72.0	3.0	7.65	7.65
1223	127053	72.0	75.0	3.0	3.8	3.80
1223	127054	75.0	78.1	3.0	4.8	4.80
1223	127055	78.1	81.1	3.0	0.2	0.20
1223	127056	81.1	84.2	3.0	0.1	0.10
1223	127057	84.2	87.2	3.0	3.05	3.05
1223	127058	87.2	90.2	3.0	10.3	10.30
1223	127059	90.2	93.3	3.0	5.8	5.80
1223	127060	93.3	96.3	3.0	5.8	5.80
1223	127061	96.3	99.4	3.0	10.3	10.30
1223	127062	99.4	102.4	3.0	17.85	17.85
1223	127063	102.4	105.5	3.0	11.05	11.05
1223	127064	105.5	108.5	3.0	7.3	7.30
1223	127065	108.5	111.6	3.0	5.9	5.90
1223	127066	111.6	114.6	3.0	7.8	7.80
1223	127067	114.6	117.7	3.0	6.75	6.75
1223	127068	117.7	120.7	3.0	4.05	4.05
1223	127069	120.7	123.8	3.0	8.05	8.05
1223	127070	123.8	126.8	3.0	9.15	9.15
1223	127071	126.8	129.9	3.0	10.8	10.80
1223	127073	129.9	132.9	3.0	10.2	10.20
1223	127074	132.9	136.0	3.0	7.8	7.80
1223	127075	136.0	139.0	3.0	8.9	8.90
1223	127076	139.0	142.9	3.9	9.2	9.20
1223	127077	142.9	145.1	2.2	10.9	10.90
1223	127078	145.1	148.1	3.0	7.8	7.80
1223	127079	148.1	151.2	3.0	2.4	2.40
1223	127082	151.2	154.2	3.0	5.05	5.05
1223	127083	154.2	157.3	3.0	3.75	3.75
1223	127084	157.3	160.3	3.0	6.95	6.95
1223	127085	160.3	163.4	3.0	8.8	8.80
1223	127086	163.4	166.4	3.0	8.9	8.90
1223	127087	166.4	169.5	3.0	2.75	2.75
1223	127088	169.5	172.5	3.0	11.1	11.10
1223	127090	172.5	175.6	3.0	10.9	10.90
1223	127091	175.6	178.6	3.0	9.05	9.05
1223	127092	178.6	181.7	3.0	8.5	8.50
1223	127093	181.7	184.7	3.0	8.1	8.10
1223	127094	184.7	187.8	3.0	9.5	9.50
1223	127095	187.8	190.8	3.0	7.45	7.45
1223	127096	190.8	193.9	3.0	3.35	3.35
1223	127097	193.9	196.9	3.0	4.95	4.95
1223	127098	196.9	199.9	3.0	9.85	9.85

1223	127099	199.9	200.9	1.0	4.6	4.60
1225	127101	3.7	4.9	1.2	11.85	11.85
1225	127102	4.9	7.9	3.0	4	4.00
1225	127103	7.9	11.0	3.0	9.55	9.55
1225	127104	11.0	14.0	3.0	8.9	8.90
1225	127105	14.0	17.1	3.0	7.45	7.45
1225	127106	17.1	20.1	3.0	6.1	6.10
1225	127107	20.1	23.2	3.0	9.25	9.25
1225	127108	23.2	26.2	3.0	3.8	3.80
1225	127109	26.2	29.3	3.0	5.6	5.60
1225	127110	29.3	32.3	3.0	5.8	5.80
1225	127111	32.3	35.4	3.0	7	7.00
1225	127113	35.4	38.4	3.0	2.5	2.50
1225	127114	38.4	41.5	3.0	6.5	6.50
1225	127115	41.5	44.5	3.0	8.45	8.45
1225	127116	44.5	47.6	3.0	5.85	5.85
1225	127117	47.6	50.6	3.0	5.5	5.50
1225	127118	50.6	53.7	3.0	10.85	10.85
1225	127119	53.7	56.7	3.0	11.95	11.95
1225	127120	56.7	59.8	3.0	12.8	12.80
1225	127121	59.8	62.8	3.0	11.75	11.75
1225	127122	62.8	65.9	3.0	11.75	11.75
1225	127123	65.9	68.9	3.0	12.5	12.50
1225	127124	68.9	72.0	3.0	11.65	11.65
1225	127125	72.0	75.0	3.0	12.7	12.70
1225	127126	75.0	78.1	3.0	8.5	8.50
1225	127127	78.1	81.1	3.0	10.35	10.35
1225	127129	81.1	84.1	3.0	13	13.00
1225	127130	84.1	87.2	3.0	12.85	12.85
1225	127131	87.2	90.2	3.0	12.4	12.40
1225	127133	90.2	93.3	3.0	8.95	8.95
1225	127135	93.3	96.3	3.0	10.15	10.15
1225	127136	96.3	99.4	3.0	1.1	1.10
1225	127137	99.4	102.4	3.0	BDL	0.05
1225	127138	102.4	106.5	4.1	2.4	2.40
1225	127139	106.5	109.5	3.0	11.3	11.30
1225	127140	109.5	112.6	3.0	7.95	7.95
1225	127141	112.6	115.6	3.0	8	8.00
1225	127142	115.6	118.7	3.0	9.5	9.50
1225	127143	118.7	121.7	3.0	6.3	6.30
1225	127144	121.7	124.8	3.0	11.3	11.30
1225	127145	124.8	127.8	3.0	13.05	13.05
1225	127146	127.8	130.9	3.0	12.9	12.90
1225	127147	130.9	133.9	3.0	6.15	6.15
1225	127148	133.9	137.0	3.0	12.35	12.35
1225	127149	137.0	140.0	3.0	13.15	13.15

1225	127150	140.0	143.1	3.0	10.9	10.90
1225	127151	143.1	146.1	3.0	11.7	11.70
1225	127152	146.1	149.2	3.0	8.55	8.55
1225	127153	149.2	152.2	3.0	4.6	4.60
1225	127154	152.2	155.3	3.0	2.85	2.85
1225	127155	155.3	158.3	3.0	10.25	10.25
1225	127157	158.3	161.4	3.0	7.8	7.80
1225	127158	161.4	164.4	3.0	10.3	10.30
1225	127159	164.4	167.5	3.0	12.1	12.10
1225	127160	167.5	170.5	3.0	6.05	6.05
1225	127161	170.5	173.6	3.0	11	11.00
1225	127162	173.6	176.6	3.0	7.3	7.30
1225	127163	176.6	179.7	3.0	14.7	14.70
1225	127164	179.7	182.7	3.0	12.7	12.70
1225	127165	182.7	185.7	3.0	13.3	13.30
1225	127166	185.7	188.8	3.0	10.9	10.90
1225	127167	188.8	191.8	3.0	13.5	13.50
1225	127168	191.8	194.9	3.0	13.2	13.20
1225	127169	194.9	197.9	3.0	8.8	8.80
1225	127170	197.9	201.0	3.0	5.55	5.55
1225	127171	201.0	204.0	3.0	7.75	7.75
1225	127172	204.0	207.1	3.0	1.3	1.30
1225	127173	207.1	210.1	3.0	5.85	5.85
1225	127174	210.1	213.2	3.0	13.5	13.50
1225	127175	213.2	216.2	3.0	6.15	6.15
1225	127177	216.2	218.6	2.4	5.95	5.95
1226	127240	2.3	4.9	2.6	0.65	0.65
1226	127241	4.9	7.9	3.0	0.2	0.20
1226	127242	7.9	11.0	3.0	2.7	2.70
1226	127244	11.0	14.0	3.0	3.25	3.25
1226	127245	14.0	17.1	3.0	5.5	5.50
1226	127246	17.1	20.1	3.0	1.6	1.60
1226	127247	20.1	23.2	3.0	1.35	1.35
1226	127248	23.2	26.2	3.0	2.05	2.05
1226	127249	26.2	29.3	3.0	5.85	5.85
1226	127251	29.3	32.3	3.0	9	9.00
1226	127252	32.3	35.4	3.0	3.7	3.70
1226	127253	35.4	38.4	3.0	9.6	9.60
1226	127254	38.4	41.5	3.0	6.4	6.40
1226	127255	41.5	44.5	3.0	5.45	5.45
1226	127257	44.5	47.6	3.0	8.35	8.35
1226	127258	47.6	50.6	3.0	11	11.00
1226	127259	50.6	53.7	3.0	13.2	13.20
1226	127260	53.7	56.7	3.0	10.25	10.25
1226	127261	56.7	59.8	3.0	12.3	12.30
1226	127262	59.8	62.8	3.0	12.4	12.40

1226	127263	62.8	65.9	3.0	8.2	8.20
1226	127264	65.9	68.9	3.0	7.85	7.85
1226	127265	68.9	72.0	3.0	5.65	5.65
1226	127266	72.0	75.0	3.0	4.25	4.25
1226	127267	75.0	78.1	3.0	0.95	0.95
1226	127268	78.1	81.1	3.0	1.9	1.90
1226	127269	81.1	84.1	3.0	5.3	5.30
1226	127270	84.1	87.2	3.0	5.55	5.55
1226	127271	87.2	90.2	3.0	5.6	5.60
1226	127272	90.2	93.3	3.0	7	7.00
1226	127273	93.3	96.3	3.0	3.05	3.05
1226	127274	96.3	99.4	3.0	2.75	2.75
1226	127275	99.4	102.4	3.0	8.4	8.40
1226	127276	102.4	105.5	3.0	2.8	2.80
1226	127278	105.5	108.5	3.0	2.75	2.75
1226	127279	108.5	111.6	3.0	4.3	4.30
1226	127280	111.6	114.6	3.0	6.45	6.45
1226	127282	114.6	117.7	3.0	8.5	8.50
1226	127283	117.7	120.7	3.0	8	8.00
1226	127284	120.7	123.8	3.0	6.75	6.75
1226	127285	123.8	126.8	3.0	5.2	5.20
1226	127286	126.8	129.9	3.0	6.95	6.95
1226	127287	129.9	132.9	3.0	6.6	6.60
1226	127288	132.9	136.0	3.0	5.8	5.80
1226	127289	136.0	139.0	3.0	11.5	11.50
1226	127291	139.0	142.1	3.0	11.05	11.05
1226	127292	142.1	145.1	3.0	7.85	7.85
1226	127293	145.1	148.2	3.0	7.5	7.50
1226	127294	148.2	151.2	3.0	6.9	6.90
1226	127295	151.2	154.3	3.0	10.6	10.60
1226	127296	154.3	157.3	3.0	9.85	9.85
1226	127297	157.3	160.3	3.0	10.8	10.80
1226	127298	160.3	163.4	3.0	5.7	5.70
1226	127299	163.4	166.4	3.0	10.35	10.35
1226	127300	166.4	169.5	3.0	7.85	7.85
1226	127301	169.5	172.5	3.0	6.75	6.75
1226	127302	172.5	175.6	3.0	8.95	8.95
1226	127303	175.6	178.6	3.0	11.75	11.75
1226	127304	178.6	181.7	3.0	6.75	6.75
1226	127305	181.7	184.7	3.0	10.6	10.60
1226	127306	184.7	187.8	3.0	9.65	9.65
1226	127307	187.8	190.8	3.0	2.95	2.95
1226	127308	190.8	193.9	3.0	4.4	4.40
1226	127309	193.9	196.9	3.0	9	9.00
1226	127310	196.9	200.0	3.0	10.15	10.15
1226	127311	200.0	203.0	3.0	9.1	9.10

1226	127312	203.0	206.1	3.0	10.45	10.45
1226	127314	206.1	209.1	3.0	11.4	11.40
1226	127316	209.1	212.2	3.0	10.7	10.70
1226	127317	212.2	215.2	3.0	11.2	11.20
1226	127318	215.2	218.3	3.0	7	7.00
1226	127319	218.3	221.3	3.0	11.7	11.70
1226	127320	221.3	224.4	3.0	11.4	11.40
1226	127321	224.4	227.4	3.0	7.35	7.35
1226	127322	227.4	230.5	3.0	6.9	6.90
1226	127323	230.5	233.5	3.0	7.8	7.80
1226	127324	233.5	236.5	3.0	6.7	6.70
1226	127325	236.5	239.6	3.0	7.5	7.50
1226	127326	239.6	242.6	3.0	9.45	9.45
1226	127327	242.6	245.7	3.0	8.2	8.20
1226	127328	245.7	248.7	3.0	4.7	4.70
1226	127329	248.7	251.8	3.0	4.8	4.80
1226	127331	251.8	254.8	3.0	6	6.00
1226	127332	254.8	257.9	3.0	7.85	7.85
1226	127333	257.9	260.9	3.0	5.95	5.95
1226	127334	260.9	264.0	3.0	4.55	4.55
1226	127335	264.0	267.0	3.0	5.35	5.35
1226	127336	267.0	270.1	3.0	3.1	3.10
1226	127337	270.1	273.1	3.0	10.95	10.95
1226	127339	273.1	275.4	2.3	10.15	10.15
1229	127351	209.0	212.0	3.0	BDL	0.05
1229	127352	212.0	215.1	3.0	BDL	0.05
1229	127353	215.1	218.1	3.0	0.15	0.15
1229	127355	218.1	221.2	3.0	BDL	0.05
1229	127356	221.2	224.2	3.0	0.15	0.15
1229	127357	224.2	227.3	3.0	BDL	0.05
1229	127358	227.3	230.3	3.0	0.15	0.15
1229	127359	230.3	233.4	3.0	0.9	0.90
1229	127360	233.4	236.4	3.0	0.35	0.35
1229	127362	236.4	239.5	3.0	BDL	0.05
1229	127363	239.5	242.5	3.0	0.5	0.50
1229	127364	242.5	245.6	3.0	1.15	1.15
1229	127365	245.6	248.6	3.0	1.3	1.30
1229	127366	248.6	251.7	3.0	4.7	4.70
1229	127367	251.7	254.7	3.0	3.05	3.05
1229	127368	254.7	257.8	3.0	2.75	2.75
1229	127369	257.8	260.8	3.0	5.2	5.20
1229	127370	260.8	263.9	3.0	3.75	3.75
1229	127371	263.9	266.9	3.0	2.75	2.75
1229	127372	266.9	270.0	3.0	5.25	5.25
1229	127373	270.0	273.0	3.0	3.35	3.35
1229	127374	273.0	276.1	3.0	7.8	7.80

1229	127375	276.1	279.1	3.0	7.55	7.55
1229	127377	279.1	282.2	3.0	8.75	8.75
1229	127378	282.2	285.2	3.0	2.6	2.60
1229	127379	285.2	288.2	3.0	7.35	7.35
1229	127380	288.2	291.3	3.0	10.7	10.70
1229	127381	291.3	294.3	3.0	9.75	9.75
1229	127382	294.3	297.4	3.0	14.6	14.60
1229	127383	297.4	300.4	3.0	12.3	12.30
1229	127385	300.4	303.5	3.0	10.3	10.30
1229	127386	303.5	306.5	3.0	10.35	10.35
1229	127387	306.5	309.6	3.0	11.65	11.65
1229	127388	309.6	312.6	3.0	10	10.00
1229	127389	312.6	315.7	3.0	12.3	12.30
1229	127390	315.7	318.7	3.0	7.25	7.25
1229	127391	318.7	321.8	3.0	8.8	8.80
1229	127392	321.8	324.8	3.0	4.05	4.05
1229	127393	324.8	327.9	3.0	7.15	7.15
1229	127394	327.9	330.9	3.0	9.35	9.35
1229	127395	330.9	334.0	3.0	8.15	8.15
1229	127396	334.0	337.0	3.0	7.2	7.20
1229	127397	337.0	340.1	3.0	3.5	3.50
1229	127398	340.1	343.1	3.0	7.15	7.15
1229	127399	343.1	346.2	3.0	8.35	8.35
1229	127400	346.2	349.2	3.0	7.35	7.35
1229	127402	349.2	352.3	3.0	9.85	9.85
1229	127403	352.3	355.3	3.0	9.15	9.15
1229	127404	355.3	358.4	3.0	11.7	11.70
1229	127405	358.4	361.4	3.0	10.85	10.85
1229	127406	361.4	364.4	3.0	9.6	9.60
1229	127407	364.4	367.5	3.0	10.8	10.80
1229	127408	367.5	370.5	3.0	11.7	11.70
1229	127409	370.5	373.6	3.0	10.9	10.90
1229	127410	373.6	376.6	3.0	10.9	10.90
1229	127411	376.6	379.7	3.0	12.8	12.80
1229	127412	379.7	382.7	3.0	4.2	4.20
1229	127413	382.7	385.8	3.0	7.25	7.25
1229	127415	385.8	388.8	3.0	10.8	10.80
1229	127417	388.8	391.9	3.0	14.7	14.70
1229	127418	391.9	394.9	3.0	12.2	12.20
1229	127419	394.9	398.0	3.0	14.5	14.50
1229	127420	398.0	401.0	3.0	9.3	9.30
1229	127421	401.0	404.1	3.0	12.8	12.80
1229	127422	404.1	407.1	3.0	11.4	11.40
1229	127423	407.1	410.2	3.0	14.5	14.50
1229	127424	410.2	413.2	3.0	9.95	9.95
1229	127425	413.2	416.3	3.0	16	16.00

1229	127426	416.3	419.3	3.0	10.9	10.90
1229	127427	419.3	422.4	3.0	8.9	8.90
1229	127428	422.4	425.4	3.0	7.8	7.80
1229	127428	425.4	428.5	3.0	7.8	7.80
1229	127429	428.5	431.5	3.0	10.95	10.95
1229	127430	431.5	434.6	3.0	4.4	4.40
1229	127431	434.6	437.6	3.0	7.95	7.95
1229	127432	437.6	440.6	3.0	6.0	6.00
1229	127433	440.6	443.7	3.0	6.2	6.20
1229	127434	443.7	446.7	3.0	6.3	6.30
1229	127435	446.7	450.2	3.5	7.3	7.30
1232	127910	15.2	18.2	3.0	0.4	0.40
1232	127911	18.2	21.3	3.0	BDL	0.05
1232	127912	21.3	24.3	3.0	BDL	0.05
1232	127914	24.3	27.4	3.0	BDL	0.05
1232	127915	27.4	30.4	3.0	BDL	0.05
1232	127916	30.4	33.5	3.0	0.1	0.10
1232	127917	33.5	36.5	3.0	BDL	0.05
1232	127918	36.5	39.6	3.0	0.1	0.10
1232	127919	39.6	42.6	3.0	BDL	0.05
1232	127920	42.6	45.7	3.0	0.1	0.10
1232	127922	45.7	48.7	3.0	BDL	0.05
1232	127923	48.7	51.8	3.0	BDL	0.05
1232	127924	51.8	54.8	3.0	BDL	0.05
1232	127925	54.8	57.9	3.0	BDL	0.05
1232	127927	57.9	60.9	3.0	BDL	0.05
1232	127928	60.9	64.0	3.0	BDL	0.05
1232	127929	64.0	67.0	3.0	BDL	0.05
1232	127930	67.0	70.1	3.0	BDL	0.05
1232	127931	70.1	73.1	3.0	BDL	0.05
1232	127932	73.1	76.2	3.0	BDL	0.05
1232	127933	76.2	79.2	3.0	0.1	0.10
1232	127934	79.2	82.3	3.0	0.2	0.20
1232	127935	82.3	85.3	3.0	2.45	2.45
1232	127936	85.3	88.4	3.0	3.05	3.05
1232	127937	88.4	91.4	3.0	0.5	0.50
1232	127938	91.4	94.4	3.0	0.15	0.15
1232	127939	94.4	97.5	3.0	1.3	1.30
1232	127940	97.5	100.5	3.0	0.45	0.45
1232	127941	100.5	103.6	3.0	BDL	0.05
1232	127942	103.6	106.6	3.0	0.1	0.10
1232	127944	106.6	109.7	3.0	0.15	0.15
1232	127945	109.7	112.7	3.0	2.65	2.65
1232	127946	112.7	115.8	3.0	0.45	0.45
1232	127947	115.8	118.8	3.0	2.3	2.30
1232	127948	118.8	121.9	3.0	0.1	0.10

1232	127949	121.9	124.9	3.0	BDL	0.05
1232	127950	124.9	128.0	3.0	0.15	0.15
1232	127951	128.0	131.0	3.0	BDL	0.05
1232	127952	131.0	134.1	3.0	0.15	0.15
1232	127953	134.1	137.1	3.0	BDL	0.05
1232	127954	137.1	140.2	3.0	BDL	0.05
1232	127955	140.2	143.2	3.0	BDL	0.05
1232	127956	143.2	146.3	3.0	BDL	0.05
1232	127957	146.3	149.3	3.0	0.1	0.10
1232	127958	149.3	152.4	3.0	BDL	0.05
1232	127959	152.4	155.4	3.0	BDL	0.05
1232	127960	155.4	158.5	3.0	BDL	0.05
1232	127962	158.5	161.5	3.0	BDL	0.05
1232	127963	161.5	164.6	3.0	BDL	0.05
1232	127964	164.6	167.6	3.0	BDL	0.05
1232	127965	167.6	170.6	3.0	BDL	0.05
1232	127967	170.6	173.7	3.0	BDL	0.05
1232	127968	173.7	176.7	3.0	0.15	0.15
1232	127969	176.7	179.8	3.0	0.2	0.20
1232	127970	179.8	182.8	3.0	BDL	0.05
1232	127971	182.8	185.9	3.0	0.1	0.10
1232	127972	185.9	188.9	3.0	0.1	0.10
1232	127974	188.9	192.0	3.0	BDL	0.05
1232	127975	192.0	195.0	3.0	0.2	0.20
1232	127976	195.0	198.1	3.0	0.1	0.10
1232	127977	198.1	201.1	3.0	BDL	0.05
1232	127978	201.1	204.2	3.0	BDL	0.05
1232	127979	204.2	207.2	3.0	BDL	0.05
1232	127980	207.2	210.3	3.0	BDL	0.05
1232	127981	210.3	213.3	3.0	BDL	0.05
1232	127982	213.3	216.4	3.0	0.25	0.25
1232	127983	216.4	219.6	3.2	BDL	0.05
1245	127451	334.5	337.5	3.0	BDL	0.05
1245	127453	337.5	340.6	3.0	BDL	0.05
1245	127454	340.6	343.6	3.0	BDL	0.05
1245	127455	343.6	346.7	3.0	BDL	0.05
1245	127456	346.7	349.7	3.0	BDL	0.05
1245	127458	349.7	352.8	3.0	BDL	0.05
1245	127459	352.8	355.8	3.0	BDL	0.05
1245	127461	355.8	358.9	3.0	BDL	0.05
1245	127462	358.9	361.9	3.0	0.1	0.10
1245	127463	361.9	365.0	3.0	BDL	0.05
1245	127464	365.0	368.0	3.0	BDL	0.05
1245	127465	368.0	371.1	3.0	BDL	0.05
1245	127466	371.1	374.1	3.0	BDL	0.05
1245	127467	374.1	377.2	3.0	BDL	0.05

1245	127468	377.2	380.2	3.0	BDL	0.05
1245	127469	380.2	383.3	3.0	0.1	0.10
1245	127470	383.3	386.3	3.0	BDL	0.05
1245	127471	386.3	389.4	3.0	0.1	0.10
1245	127472	389.4	392.4	3.0	BDL	0.05
1245	127473	392.4	395.5	3.0	BDL	0.05
1245	127474	395.5	398.5	3.0	BDL	0.05
1245	127475	398.5	401.6	3.0	BDL	0.05
1245	127476	401.6	404.6	3.0	BDL	0.05
1245	127477	404.6	407.7	3.0	BDL	0.05
1245	127478	407.7	410.7	3.0	BDL	0.05
1245	127479	410.7	413.7	3.0	BDL	0.05
1245	127481	413.7	416.8	3.0	BDL	0.05
1245	127482	416.8	419.8	3.0	BDL	0.05
1245	127483	419.8	422.9	3.0	BDL	0.05
1245	127484	422.9	425.9	3.0	BDL	0.05
1245	127485	425.9	429.0	3.0	0.1	0.10
1245	127486	429.0	432.0	3.0	BDL	0.05
1245	127487	432.0	435.1	3.0	BDL	0.05
1245	127488	435.1	438.1	3.0	BDL	0.05
1245	127489	438.1	441.2	3.0	BDL	0.05
1245	127490	441.2	444.2	3.0	BDL	0.05
1245	127491	444.2	447.3	3.0	0.15	0.15
1245	127492	447.3	450.3	3.0	BDL	0.05
1245	127493	450.3	453.4	3.0	0.1	0.10
1245	127494	453.4	456.4	3.0	0.15	0.15
1245	127495	456.4	459.5	3.0	0.15	0.15
1245	127496	459.5	462.5	3.0	0.15	0.15
1245	127498	462.5	465.6	3.0	BDL	0.05
1245	127499	465.6	468.6	3.0	BDL	0.05
1245	127500	468.6	471.7	3.0	BDL	0.05
1245	127501	471.7	474.7	3.0	BDL	0.05
1245	127503	474.7	477.8	3.0	BDL	0.05
1245	127504	477.8	480.8	3.0	BDL	0.05
1245	127506	480.8	483.9	3.0	0.1	0.10
1245	127507	483.9	486.9	3.0	0.15	0.15
1245	127508	486.9	489.9	3.0	BDL	0.05
1245	127509	489.9	493.0	3.0	BDL	0.05
1246	127520	401.5	404.5	3.0	BDL	0.05
1246	127522	404.5	407.6	3.0	BDL	0.05
1246	127523	407.6	410.6	3.0	BDL	0.05
1246	127524	410.6	413.7	3.0	BDL	0.05
1246	127525	413.7	416.7	3.0	BDL	0.05
1246	127527	416.7	419.8	3.0	BDL	0.05
1246	127528	419.8	422.8	3.0	0.1	0.10
1246	127530	422.8	425.9	3.0	BDL	0.05

1246	127531	425.9	428.9	3.0	BDL	0.05
1246	127532	428.9	432.0	3.0	BDL	0.05
1246	127533	432.0	435.0	3.0	BDL	0.05
1246	127534	435.0	438.1	3.0	0.2	0.20
1246	127535	438.1	441.1	3.0	BDL	0.05
1246	127536	441.1	444.2	3.0	BDL	0.05
1246	127537	444.2	447.2	3.0	BDL	0.05
1246	127538	447.2	450.3	3.0	BDL	0.05
1246	127539	450.3	453.3	3.0	BDL	0.05
1246	127540	453.3	456.4	3.0	BDL	0.05
1246	127541	456.4	459.4	3.0	BDL	0.05
1246	127542	459.4	462.5	3.0	BDL	0.05
1246	127543	462.5	465.5	3.0	BDL	0.05
1246	127544	465.5	468.6	3.0	BDL	0.05
1246	127545	468.6	471.6	3.0	BDL	0.05
1246	127547	471.6	474.7	3.0	BDL	0.05
1246	127548	474.7	477.7	3.0	BDL	0.05
1246	127549	477.7	480.7	3.0	BDL	0.05
1246	127550	480.7	483.8	3.0	BDL	0.05
1246	127551	483.8	486.8	3.0	BDL	0.05
1246	127552	486.8	489.9	3.0	0.15	0.15
1246	127553	489.9	492.9	3.0	BDL	0.05
1246	127554	492.9	496.0	3.0	BDL	0.05
1246	127555	496.0	499.0	3.0	BDL	0.05
1246	127556	499.0	502.1	3.0	BDL	0.05
1246	127557	502.1	505.1	3.0	BDL	0.05
1246	127558	505.1	508.2	3.0	BDL	0.05
1246	127559	508.2	511.2	3.0	BDL	0.05
1246	127560	511.2	514.3	3.0	0.1	0.10
1246	127561	514.3	517.3	3.0	BDL	0.05
1246	127562	517.3	520.4	3.0	BDL	0.05
1246	127563	520.4	523.4	3.0	0.15	0.15
1246	127564	523.4	526.5	3.0	BDL	0.05
1246	127565	526.5	529.5	3.0	0.1	0.10
1246	127567	529.5	532.6	3.0	0.1	0.10
1246	127569	532.6	535.6	3.0	BDL	0.05
1246	127570	535.6	538.7	3.0	0.1	0.10
1246	127572	538.7	541.7	3.0	BDL	0.05
1246	127573	541.7	544.8	3.0	BDL	0.05
1246	127574	544.8	545.7	0.9	BDL	0.05
BS0702	430363	3.4	6.1	2.7	6.1	6.07
BS0702	430364	6.1	9.1	3.0	6.8	6.80
BS0702	430365	9.1	12.2	3.1	5.2	5.20
BS0702	430367	12.2	15.2	3.0	5.5	5.53
BS0702	430368	15.2	18.2	3.0	3.9	3.93
BS0702	430369	18.2	18.7	0.5	0.2	0.20

BS0702	430370	18.7	21.3	2.6	3.9	3.87
BS0702	430371	21.3	21.7	0.4	4.3	4.33
BS0702	430372	21.7	23.3	1.6	0.0	0.00
BS0702	430373	23.3	24.4	1.1	4.7	4.73
BS0702	430374	24.4	27.0	2.6	6.0	6.00
BS0702	430375	27.0	28.1	1.1	0.3	0.27
BS0702	430376	28.1	30.5	2.4	2.2	2.20
BS0702	430377	30.5	33.5	3.0	6.0	6.00
BS0702	430378	33.5	36.5	3.0	10.2	10.20
BS0702	430379	36.5	39.6	3.1	4.1	4.07
BS0702	430380	39.6	42.6	3.0	6.6	6.60
BS0702	430381	42.6	45.7	3.1	1.9	1.87
BS0702	430382	45.7	48.8	3.1	2.5	2.53
BS0702	430383	48.8	51.8	3.0	3.6	3.60
BS0702	430384	51.8	54.3	2.5	2.3	2.27
BS0702	430385	54.3	54.9	0.6	7.7	7.67
BS0702	430387	54.9	57.9	3.0	3.8	3.80
BS0702	430388	57.9	61.0	3.1	1.9	1.93
BS0702	430389	61.0	64.0	3.0	3.7	3.73
BS0702	430390	64.0	67.0	3.0	1.9	1.87
BS0702	430391	67	70.1	3.1	6.5	6.53
BS0702	430392	70.1	73.2	3.1	4.5	4.53
BS0702	430393	73.2	76.2	3.0	1.7	1.73
BS0702	430394	76.2	79.2	3.0	2.5	2.47
BS0702	430395	79.2	82.3	3.1	4.7	4.73
BS0702	430396	82.3	85.3	3.0	7.9	7.87
BS0702	430397	85.3	88.4	3.1	4.3	4.33
BS0702	430398	88.4	91.4	3.0	6.7	6.67
BS0702	430399	91.4	94.5	3.1	6.8	6.80
BS0702	430400	94.5	97.5	3.0	3.0	3.00
BS0702	430401	97.5	100.6	3.1	5.7	5.73
BS0702	430402	100.6	103.6	3.0	6.9	6.93
BS0702	430403	103.6	106.7	3.1	8.8	8.80
BS0702	430404	106.7	109.7	3.0	3.1	3.13
BS0702	430405	109.7	112.8	3.1	4.1	4.13
BS0702	430406	112.8	115.8	3.0	6.8	6.80
BS0702	430408	115.8	118.9	3.1	10.6	10.60
BS0702	430409	118.9	121.9	3.0	5.6	5.60
BS0702	430410	121.9	123.4	1.5	1.3	1.27
BS0702	430411	123.4	125.6	2.2	0.2	0.20
BS0702	430412	125.6	128	2.4	2.3	2.33
BS0702	430413	128	131.1	3.1	4.5	4.53
BS0702	430414	131.1	134.1	3.0	3.6	3.60
BS0702	430415	134.1	137.1	3.0	0.3	0.27
BS0702	430416	137.1	140.2	3.1	0.4	0.40
BS0702	430417	140.2	143.3	3.1	0.3	0.33

BS0702	430418	143.3	146.5	3.2	1.7	1.67
BS0702	430419	146.5	147.7	1.2	0.9	0.93
BS0702	430420	147.7	149.4	1.7	3.0	3.00
BS0702	430421	149.4	151.4	2.0	6.5	6.47
BS0702	430422	151.4	153	1.6	4.0	4.00
BS0702	430423	153	156	3.0	0.5	0.53
BS0702	430424	156	158.5	2.5	1.3	1.33
BS0702	430425	158.5	161.5	3.0	3.5	3.47
BS0702	430427	161.5	165	3.5	2.9	2.93
BS0702	430428	165	167.6	2.6	5.2	5.20
BS0702	430429	167.6	170.7	3.1	2.7	2.73
BS0702	430430	170.7	173.7	3.0	2.1	2.13
BS0702	430431	173.7	176.8	3.1	2.4	2.40
BS0702	430432	176.8	180	3.2	3.8	3.80
BS0702	430433	180	182.9	2.9	1.6	1.60
BS0702	430434	182.9	185.9	3.0	0.2	0.20
BS0702	430435	185.9	189	3.1	BDL	0.05
BS0702	430436	189	191	2.0	0.1	0.13
BS0702	430437	191	195.1	4.1	0.1	0.13
BS0702	430438	195.1	198.1	3.0	0.1	0.13
BS0702	430439	198.1	201.1	3.0	0.1	0.13
BS0702	430440	201.1	204	2.9	BDL	0.05
BS0702	430441	204	207.3	3.3	0.1	0.13
BS0702	430442	207.3	210.3	3.0	BDL	0.05
BS0702	430443	210.3	213.3	3.0	BDL	0.05
BS0702	430444	213.3	216.4	3.1	BDL	0.05
BS0702	430445	216.4	219.5	3.1	0.2	0.20
BS0702	430446	219.5	222.5	3.0	0.2	0.20
BS0702	430447	222.5	225.5	3.0	0.2	0.20
BS0702	430448	225.5	228.6	3.1	0.2	0.15
BS0702	430450	228.6	231.6	3.0	0.1	0.15
BS0702	430451	231.6	234.7	3.1	BDL	0.05
BS0702	430452	234.7	237.7	3.0	BDL	0.05
BS0702	430453	237.7	240.8	3.1	0.2	0.15
BS0702	430454	240.8	243.8	3.0	BDL	0.05
BS0702	430455	243.8	246.9	3.1	BDL	0.05
BS0702	430456	246.9	249.9	3.0	BDL	0.05
BS0702	430457	249.9	253	3.1	BDL	0.05
BS0702	430458	253	256	3.0	0.1	0.10
BS0702	430459	256	259.1	3.1	BDL	0.05
BS0702	430460	259.1	262.1	3.0	BDL	0.05
BS0702	430461	262.1	265.2	3.1	BDL	0.05
BS0702	430462	265.2	268.2	3.0	0.1	0.10
BS0702	430463	268.2	271.3	3.1	0.1	0.10
BS0702	430464	271.3	274.3	3.0	BDL	0.05
BS0702	430465	274.3	277.4	3.1	BDL	0.05

BS0702	430466	277.4	280.4	3.0	BDL	0.05
BS0702	430467	280.4	283.5	3.1	0.1	0.10
BS0702	430468	283.5	286.5	3.0	BDL	0.05
BS0702	430469	286.5	289.6	3.1	BDL	0.05
BS0702	430470	289.6	292.6	3.0	BDL	0.05
BS0702	430472	292.6	295.7	3.1	BDL	0.05
BS0702	430473	295.7	298.7	3.0	BDL	0.05
BS0702	430474	298.7	301.8	3.1	BDL	0.05
BS0702	430475	301.8	304.8	3.0	BDL	0.05
BS0702	430476	304.8	307.8	3.0	BDL	0.05
BS0702	430477	307.8	310.9	3.1	BDL	0.05
BS0702	430478	310.9	313.9	3.0	BDL	0.05
BS0702	430479	313.9	317	3.1	BDL	0.05
BS0702	430480	317	320	3.0	BDL	0.05
BS0702	430481	320	323.1	3.1	BDL	0.05
BS0702	430482	323.1	326.1	3.0	0.1	0.10
BS0702	430483	326.1	329.2	3.1	BDL	0.05
BS0702	430484	329.2	332.2	3.0	BDL	0.05
BS0702	430485	332.2	335.3	3.1	BDL	0.05
BS0702	430486	335.3	338.3	3.0	BDL	0.05
BS0702	430487	338.3	341.4	3.1	BDL	0.05
BS0702	430488	341.4	344.4	3.0	BDL	0.05
BS0702	430490	344.4	347.5	3.1	BDL	0.05
BS0702	430491	347.5	350	2.5	BDL	0.05
BS0702	430492	350	353.6	3.6	BDL	0.05
BS0702	430493	353.6	356.6	3.0	BDL	0.05
BS0702	430494	356.6	359.7	3.1	BDL	0.05
BS0702	430495	359.7	362.7	3.0	BDL	0.05
BS0702	430496	362.7	365.8	3.1	BDL	0.05
BS0702	430497	365.8	368.9	3.1	BDL	0.05
BS0702	430498	368.9	371.9	3.0	BDL	0.05
BS0702	430499	371.9	374.9	3.0	BDL	0.05
BS0702	430500	374.9	378	3.1	BDL	0.05
BS0702	430701	378	381	3.0	BDL	0.05
BS0702	430702	381	384	3.0	BDL	0.05
BS0702	430703	384	387.1	3.1	BDL	0.05
BS0702	430704	387.1	390.1	3.0	BDL	0.05
BS0702	430705	390.1	393.2	3.1	BDL	0.05
BS0703	430706	18.3	21.3	3.0	0.2	0.20
BS0703	430707	21.3	24.4	3.1	0.3	0.30
BS0703	430708	24.4	27.4	3.0	0.2	0.20
BS0703	430709	27.4	30.5	3.1	0.3	0.35
BS0703	430710	30.5	33.5	3.0	1.0	0.95
BS0703	430711	33.5	36.6	3.1	5.2	5.20
BS0703	430712	36.6	39.6	3.0	1.4	1.40
BS0703	430713	39.6	42.7	3.1	0.3	0.35

BS0703	430714	42.7	45.7	3.0	BDL	0.05
BS0703	430715	45.7	48.8	3.1	0.2	0.20
BS0703	430716	48.8	51.8	3.0	0.2	0.15
BS0703	430717	51.8	54.9	3.1	0.2	0.15
BS0703	430718	54.9	57.9	3.0	0.1	0.10
BS0703	430720	57.9	61	3.1	0.2	0.15
BS0703	430721	61	64	3.0	0.2	0.20
BS0703	430722	64	67.1	3.1	0.2	0.15
BS0703	430723	67.1	70.1	3.0	0.2	0.20
BS0703	430724	70.1	73.2	3.1	BDL	0.05
BS0703	430725	73.2	76.2	3.0	0.2	0.20
BS0703	430726	76.2	79.2	3.0	0.2	0.20
BS0703	430727	79.2	82.3	3.1	0.2	0.20
BS0703	430728	82.3	85.3	3.0	0.2	0.15
BS0703	430729	85.3	88.4	3.1	0.1	0.10
BS0703	430730	88.4	91.4	3.0	0.1	0.10
BS0703	430731	91.4	94.5	3.1	BDL	0.05
BS0703	430732	94.5	97.5	3.0	1.4	1.40
BS0703	430733	97.5	100.6	3.1	BDL	0.05
BS0703	430734	100.6	103.6	3.0	0.1	0.10
BS0703	430735	103.6	106.7	3.1	0.2	0.15
BS0703	430736	106.7	109.7	3.0	0.1	0.10
BS0703	430737	109.7	112.8	3.1	BDL	0.05
BS0703	430739	112.8	115.8	3.0	0.2	0.15
BS0703	430740	115.8	118.9	3.1	BDL	0.05
BS0703	430741	118.9	121.9	3.0	BDL	0.05
BS0703	430742	121.9	125	3.1	BDL	0.05
BS0703	430743	125	128	3.0	BDL	0.05
BS0703	430744	128	131.1	3.1	BDL	0.05
BS0703	430745	131.1	134.1	3.0	BDL	0.05
BS0703	430746	134.1	137.2	3.1	0.2	0.15
BS0703	430747	137.2	140.2	3.0	BDL	0.05
BS0703	430748	140.2	143.3	3.1	BDL	0.05
BS0703	430749	143.3	146.3	3.0	BDL	0.05
BS0703	430750	146.3	149.4	3.1	BDL	0.05
BS0703	430751	149.4	152.4	3.0	BDL	0.05
BS0703	430752	152.4	155.4	3.0	BDL	0.05
BS0703	430753	155.4	158.5	3.1	BDL	0.05
BS0703	430754	158.5	161.5	3.0	BDL	0.05
BS0703	430755	161.5	164.6	3.1	0.1	0.10
BS0703	430756	164.6	167.6	3.0	BDL	0.05
BS0703	430757	167.6	170.7	3.1	BDL	0.05
BS0703	430758	170.7	173.7	3.0	BDL	0.05
BS0703	430760	173.7	176.8	3.1	0.2	0.15
BS0703	430761	176.8	180	3.2	BDL	0.05
BS0703	430762	180	182.9	2.9	BDL	0.05

BS0703	430763	182.9	185.9	3.0	BDL	0.05
BS0703	430764	185.9	189	3.1	BDL	0.05
BS0703	430765	189	192	3.0	BDL	0.05
BS0703	430766	192	195.1	3.1	0.1	0.10
BS0703	430767	195.1	198.1	3.0	BDL	0.05
BS0703	430768	198.1	201.2	3.1	BDL	0.05
BS0703	430769	201.2	204.2	3.0	0.1	0.10
BS0703	430770	204.2	207.3	3.1	BDL	0.05
BS0703	430771	207.3	210.3	3.0	0.1	0.10
BS0703	430772	210.3	213.4	3.1	0.1	0.10
BS0703	430773	213.4	216.4	3.0	BDL	0.05
BS0703	430774	216.4	219.5	3.1	BDL	0.05
BS0703	430775	219.5	222.5	3.0	0.3	0.25
BS0703	430776	222.5	225.6	3.1	0.1	0.10
BS0703	430777	225.6	228.6	3.0	BDL	0.05
BS0703	430779	228.6	231.6	3.0	BDL	0.05
BS0703	430780	231.6	234.7	3.1	BDL	0.05
BS0703	430781	234.7	237.7	3.0	BDL	0.05
BS0703	430782	237.7	240.8	3.1	BDL	0.05
BS0703	430783	240.8	243.8	3.0	BDL	0.05
BS0703	430784	243.8	246.9	3.1	0.1	0.10
BS0703	430785	246.9	250	3.1	BDL	0.05
BS0703	430786	250	253	3.0	0.2	0.15
BS0703	430787	253	256	3.0	BDL	0.05
BS0703	430788	256	259.1	3.1	BDL	0.05
BS0703	430789	259.1	262.1	3.0	BDL	0.05
BS0703	430790	262.1	265.2	3.1	0.1	0.15
BS0703	430791	265.2	268.2	3.0	BDL	0.05
BS0703	430792	268.2	271.3	3.1	0.2	0.15
BS0703	430793	271.3	274.3	3.0	0.1	0.10
BS0703	430794	274.3	277.4	3.1	0.2	0.20
BS0703	430795	277.4	280.4	3.0	BDL	0.05
BS0703	430796	280.4	283.5	3.1	0.3	0.30
BS0703	430797	283.5	286.5	3.0	0.2	0.15
BS0703	430798	286.5	289.6	3.1	BDL	0.05
BS0703	430799	289.6	292.6	3.0	0.1	0.10
BS0703	430801	292.6	295.7	3.1	0.2	0.20
BS0704	431084	5.5	6.7	1.2	0.2	0.15
BS0704	431085	6.7	9.8	3.1	0.4	0.40
BS0704	431086	9.8	12.8	3.0	0.2	0.20
BS0704	431087	12.8	15.8	3.0	0.2	0.15
BS0704	431088	15.8	18.9	3.1	0.6	0.55
BS0704	431089	18.9	21.9	3.0	0.2	0.15
BS0704	431090	21.9	25	3.1	BDL	0.05
BS0704	431092	25	26.2	1.2	BDL	0.05
BS0704	431093	26.2	27	0.8	0.2	0.20

BS0704	431094	27	28	1.0	0.2	0.15
BS0704	431095	28	31.1	3.1	0.4	0.40
BS0704	431096	31.1	34.1	3.0	0.6	0.65
BS0704	431097	34.1	37.2	3.1	0.2	0.25
BS0704	431098	37.2	40.2	3.0	0.6	0.65
BS0704	431099	40.2	43.3	3.1	0.1	0.10
BS0704	431101	43.3	46.3	3.0	0.1	0.10
BS0704	431102	46.3	49.4	3.1	0.2	0.20
BS0704	431103	49.4	52.4	3.0	BDL	0.05
BS0704	431104	52.4	55.5	3.1	0.4	0.40
BS0704	431105	55.5	58.5	3.0	0.1	0.10
BS0704	431106	58.5	61.6	3.1	0.2	0.15
BS0704	431107	61.6	64.6	3.0	0.1	0.10
BS0704	431108	64.6	67.7	3.1	0.2	0.15
BS0704	431109	67.7	70.7	3.0	BDL	0.05
BS0704	431110	70.7	73.8	3.1	0.2	0.15
BS0704	431111	73.8	76.8	3.0	BDL	0.05
BS0704	431112	76.8	79.9	3.1	0.8	0.85
BS0704	431113	79.9	82.9	3.0	0.2	0.15
BS0704	431114	82.9	85.9	3.0	BDL	0.05
BS0704	431115	85.9	89	3.1	BDL	0.05
BS0704	431116	89	92	3.0	BDL	0.05
BS0704	431117	92	95.1	3.1	BDL	0.05
BS0704	431118	95.1	98.1	3.0	BDL	0.05
BS0704	431119	98.1	101.2	3.1	BDL	0.05
BS0704	431120	101.2	104.2	3.0	BDL	0.05
BS0704	431121	104.2	107.3	3.1	BDL	0.05
BS0704	431123	107.3	110.3	3.0	BDL	0.05
BS0704	431124	110.3	113.4	3.1	BDL	0.05
BS0704	431125	113.4	116.4	3.0	BDL	0.05
BS0704	431126	116.4	119.5	3.1	0.6	0.65
BS0704	431127	119.5	122.5	3.0	BDL	0.05
BS0704	431128	122.5	125.6	3.1	1.3	1.30
BS0704	431129	125.6	128.6	3.0	BDL	0.05
BS0704	431130	128.6	131.7	3.1	BDL	0.05
BS0704	431131	131.7	134.7	3.0	BDL	0.05
BS0704	431132	134.7	137.8	3.1	BDL	0.05
BS0704	431133	137.8	140.8	3.0	BDL	0.05
BS0704	431134	140.8	143.9	3.1	BDL	0.05
BS0704	431135	143.9	146.9	3.0	BDL	0.05
BS0704	431136	146.9	150	3.1	0.1	0.10
BS0704	431137	150	153	3.0	BDL	0.05
BS0704	431138	153	156.1	3.1	BDL	0.05
BS0704	431139	156.1	159.1	3.0	0.1	0.10
BS0704	431140	159.1	162.2	3.1	BDL	0.05
BS0704	431141	162.2	165.2	3.0	0.2	0.20

BS0704	431143	165.2	168.2	3.0	0.4	0.40
BS0704	431144	168.2	171.3	3.1	0.1	0.10
BS0704	431145	171.3	174.3	3.0	BDL	0.05
BS0704	431146	174.3	177.4	3.1	BDL	0.05
BS0704	431147	177.4	180.4	3.0	BDL	0.05
BS0704	431148	180.4	183.5	3.1	0.2	0.20
BS0704	431149	183.5	186.5	3.0	BDL	0.05
BS0704	431150	186.5	189.6	3.1	BDL	0.05
BS0704	431151	189.6	191.5	1.9	0.1	0.10
BS0704	431152	191.5	195	3.5	BDL	0.05
BS0704	431153	195	198.7	3.7	0.2	0.15
BS0704	431154	198.7	201.8	3.1	BDL	0.05
BS0704	431155	201.8	204.8	3.0	BDL	0.05
BS0704	431156	204.8	207.9	3.1	0.2	0.20
BS0704	431157	207.9	210.9	3.0	BDL	0.05
BS0704	431158	210.9	214	3.1	0.3	0.25
BS0704	431159	214	217	3.0	BDL	0.05
BS0704	431160	217	220.1	3.1	BDL	0.05
BS0704	431161	220.1	223.1	3.0	BDL	0.05
BS0704	431162	223.1	226.2	3.1	BDL	0.05
BS0704	431163	226.2	229.2	3.0	BDL	0.05
BS0704	431165	229.2	232.3	3.1	0.1	0.10
BS0704	431166	232.3	235.3	3.0	0.1	0.10
BS0704	431167	235.3	238.4	3.1	0.1	0.10
BS0704	431168	238.4	241.4	3.0	BDL	0.05
BS0704	431169	241.4	244.4	3.0	BDL	0.05
BS0704	431170	244.4	247.5	3.1	0.1	0.10
BS0704	431171	247.5	250.5	3.0	BDL	0.05
BS0704	431172	250.5	253.6	3.1	BDL	0.05
BS0704	431173	253.6	256.6	3.0	BDL	0.05
BS0704	431174	256.6	259.7	3.1	BDL	0.05
BS0704	431175	259.7	261.6	1.9	BDL	0.05
BS0704	431176	261.6	262.7	1.1	BDL	0.05
BS0704	431177	262.7	265.8	3.1	BDL	0.05
BS0704	431178	265.8	268.8	3.0	0.1	0.10
BS0704	431179	268.8	271.9	3.1	BDL	0.05
BS0704	431180	271.9	274.9	3.0	BDL	0.05
BS0704	431181	274.9	278	3.1	BDL	0.05
BS0704	431182	278	281	3.0	BDL	0.05
BS0704	431183	281	284	3.0	BDL	0.05
BS0704	431184	284	286.3	2.3	0.1	0.10
BS0704	431186	286.3	286.9	0.6	BDL	0.05
BS0704	431187	286.9	290.2	3.3	BDL	0.05
BS0704	431188	290.2	291	0.8	0.1	0.10
BS0704	431189	291	291.5	0.5	BDL	0.05
BS0704	431190	291.5	293.2	1.7	BDL	0.05

BS0704	431191	293.2	296.3	3.1	BDL	0.05
BS0704	431192	296.3	299.3	3.0	BDL	0.05
BS0704	431193	299.3	299.8	0.5	0.4	0.40
BS0704	431194	299.8	300.2	0.4	BDL	0.05
BS0704	431195	300.2	302.3	2.1	BDL	0.05
BS0704	431196	302.3	305.4	3.1	BDL	0.05
BS0704	431197	305.4	308.5	3.1	0.2	0.15
BS0704	431198	308.5	311.5	3.0	BDL	0.05
BS0704	431199	311.5	313.2	1.7	BDL	0.05
BS0704	431200	313.2	314.6	1.4	1.5	1.50
BS0704	431201	314.6	317.6	3.0	0.4	0.45
BS0704	431202	317.6	320.6	3.0	0.7	0.75
BS0704	431203	320.6	323.7	3.1	0.3	0.35
BS0704	431204	323.7	326.7	3.0	1.0	1.00
BS0704	431206	326.7	329.8	3.1	0.6	0.55
BS0704	431207	329.8	330.5	0.7	0.1	0.10
BS0704	431208	330.5	331.4	0.9	4.1	4.05
BS0704	431209	331.4	332.8	1.4	0.1	0.10
BS0704	431210	332.8	335.9	3.1	0.7	0.70
BS0704	431211	335.9	338.9	3.0	BDL	0.05
BS0704	431212	338.9	342	3.1	BDL	0.05
BS0704	431213	342	345	3.0	0.2	0.15
BS0704	431214	345	348.1	3.1	0.6	0.60
BS0704	431215	348.1	351.1	3.0	BDL	0.05
BS0704	431216	351.1	354	2.9	0.5	0.45
BS0704	431217	354	356.7	2.7	0.2	0.20
BS0704	431218	356.7	360	3.3	0.5	0.45
BS0705	430929	3.5	6.1	2.6	BDL	0.05
BS0705	430930	6.1	9.1	3.0	4.3	4.30
BS0705	430931	9.1	12.2	3.1	2.9	2.90
BS0705	430932	12.2	15.2	3.0	1.0	1.00
BS0705	430934	15.2	17	1.8	4.5	4.45
BS0705	430935	17	17.5	0.5	1.5	1.45
BS0705	430936	17.5	18.3	0.8	2.0	2.00
BS0705	430937	18.3	21.3	3.0	1.8	1.80
BS0705	430938	21.3	24.6	3.3	0.9	0.85
BS0705	430939	24.6	25.6	1.0	4.1	4.05
BS0705	430940	25.6	27.4	1.8	1.6	1.60
BS0705	430941	27.4	30.5	3.1	2.1	2.10
BS0705	430942	30.5	33.5	3.0	0.6	0.55
BS0705	430943	33.5	36.6	3.1	1.4	1.40
BS0705	430944	36.6	39.6	3.0	1.2	1.20
BS0705	430945	39.6	42.7	3.1	0.6	0.55
BS0705	430946	42.7	45.7	3.0	0.7	0.70
BS0705	430947	45.7	48.8	3.1	0.6	0.60
BS0705	430948	48.8	51.8	3.0	0.6	0.60

BS0705	430949	51.8	54.9	3.1	0.2	0.15
BS0705	430950	54.9	57.9	3.0	0.8	0.80
BS0705	430951	57.9	60.7	2.8	0.2	0.25
BS0705	430953	60.7	64	3.3	2.1	2.10
BS0705	430954	64	67.1	3.1	1.9	1.90
BS0705	430955	67.1	70.1	3.0	0.6	0.65
BS0705	430956	70.1	73.2	3.1	0.3	0.25
BS0705	430957	73.2	76.2	3.0	0.4	0.40
BS0705	430958	76.2	79.2	3.0	0.2	0.15
BS0705	430959	79.2	82.3	3.1	BDL	0.05
BS0705	430960	82.3	85.3	3.0	0.3	0.30
BS0705	430961	85.3	88.4	3.1	0.2	0.20
BS0705	430962	88.4	91.4	3.0	0.7	0.70
BS0705	430963	91.4	94.5	3.1	0.9	0.95
BS0705	430964	94.5	97.5	3.0	0.2	0.15
BS0705	430965	97.5	100.6	3.1	0.3	0.30
BS0705	430966	100.6	103.6	3.0	BDL	0.05
BS0705	430967	103.6	106.7	3.1	0.1	0.13
BS0705	430968	106.7	109.7	3.0	0.2	0.15
BS0705	430969	109.7	112.8	3.1	1.1	1.10
BS0705	430970	112.8	115.8	3.0	0.7	0.70
BS0705	430972	115.8	118.9	3.1	0.4	0.40
BS0705	430973	118.9	121.9	3.0	1.6	1.55
BS0705	430974	121.9	125	3.1	BDL	0.05
BS0705	430975	125	128	3.0	BDL	0.05
BS0705	430976	128	131.1	3.1	BDL	0.05
BS0705	430977	131.1	134.1	3.0	0.1	0.10
BS0705	430978	134.1	137.2	3.1	0.2	0.15
BS0705	430979	137.2	140.2	3.0	BDL	0.05
BS0705	430980	140.2	143.3	3.1	BDL	0.05
BS0705	430981	143.3	146.3	3.0	0.1	0.15
BS0705	430982	146.3	149.4	3.1	0.2	0.15
BS0705	430983	149.4	152.4	3.0	0.1	0.10
BS0705	430984	152.4	155.4	3.0	BDL	0.05
BS0705	430985	155.4	158.5	3.1	BDL	0.05
BS0705	430986	158.5	161.5	3.0	0.1	0.10
BS0705	430987	161.5	164.5	3.0	BDL	0.05
BS0705	430988	164.5	167.6	3.1	BDL	0.05
BS0705	430990	167.6	170.7	3.1	BDL	0.05
BS0705	430991	170.7	173.7	3.0	BDL	0.05
BS0705	430992	173.7	176.7	3.0	BDL	0.05
BS0705	430993	176.7	179.8	3.1	BDL	0.05
BS0705	430994	179.8	182.9	3.1	0.2	0.20
BS0705	430995	182.9	185.9	3.0	0.1	0.10
BS0705	430996	185.9	189	3.1	BDL	0.05
BS0705	430997	189	192	3.0	BDL	0.05

BS0705	430998	192	195.1	3.1	0.1	0.10
BS0705	430999	195.1	198.1	3.0	BDL	0.05
BS0705	431000	198.1	201.2	3.1	BDL	0.05
BS0705	431001	201.2	204.2	3.0	BDL	0.05
BS0705	431002	204.2	207.3	3.1	BDL	0.05
BS0705	431003	207.3	210.3	3.0	0.2	0.15
BS0705	431004	210.3	213.4	3.1	BDL	0.05
BS0705	431005	213.4	216.4	3.0	BDL	0.05
BS0705	431006	216.4	219.5	3.1	BDL	0.05
BS0705	431007	219.5	222.5	3.0	BDL	0.05
BS0705	431009	222.5	225.6	3.1	BDL	0.05
BS0705	431010	225.6	228.6	3.0	BDL	0.05
BS0705	431011	228.6	231.6	3.0	BDL	0.05
BS0705	431012	231.6	234.7	3.1	BDL	0.05
BS0705	431013	234.7	237.7	3.0	BDL	0.05
BS0705	431014	237.7	240.8	3.1	BDL	0.05
BS0705	431015	240.8	243.8	3.0	BDL	0.05
BS0705	431016	243.8	246.9	3.1	BDL	0.05
BS0705	431017	246.9	249.9	3.0	BDL	0.05
BS0705	431018	249.9	253	3.1	BDL	0.05
BS0705	431019	253	256	3.0	BDL	0.05
BS0705	431020	256	259.1	3.1	BDL	0.05
BS0705	431021	259.1	262.1	3.0	BDL	0.05
BS0705	431022	262.1	265.2	3.1	BDL	0.05
BS0705	431023	265.2	268.2	3.0	BDL	0.05
BS0705	431024	268.2	271.3	3.1	BDL	0.05
BS0705	431025	271.3	274.2	2.9	BDL	0.05
BS0705	431026	274.2	277.4	3.2	0.1	0.10
BS0705	431027	277.4	280.4	3.0	BDL	0.05
BS0705	431028	280.4	283.5	3.1	BDL	0.05
BS0705	431030	283.5	286.5	3.0	BDL	0.05
BS0705	431031	286.5	289.6	3.1	BDL	0.05
BS0705	431032	289.6	292.6	3.0	BDL	0.05
BS0705	431033	292.6	295.7	3.1	0.1	0.10
BS0705	431034	295.7	298.7	3.0	0.1	0.10
BS0705	431035	298.7	301.7	3.0	BDL	0.05
BS0705	431036	301.7	304.8	3.1	BDL	0.05
BS0705	431037	304.8	307.8	3.0	BDL	0.05
BS0705	431038	307.8	310.9	3.1	0.2	0.15
BS0705	431039	310.9	313.9	3.0	BDL	0.05
BS0705	431040	313.9	317	3.1	BDL	0.05
BS0705	431041	317	320	3.0	BDL	0.05
BS0705	431042	320	323.1	3.1	BDL	0.05
BS0705	431043	323.1	326.1	3.0	BDL	0.05
BS0705	431044	326.1	329.2	3.1	BDL	0.05
BS0705	431045	329.2	332.2	3.0	BDL	0.05

BS0705	431046	332.2	335.3	3.1	BDL	0.05
BS0705	431047	335.3	338.3	3.0	BDL	0.05
BS0705	431048	338.3	341.4	3.1	BDL	0.05
BS0705	431049	341.4	344.4	3.0	BDL	0.05
BS0705	431051	344.4	347.5	3.1	BDL	0.05
BS0705	431052	347.5	350.5	3.0	BDL	0.05
BS0705	431053	350.5	353.6	3.1	0.1	0.10
BS0705	431054	353.6	356.6	3.0	BDL	0.05
BS0705	431055	356.6	359.7	3.1	BDL	0.05
BS0705	431056	359.7	362.7	3.0	BDL	0.05
BS0705	431057	362.7	365.8	3.1	BDL	0.05
BS0705	431058	365.8	368.8	3.0	0.2	0.15
BS0705	431059	368.8	370.4	1.6	0.1	0.10
BS0705	431060	370.4	371.5	1.1	0.1	0.10
BS0705	431061	371.5	371.9	0.4	BDL	0.05
BS0705	431062	371.9	374.9	3.0	BDL	0.05
BS0705	431063	374.9	377.9	3.0	BDL	0.05
BS0705	431064	377.9	378.7	0.8	BDL	0.05
BS0705	431065	378.7	379.6	0.9	0.2	0.15
BS0705	431066	379.6	381	1.4	0.2	0.15
BS0705	431067	381	384	3.0	0.1	0.10
BS0705	431068	384	387.1	3.1	BDL	0.05
BS0705	431070	387.1	390.1	3.0	BDL	0.05
BS0705	431071	390.1	393.2	3.1	BDL	0.05
BS0705	431072	393.2	396.2	3.0	0.3	0.25
BS0705	431073	396.2	399.3	3.1	0.2	0.15
BS0705	431074	399.3	402.3	3.0	0.1	0.10
BS0705	431075	402.3	405.4	3.1	BDL	0.05
BS0705	431076	405.4	408.4	3.0	0.2	0.15
BS0705	431077	408.4	411.5	3.1	0.1	0.10
BS0705	431078	411.5	414.5	3.0	0.1	0.10
BS0705	431079	414.5	417.6	3.1	0.1	0.10
BS0705	431080	417.6	420.6	3.0	BDL	0.05
BS0705	431081	420.6	423.7	3.1	0.1	0.10
BS0705	431082	423.7	426.7	3.0	BDL	0.05
BS0705	431083	426.7	429.8	3.1	BDL	0.05
BS0710	430802	10.7	18.3	7.6	0.1	0.10
BS0710	430803	18.3	21.3	3.0	0.2	0.15
BS0710	430804	21.3	24.4	3.1	0.1	0.10
BS0710	430805	24.4	27.4	3.0	BDL	0.05
BS0710	430806	27.4	30.5	3.1	BDL	0.05
BS0710	430807	30.5	33.5	3.0	BDL	0.05
BS0710	430808	33.5	36.6	3.1	0.2	0.15
BS0710	430809	36.6	39.6	3.0	0.3	0.30
BS0710	430810	39.6	42.7	3.1	0.1	0.10
BS0710	430811	42.7	45.7	3.0	BDL	0.05

BS0710	430812	45.7	48.8	3.1	BDL	0.05
BS0710	430813	48.8	51.8	3.0	BDL	0.05
BS0710	430814	51.8	54.9	3.1	0.2	0.25
BS0710	430815	54.9	57.9	3.0	BDL	0.05
BS0710	430816	57.9	61	3.1	BDL	0.05
BS0710	430817	61	64	3.0	BDL	0.05
BS0710	430819	64	67.1	3.1	BDL	0.05
BS0710	430820	67.1	68.3	1.2	BDL	0.05
BS0710	430821	68.3	69.7	1.4	0.2	0.15
BS0710	430822	69.7	70.1	0.4	0.1	0.10
BS0710	430823	70.1	73.2	3.1	0.3	0.25
BS0710	430824	73.2	76.2	3.0	0.3	0.35
BS0710	430825	76.2	79.2	3.0	BDL	0.05
BS0710	430826	79.2	81.3	2.1	0.1	0.10
BS0710	430827	81.3	85.3	4.0	BDL	0.05
BS0710	430828	85.3	86	0.7	BDL	0.05
BS0710	430829	86	87.3	1.3	BDL	0.05
BS0710	430830	87.3	88.4	1.1	0.1	0.10
BS0710	430831	88.4	91.4	3.0	BDL	0.05
BS0710	430832	91.4	94.5	3.1	BDL	0.05
BS0710	430833	94.5	97.5	3.0	1.3	1.25
BS0710	430834	97.5	100.5	3.0	8.3	8.35
BS0710	430835	100.5	103.6	3.1	BDL	0.05
BS0710	430836	103.6	106.7	3.1	BDL	0.05
BS0710	430837	106.7	109.7	3.0	0.1	0.10
BS0710	430838	109.7	112.8	3.1	0.1	0.10
BS0710	430840	112.8	115.8	3.0	0.1	0.10
BS0710	430841	115.8	118.9	3.1	BDL	0.05
BS0710	430842	118.9	121.9	3.0	0.1	0.10
BS0710	430843	121.9	125	3.1	BDL	0.05
BS0710	430844	125	128	3.0	BDL	0.05
BS0710	430845	128	131.1	3.1	BDL	0.05
BS0710	430846	131.1	134.1	3.0	BDL	0.05
BS0710	430847	134.1	137.2	3.1	BDL	0.05
BS0710	430848	137.2	140.2	3.0	0.1	0.10
BS0710	430849	140.2	143.3	3.1	BDL	0.05
BS0710	430850	143.3	146.3	3.0	BDL	0.05
BS0710	430851	146.3	149.4	3.1	BDL	0.05
BS0710	430852	149.4	152.4	3.0	BDL	0.05
BS0710	430853	152.4	155.4	3.0	BDL	0.05
BS0710	430854	155.4	158.5	3.1	BDL	0.05
BS0710	430855	158.5	161.5	3.0	BDL	0.05
BS0710	430856	161.5	164.6	3.1	0.1	0.10
BS0710	430857	164.6	167.6	3.0	BDL	0.05
BS0710	430859	167.6	170.7	3.1	BDL	0.05
BS0710	430860	170.7	173.6	2.9	BDL	0.05

BS0710	430861	173.6	175.9	2.3	BDL	0.05
BS0710	430862	175.9	176.8	0.9	0.2	0.15
BS0710	430863	176.8	179.8	3.0	BDL	0.05
BS0710	430864	179.8	182.9	3.1	BDL	0.05
BS0710	430865	182.9	185.9	3.0	BDL	0.05
BS0710	430866	185.9	188.9	3.0	BDL	0.05
BS0710	430867	188.9	192	3.1	BDL	0.05
BS0710	430868	192	195.1	3.1	BDL	0.05
BS0710	430869	195.1	198.1	3.0	BDL	0.05
BS0710	430870	198.1	201.2	3.1	BDL	0.05
BS0710	430871	201.2	204.2	3.0	BDL	0.05
BS0710	430872	204.2	207.3	3.1	BDL	0.05
BS0710	430873	207.3	210.3	3.0	BDL	0.05
BS0710	430874	210.3	213.4	3.1	BDL	0.05
BS0710	430876	213.4	216.4	3.0	BDL	0.05
BS0710	430877	216.4	219.5	3.1	BDL	0.05
BS0710	430878	219.5	222.5	3.0	BDL	0.05
BS0710	430879	222.5	225.6	3.1	BDL	0.05
BS0710	430880	225.6	228.6	3.0	BDL	0.05
BS0710	430881	228.6	231.6	3.0	BDL	0.05
BS0710	430882	231.6	234.7	3.1	BDL	0.05
BS0710	430883	234.7	237.7	3.0	BDL	0.05
BS0710	430884	237.7	240.1	2.4	BDL	0.05
BS0710	430885	240.1	242.2	2.1	0.1	0.10
BS0710	430886	242.2	243.8	1.6	BDL	0.05
BS0710	430887	243.8	246.9	3.1	BDL	0.05
BS0710	430888	246.9	249.9	3.0	BDL	0.05
BS0710	430889	249.9	253	3.1	BDL	0.05
BS0710	430890	253	256	3.0	BDL	0.05
BS0710	430891	256	259.1	3.1	BDL	0.05
BS0710	430892	259.1	262.1	3.0	0.1	0.10
BS0710	430893	262.1	265.2	3.1	0.1	0.10
BS0710	430894	265.2	268.2	3.0	BDL	0.05
BS0710	430895	268.2	271.3	3.1	BDL	0.05
BS0710	430897	271.3	274.3	3.0	BDL	0.05
BS0710	430898	274.3	277.4	3.1	BDL	0.05
BS0710	430899	277.4	280.4	3.0	BDL	0.05
BS0710	430900	280.4	283.5	3.1	BDL	0.05
BS0710	430901	283.5	286.5	3.0	BDL	0.05
BS0710	430902	286.5	289.6	3.1	BDL	0.05
BS0710	430903	289.6	292.6	3.0	BDL	0.05
BS0710	430904	292.6	295.7	3.1	BDL	0.05
BS0710	430905	295.7	298.7	3.0	BDL	0.05
BS0710	430906	298.7	301.8	3.1	BDL	0.05
BS0710	430907	301.8	304.8	3.0	BDL	0.05
BS0710	430908	304.8	307.8	3.0	BDL	0.05

BS0710	430909	307.8	310.9	3.1	BDL	0.05
BS0710	430910	310.9	313.9	3.0	BDL	0.05
BS0710	430911	313.9	317	3.1	BDL	0.05
BS0710	430912	317	320	3.0	BDL	0.05
BS0710	430913	320	323.1	3.1	BDL	0.05
BS0710	430914	323.1	326.1	3.0	BDL	0.05
BS0710	430916	326.1	329.2	3.1	BDL	0.05
BS0710	430917	329.2	332.2	3.0	BDL	0.05
BS0710	430918	332.2	335.3	3.1	BDL	0.05
BS0710	430919	335.3	338.3	3.0	0.1	0.10
BS0710	430920	338.3	341.4	3.1	BDL	0.05
BS0710	430921	341.4	344.4	3.0	BDL	0.05
BS0710	430922	344.4	347.4	3.0	BDL	0.05
BS0710	430923	347.4	350.5	3.1	BDL	0.05
BS0710	430924	350.5	353.6	3.1	BDL	0.05
BS0710	430925	353.6	356.6	3.0	BDL	0.05
BS0710	430926	356.6	359.7	3.1	BDL	0.05
BS0710	430927	359.7	362.7	3.0	BDL	0.05
BS0710	430928	362.7	365.8	3.1	8.4	8.45
BS0701	430277	216.4	219.5	3.1	BDL	0.05
BS0701	430278	219.5	222.5	3.0	BDL	0.05
BS0701	430279	222.5	225.6	3.1	BDL	0.05
BS0701	430280	225.6	228.6	3.0	BDL	0.05
BS0701	430281	228.6	231.6	3.0	BDL	0.05
BS0701	430282	231.6	234.7	3.1	BDL	0.05
BS0701	430283	234.7	237.7	3.0	0.3	0.30
BS0701	430284	237.7	240.8	3.1	BDL	0.05
BS0701	430285	240.8	243.8	3.0	BDL	0.05
BS0701	430286	243.8	246.9	3.1	BDL	0.05
BS0701	430287	246.9	250	3.1	BDL	0.05
BS0701	430288	250	252.9	2.9	BDL	0.05
BS0701	430289	252.9	256	3.1	BDL	0.05
BS0701	430291	256	259.1	3.1	BDL	0.05
BS0701	430292	259.1	262.1	3.0	BDL	0.05
BS0701	430293	262.1	265.2	3.1	BDL	0.05
BS0701	430294	265.2	268.2	3.0	BDL	0.05
BS0701	430295	268.2	271.3	3.1	BDL	0.05
BS0701	430296	271.3	274.3	3.0	BDL	0.05
BS0701	430297	274.3	277.4	3.1	BDL	0.05
BS0701	430298	277.4	280.4	3.0	BDL	0.05
BS0701	430299	280.4	283.5	3.1	BDL	0.05
BS0701	430300	283.5	286.5	3.0	BDL	0.05
BS0701	430301	286.5	289.6	3.1	BDL	0.05
BS0701	430302	289.6	292.6	3.0	0.1	0.10
BS0701	430303	292.6	295.7	3.1	0.1	0.10
BS0701	430304	295.7	298.7	3.0	0.1	0.10

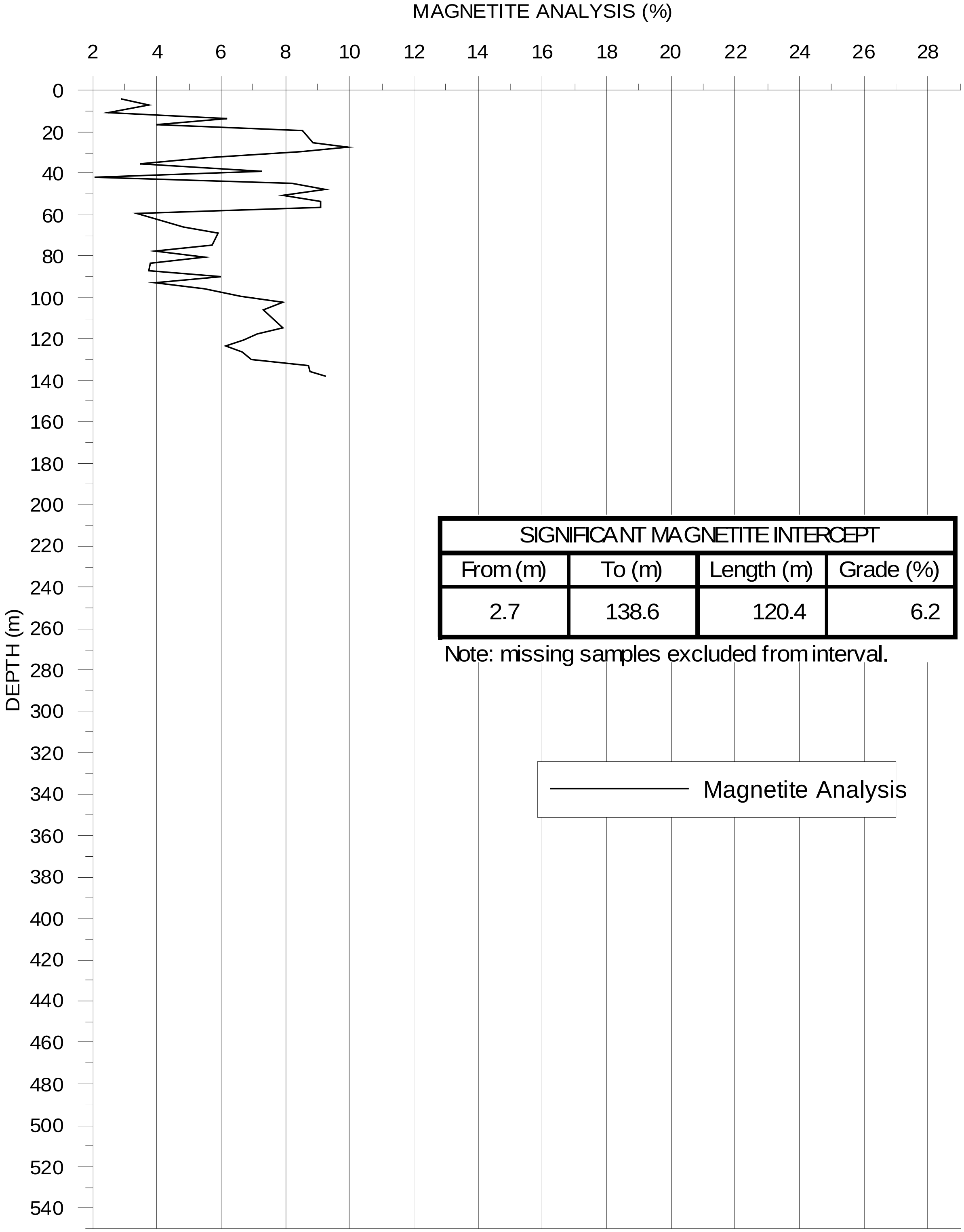
BS0701	430305	298.7	301.7	3.0	BDL	0.05
BS0701	430306	301.7	304.8	3.1	BDL	0.05
BS0701	430307	304.8	307.8	3.0	BDL	0.05
BS0701	430308	307.8	310.8	3.0	BDL	0.05
BS0701	430310	310.8	313.9	3.1	BDL	0.05
BS0701	430311	313.9	317	3.1	BDL	0.05
BS0701	430312	317	320	3.0	BDL	0.05
BS0701	430313	320	323	3.0	BDL	0.05
BS0701	430314	323	326.1	3.1	BDL	0.05
BS0701	430315	326.1	329.2	3.1	BDL	0.05
BS0701	430316	329.2	331.2	2.0	BDL	0.05
BS0701	430317	331.2	335.2	4.0	BDL	0.05
BS0701	430318	335.2	338.3	3.1	BDL	0.05
BS0701	430319	338.3	341.3	3.0	BDL	0.05
BS0701	430320	341.3	344.4	3.1	0.2	0.15
BS0701	430321	344.4	347.4	3.0	BDL	0.05
BS0701	430322	347.4	350.5	3.1	BDL	0.05
BS0701	430323	350.5	353	2.5	BDL	0.05
BS0701	430324	353	356.6	3.6	BDL	0.05
BS0701	430325	356.6	359.6	3.0	BDL	0.05
BS0701	430326	359.6	362.7	3.1	0.1	0.10
BS0701	430327	362.7	365.7	3.0	BDL	0.05
BS0701	430328	365.7	368.7	3.0	BDL	0.05
BS0701	430329	368.7	371.8	3.1	BDL	0.05
BS0701	430330	371.8	374.9	3.1	BDL	0.05
BS0701	430332	374.9	377.9	3.0	BDL	0.05
BS0701	430333	377.9	381	3.1	BDL	0.05
BS0701	430334	381	384	3.0	BDL	0.05
BS0701	430335	384	387.1	3.1	BDL	0.05
BS0701	430336	387.1	390.1	3.0	BDL	0.05
BS0701	430337	390.1	393.2	3.1	0.1	0.10
BS0701	430338	393.2	396.2	3.0	0.2	0.15
BS0701	430339	396.2	399.3	3.1	0.1	0.10
BS0701	430340	399.3	402.3	3.0	3.7	3.65
BS0701	430341	402.3	405.4	3.1	BDL	0.05
BS0701	430342	405.4	408.4	3.0	BDL	0.05
BS0701	430343	408.4	411.5	3.1	BDL	0.05
BS0701	430344	411.5	414.5	3.0	BDL	0.05
BS0701	430345	414.5	417.6	3.1	BDL	0.05
BS0701	430346	417.6	420.6	3.0	BDL	0.05
BS0701	430347	420.6	423.7	3.1	BDL	0.05
BS0701	430349	423.7	426.7	3.0	BDL	0.05
BS0701	430350	426.7	429.8	3.1	BDL	0.05
BS0701	430351	429.8	432.8	3.0	BDL	0.05
BS0701	430352	432.8	435.9	3.1	BDL	0.05
BS0701	430353	435.9	438.9	3.0	BDL	0.05

BS0701	430354	438.9	442	3.1	BDL	0.05	
BS0701	430355	442	445	3.0	BDL	0.05	
BS0701	430356	445	448.1	3.1	BDL	0.05	
BS0701	430357	448.1	451.1	3.0	BDL	0.05	
BS0701	430358	451.1	454.2	3.1	BDL	0.05	
BS0701	430359	454.2	457.2	3.0	BDL	0.05	
BS0701	430360	457.2	460.2	3.0	BDL	0.05	
BS0701	430361	460.2	463.3	3.1	BDL	0.05	
BS0701	430362	463.3	466.3	3.0	BDL	0.05	
200602	430011	2.7	5.7	3	2.9	2.90	
200602	430012	5.7	8.7	3	3.8	3.75	
200602	430013	8.7	11.7	3	2.5	2.50	
200602	430014	11.7	14.7	3	6.2	6.20	
200602	430015	14.7	17.7	3	4.0	4.00	
200602	430016	17.7	20.7	3	8.6	8.55	
200602	430017	20.7	23.7	3			SAMPLE MISSING
200602	430018	23.7	26.7	3	8.8	8.85	
200602	430019	26.7	27.6	0.9	10.0	9.95	
200602	430020	27.6	28.1	0.5			SAMPLE MISSING
200602	430021	28.1	31.1	3	8.5	8.50	
200602	430022	31.1	34.1	3	5.6	5.55	
200602	430023	34.1	37.1	3	3.5	3.45	
200602	430024	37.1	40.1	3	7.2	7.25	
200602	430025	40.1	43.1	3	2.0	2.05	
200602	430026	43.1	46.1	3	8.2	8.20	
200602	430027	46.1	49.1	3	9.2	9.25	
200602	430028	49.1	49.1	0			SAMPLE MISSING
200602	430029	49.1	52.1	3	8.0	7.95	
200602	430030	52.1	55.1	3	9.1	9.10	
200602	430031	55.1	58.1	3	9.1	9.10	
200602	430032	58.1	61.1	3	3.3	3.35	
200602	430033	61.1	64.1	3			SAMPLE MISSING
200602	430034	64.1	67.1	3	4.8	4.85	
200602	430035	67.1	70.1	3	5.9	5.90	
200602	430036	70.1	73.1	3			SAMPLE MISSING
200602	430037	73.1	76.1	3	5.7	5.70	
200602	430038	76.1	79.1	3	3.9	3.95	
200602	430039	79.1	82.1	3	5.5	5.50	
200602	430040	82.1	85.1	3	3.8	3.80	
200602	430041	85.1	88.1	3	3.8	3.75	
200602	430042	88.1	91.1	3	6.0	6.00	
200602	430043	91.1	94.1	3	4.0	3.95	
200602	430044	94.1	97.1	3	5.5	5.50	
200602	430045	97.1	101.1	4	6.6	6.60	
200602	430046	101.1	104.1	3	8.0	7.95	
200602	430047	104.1	107.1	3	7.3	7.30	

200602	430049	107.1	110.1	3			SAMPLE MISSING
200602	430050	110.1	113.1	3			SAMPLE MISSING
200602	430101	113.1	116.1	3	8.3	8.35	
200602	430102	116.1	119.1	3	7.5	7.50	
200602	430103	119.1	122.1	3	5.5	5.55	
200602	430104	122.1	125.1	3	7.0	7.00	
200602	430105	125.1	128.1	3	5.9	5.90	
200602	430106	128.1	131.1	3	7.1	7.10	
200602	430107	131.1	134.1	3	7.8	7.85	
200602	430108	134.1	137.1	3	11.3	11.25	
200602	430109	137.1	138.6	1.5	7.2	7.20	

APPENDIX C

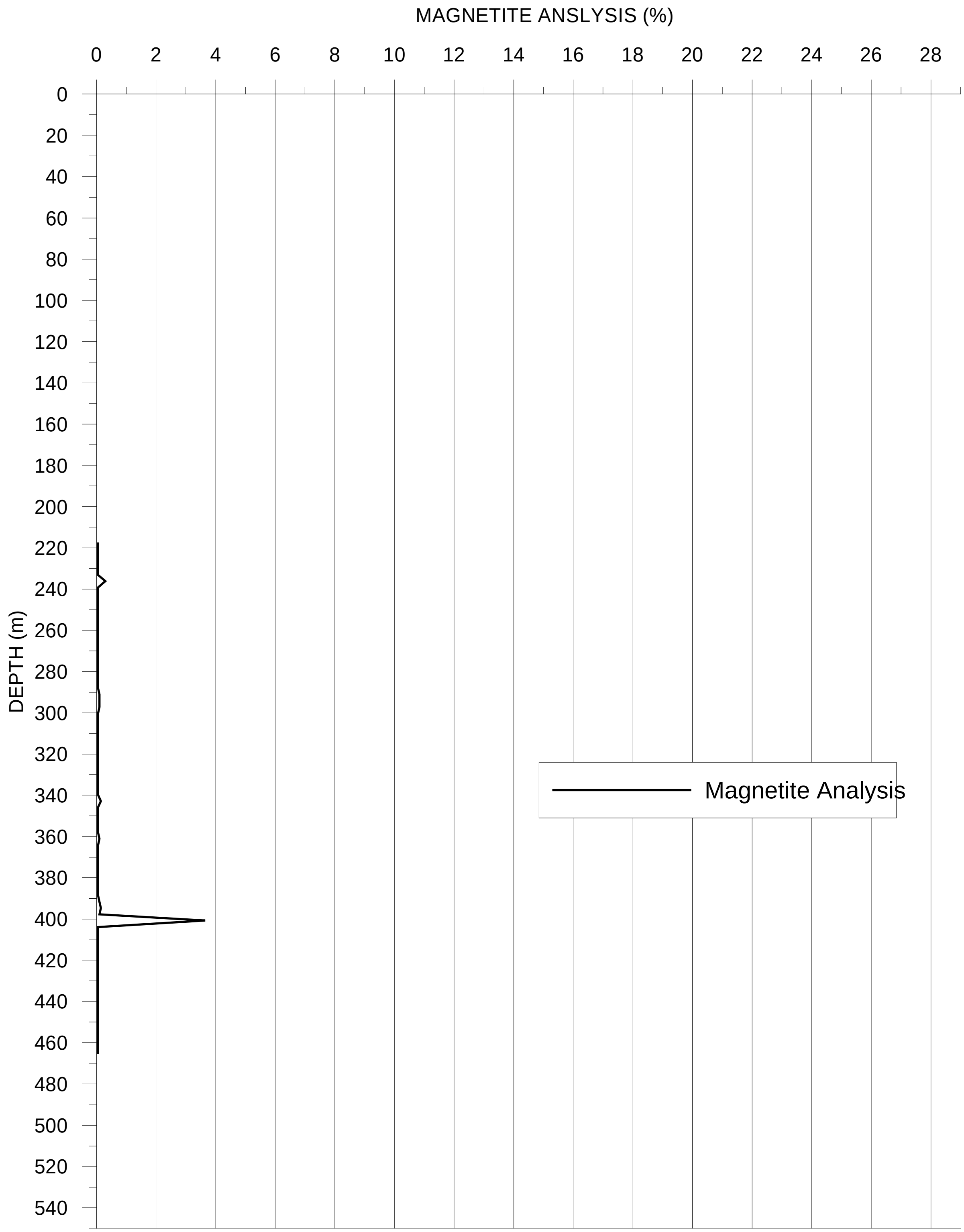
MAGNETITE GRADE VS MAGNETIC SUSCEPTIBILITY PLOTS



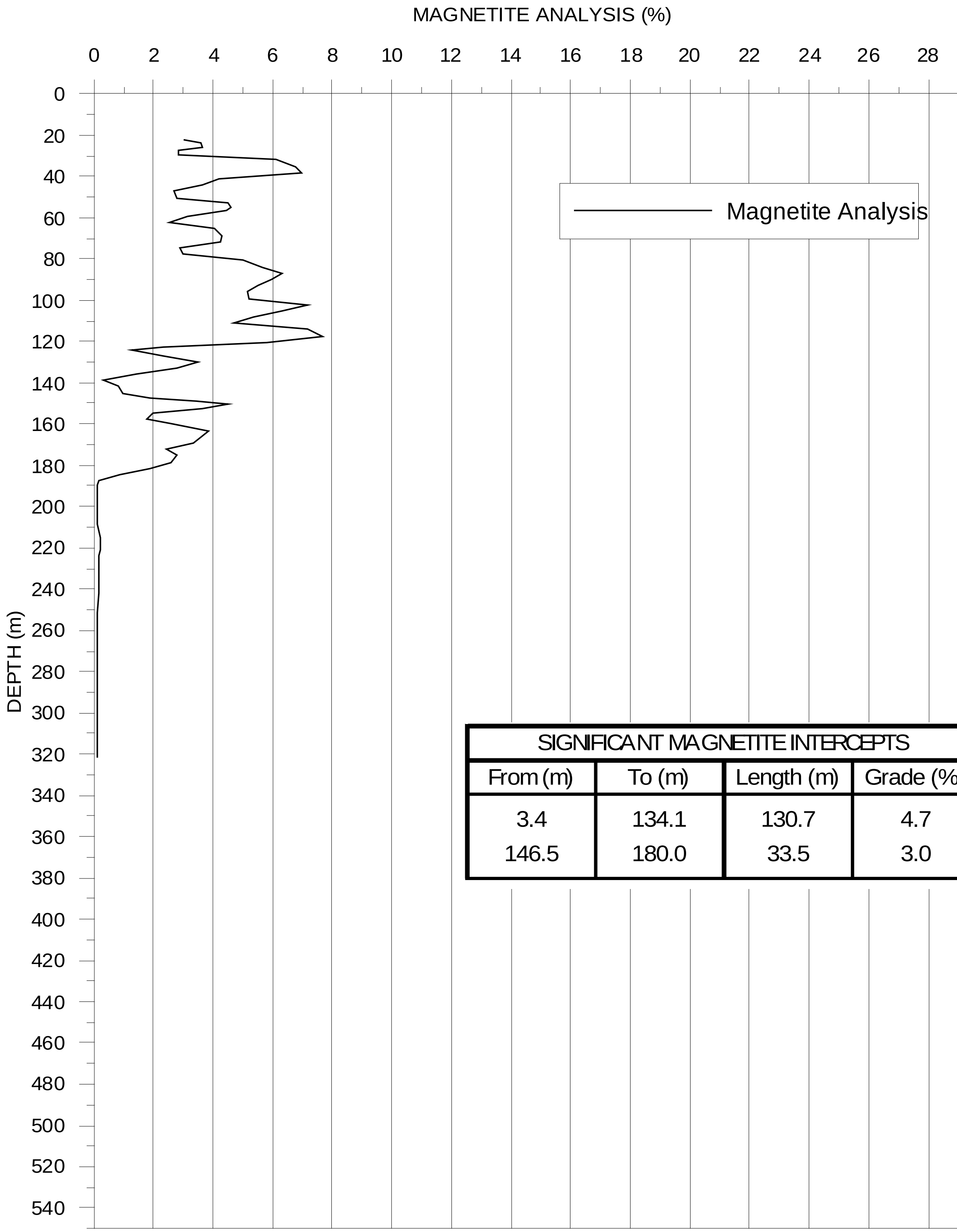
SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
2.7	138.6	120.4	6.2

Note: missing samples excluded from interval.

SKYLINE GOLD CORP.		
MAGNETITE ANALYSIS		
HOLE 0602	OCT 09	AB



SKYLINE GOLD CORP.		
MAGNETITE ANALYSIS		
HOLE 0701	OCT 09	AB

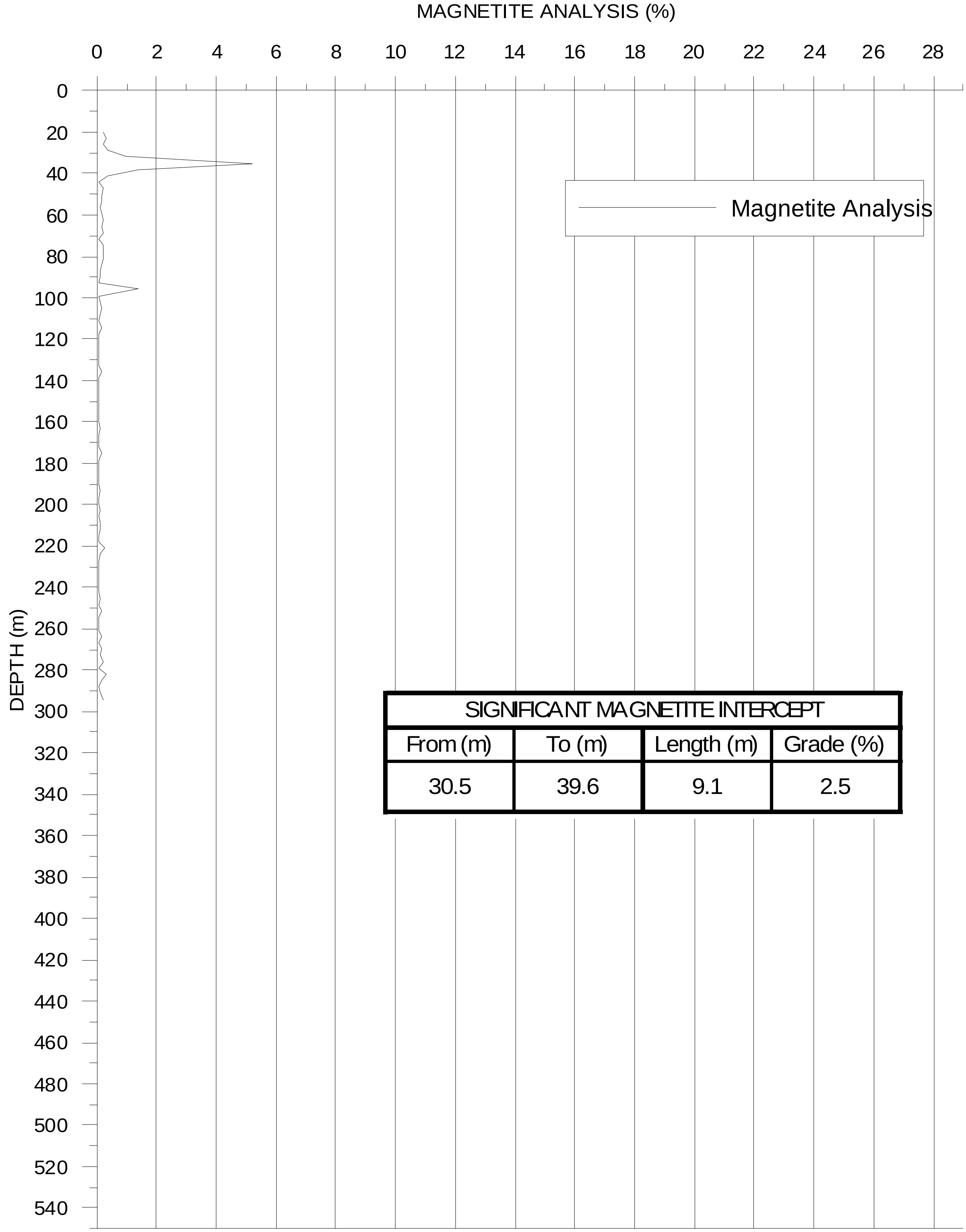


SIGNIFICANT MAGNETITE INTERCEPTS			
From (m)	To (m)	Length (m)	Grade (%)
3.4	134.1	130.7	4.7
146.5	180.0	33.5	3.0

SKYLINE GOLD CORP.

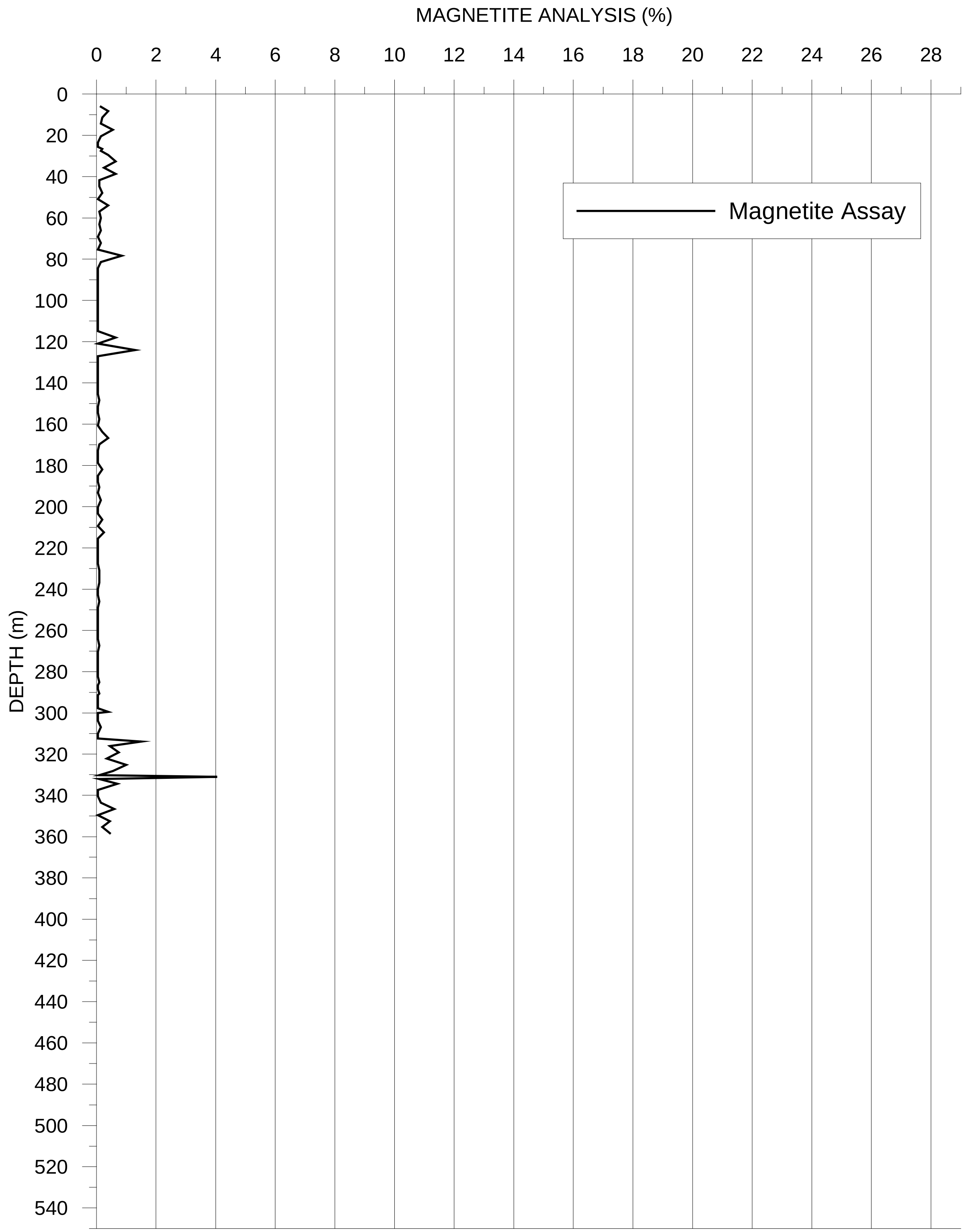
MAGNETITE ANALYSIS

HOLE 0702	OCT 09	AB

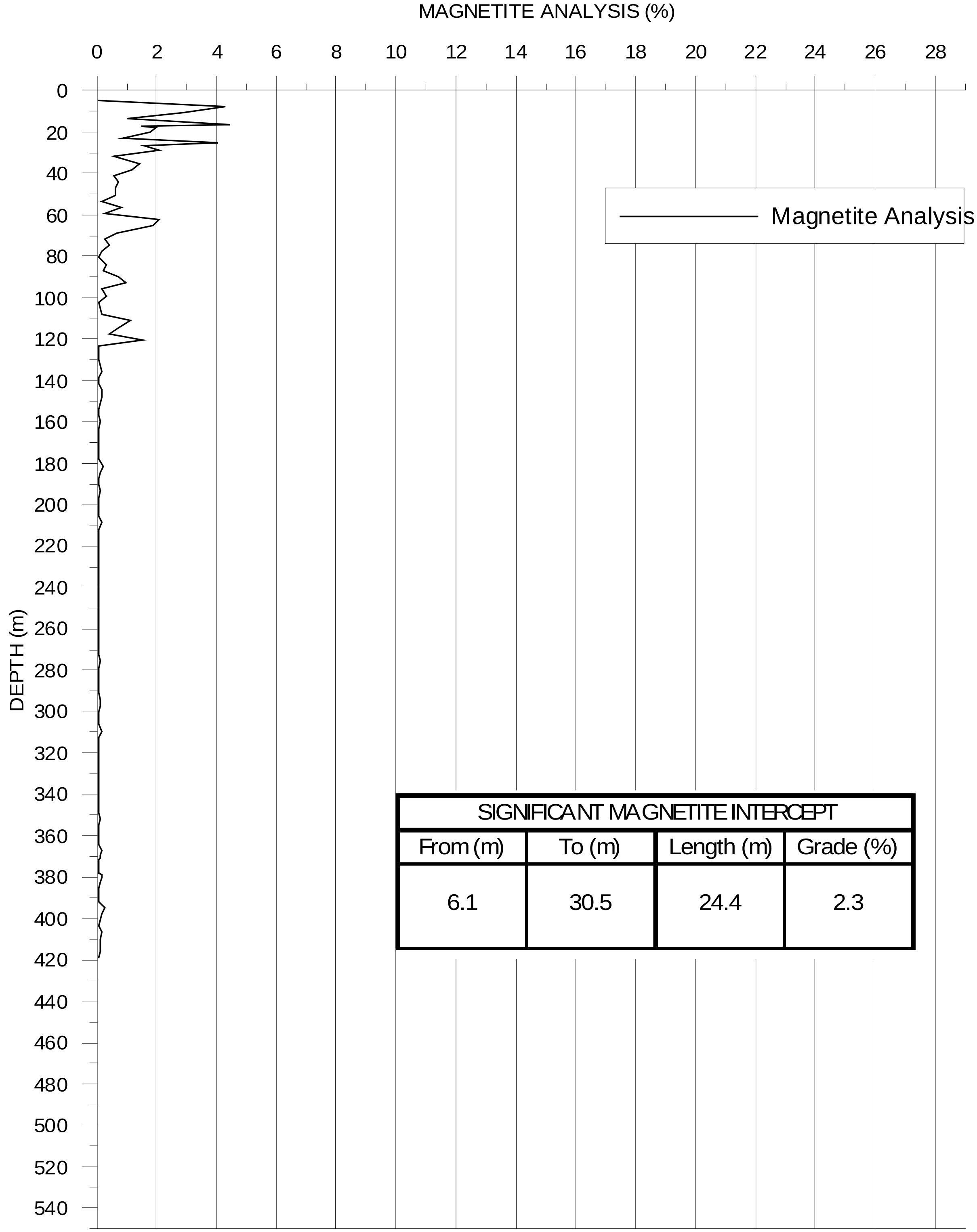


SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
30.5	39.6	9.1	2.5

SKYLINE GOLD CORP.		
MAGNETITE ANALYSIS		
HOLE 0703	NOV 09	AB

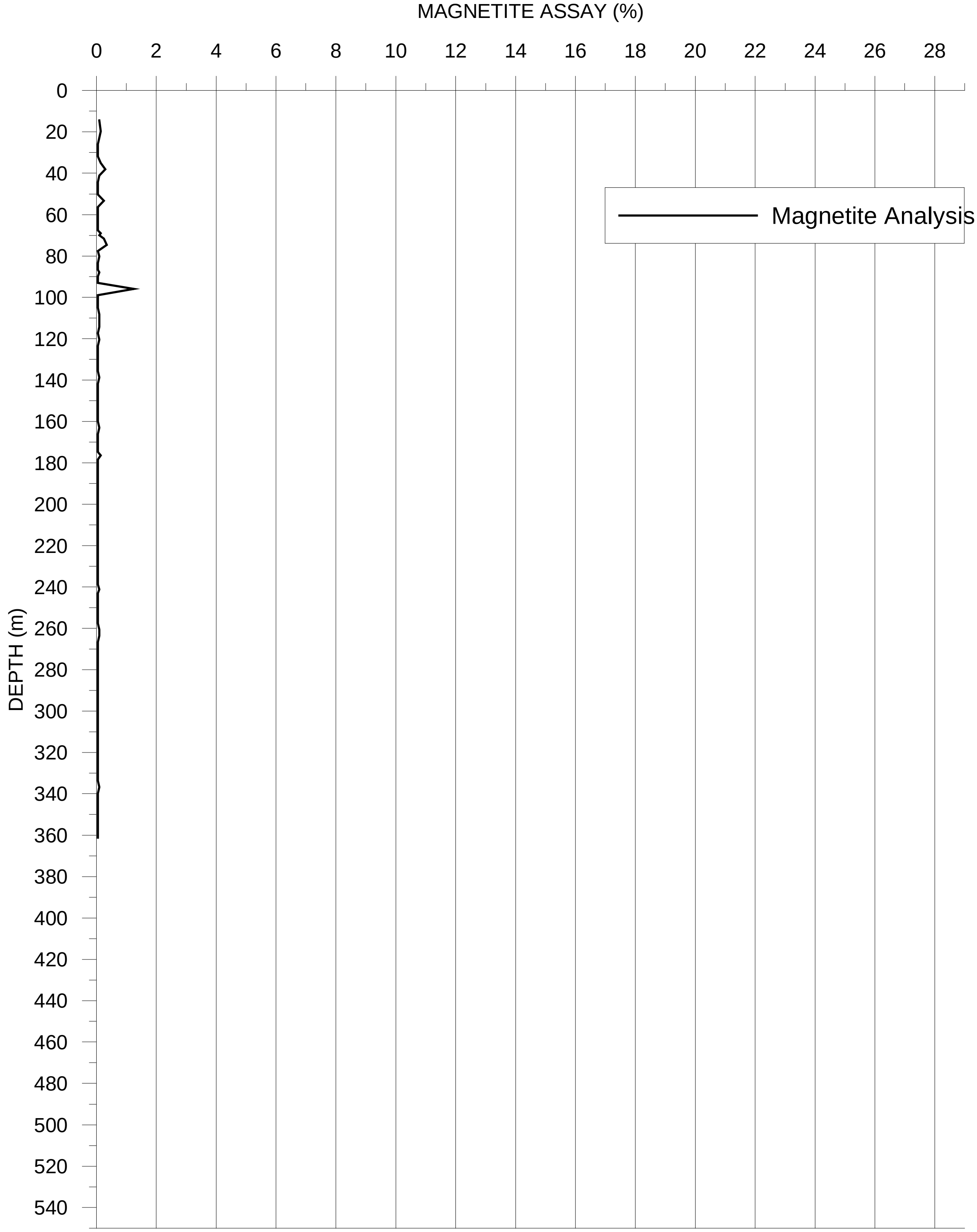


SKYLINE GOLD CORP.		
MAGNETITE ANALYSIS		
HOLE 0704	OCT 09	AB

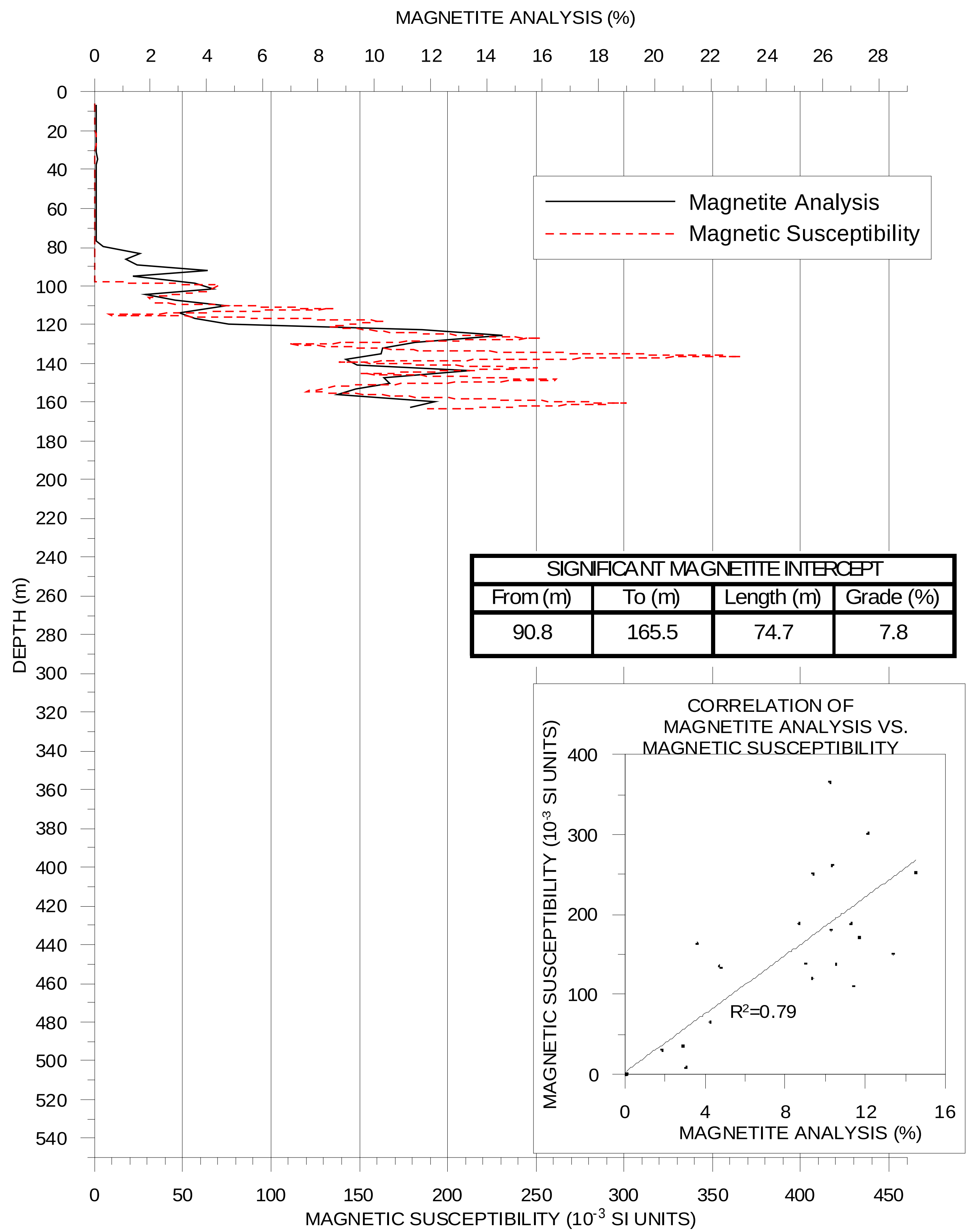


SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
6.1	30.5	24.4	2.3

SKYLINE GOLD CORP.		
MAGNETITE ANALYSIS		
HOLE 0705	OCT 09	AB

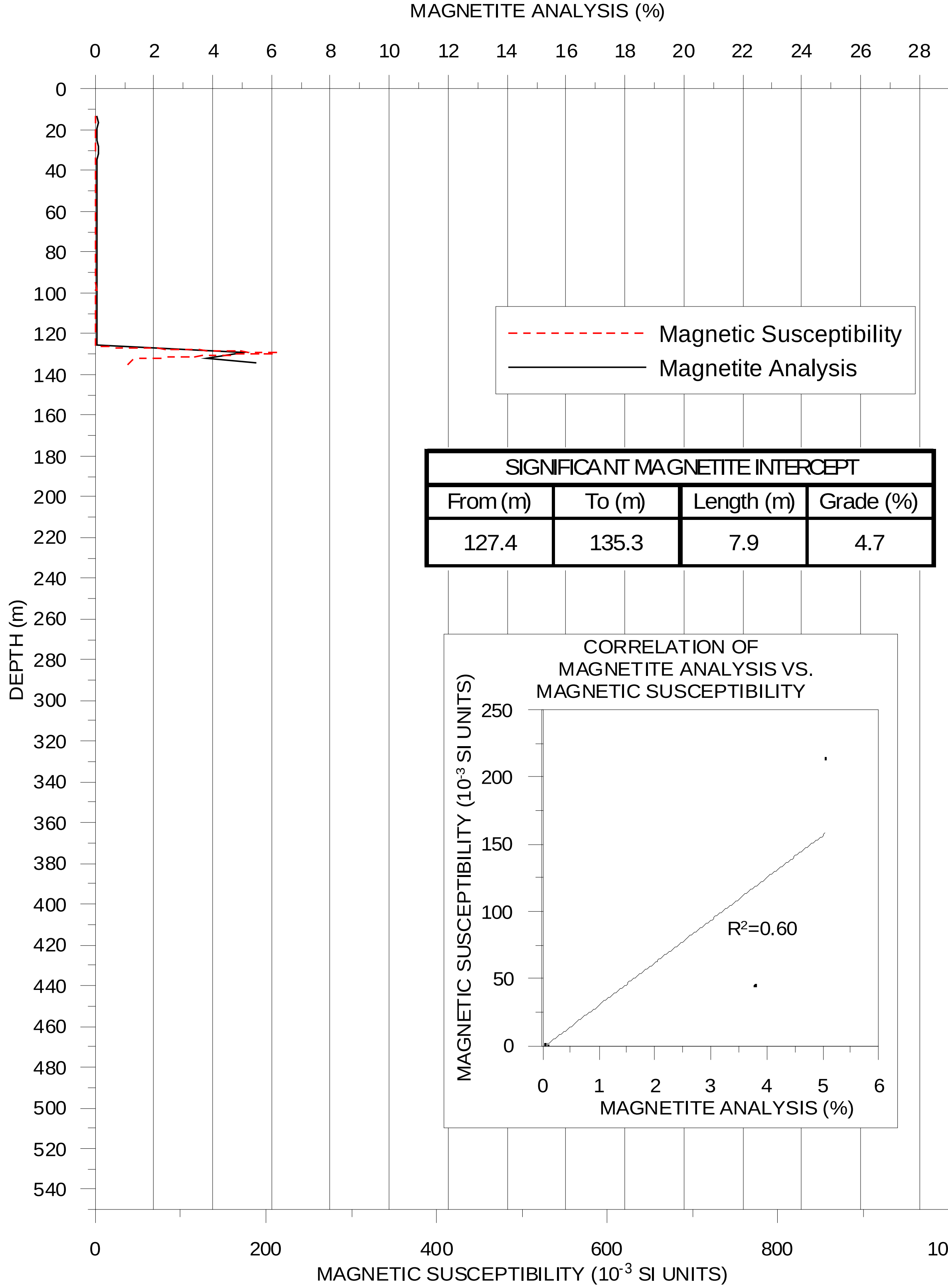


SKYLINE GOLD CORP.		
MAGNETITE ASSAY		
HOLE 0710	OCT 09	AB



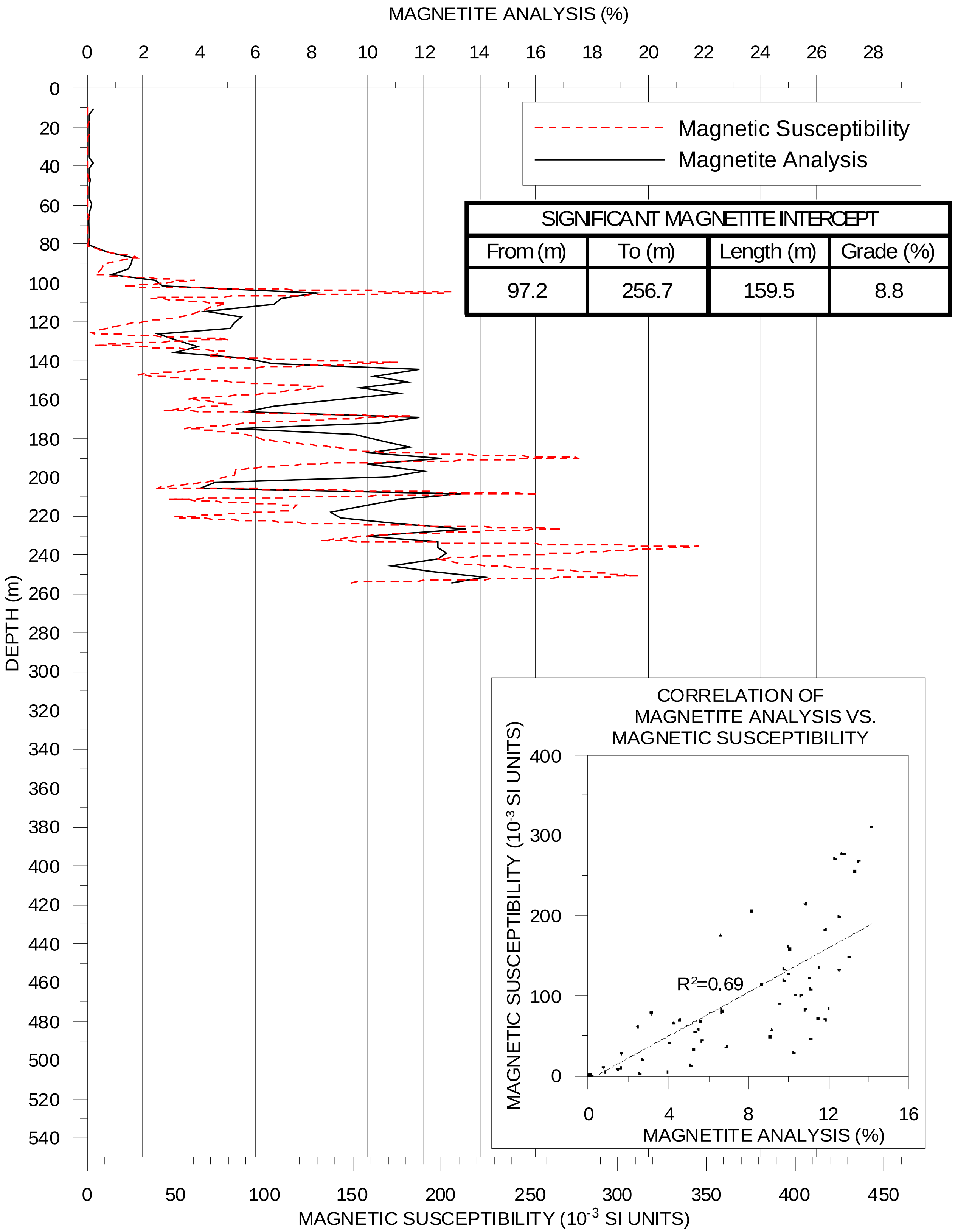
SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
90.8	165.5	74.7	7.8

SKYLINE GOLD CORP.		
MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS		
HOLE 1211	OCT 09	AB



SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
127.4	135.3	7.9	4.7

SKYLINE GOLD CORP.		
MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS		
HOLE 1212	OCT 09	AB

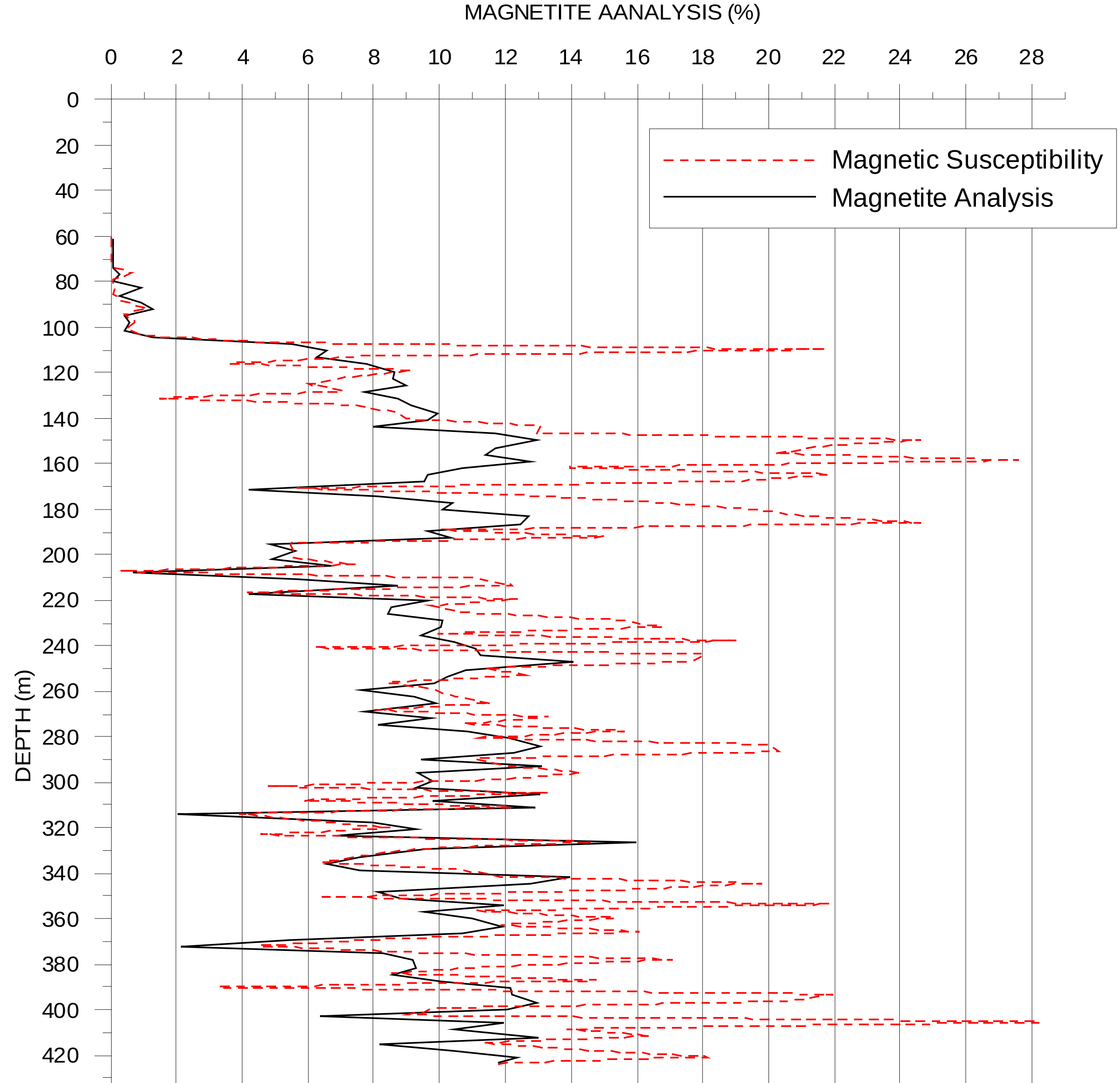


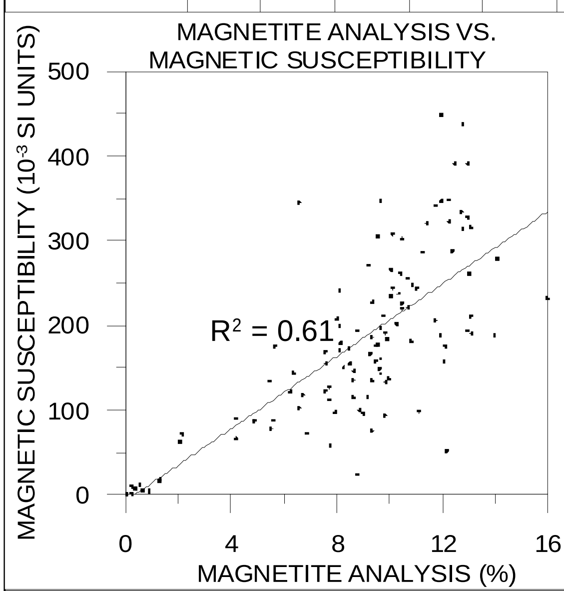
SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
97.2	256.7	159.5	8.8

SKYLINE GOLD CORP.

MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS

HOLE 1216	OCT 09	AB



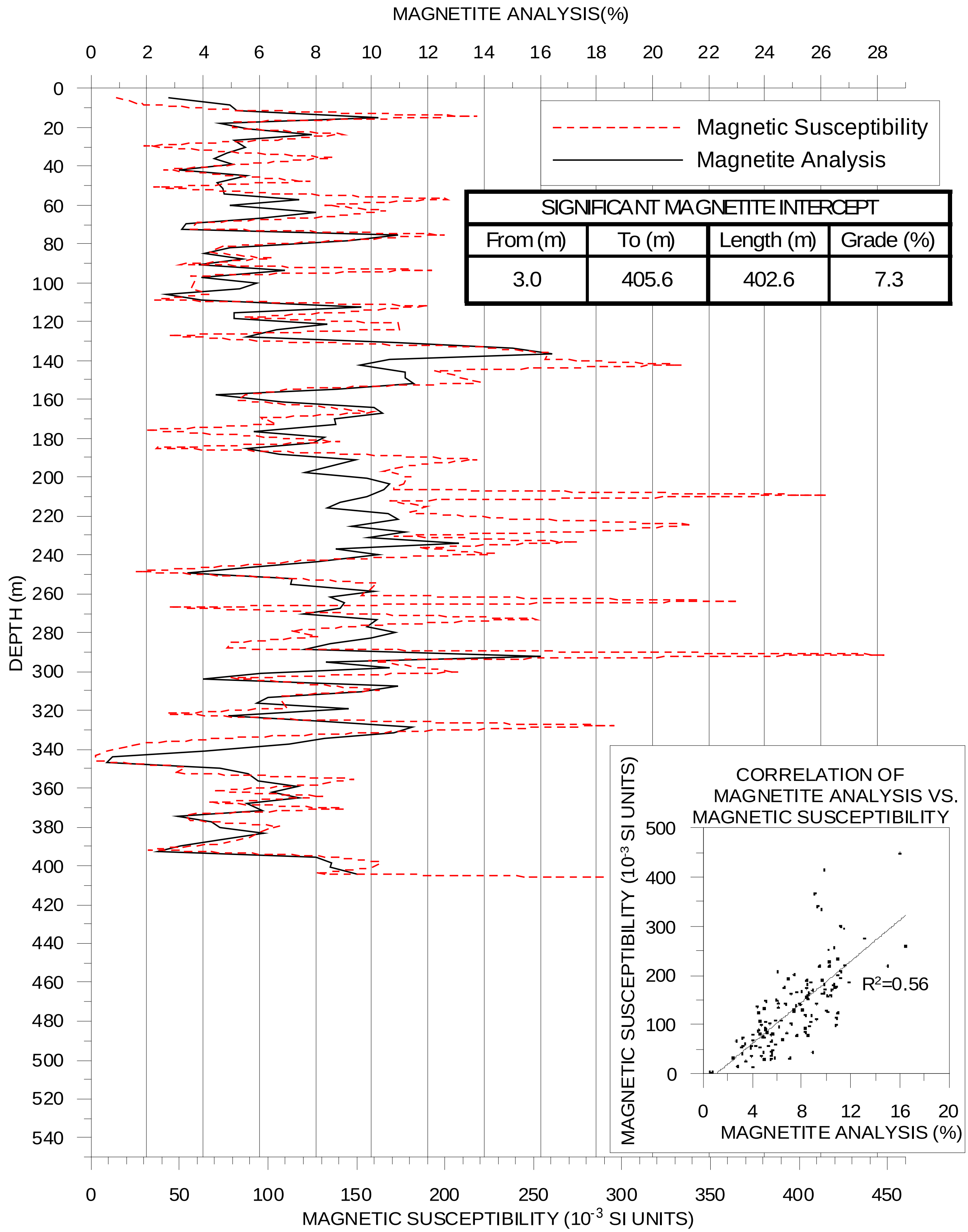


SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
105.7	423.4	317.7	9.5

SKYLINE GOLD CORP.

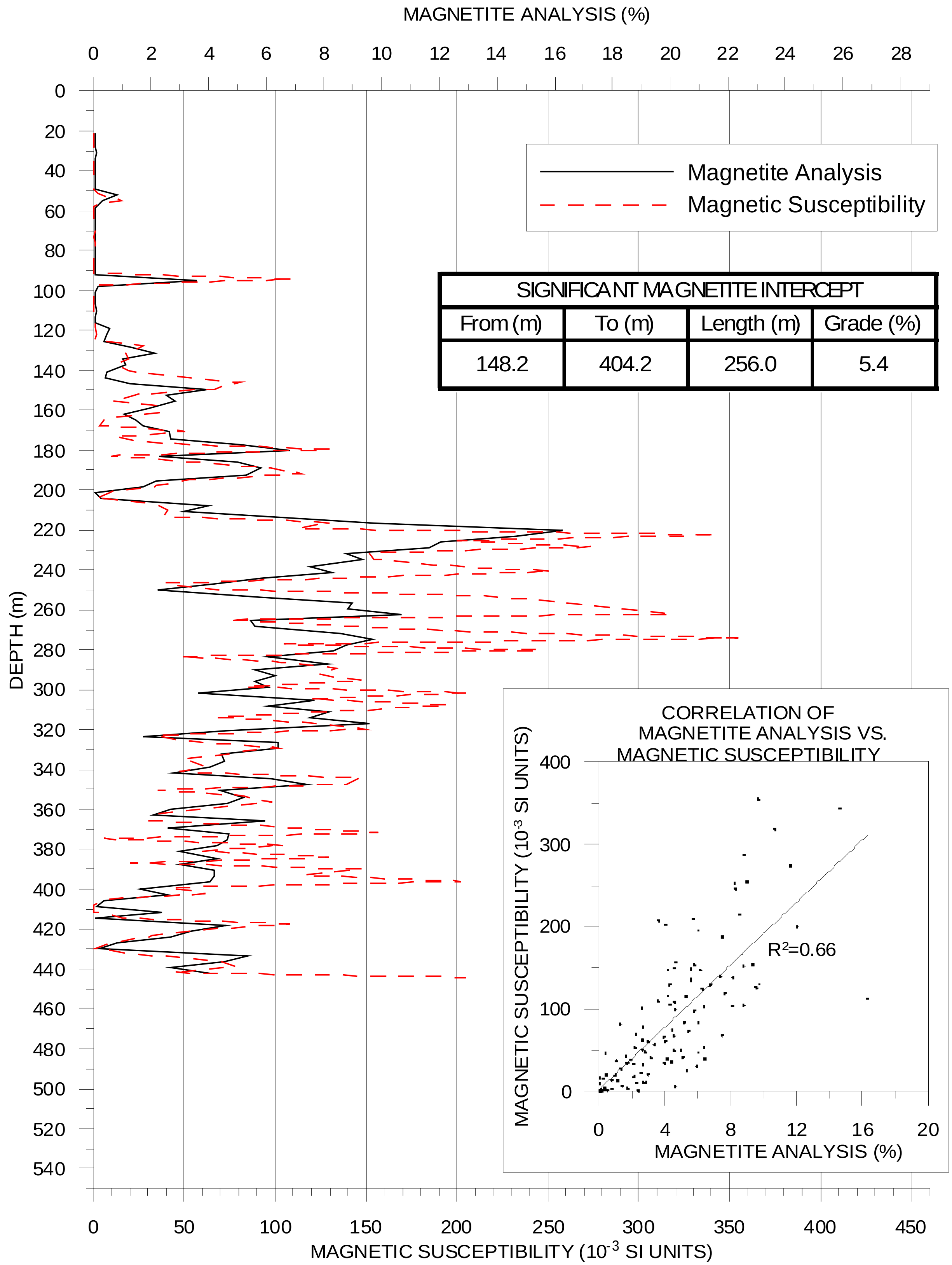
MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS

HOLE 1217	OCT 09	AB



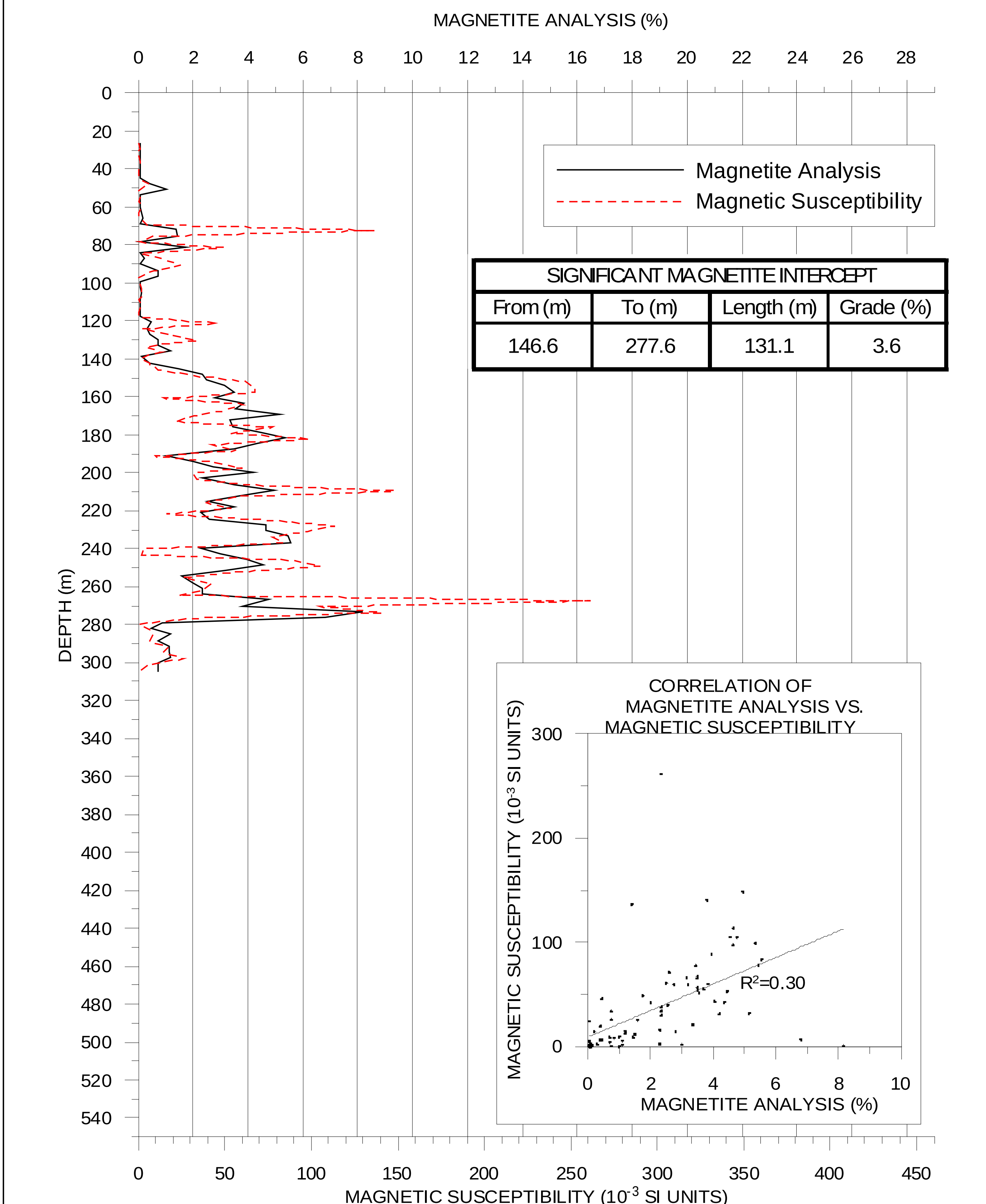
SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
3.0	405.6	402.6	7.3

SKYLINE GOLD CORP.		
MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS		
HOLE 1218	OCT 09	AB



SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
148.2	404.2	256.0	5.4

SKYLINE GOLD CORP.		
MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS		
HOLE 1219	OCT 09	AB

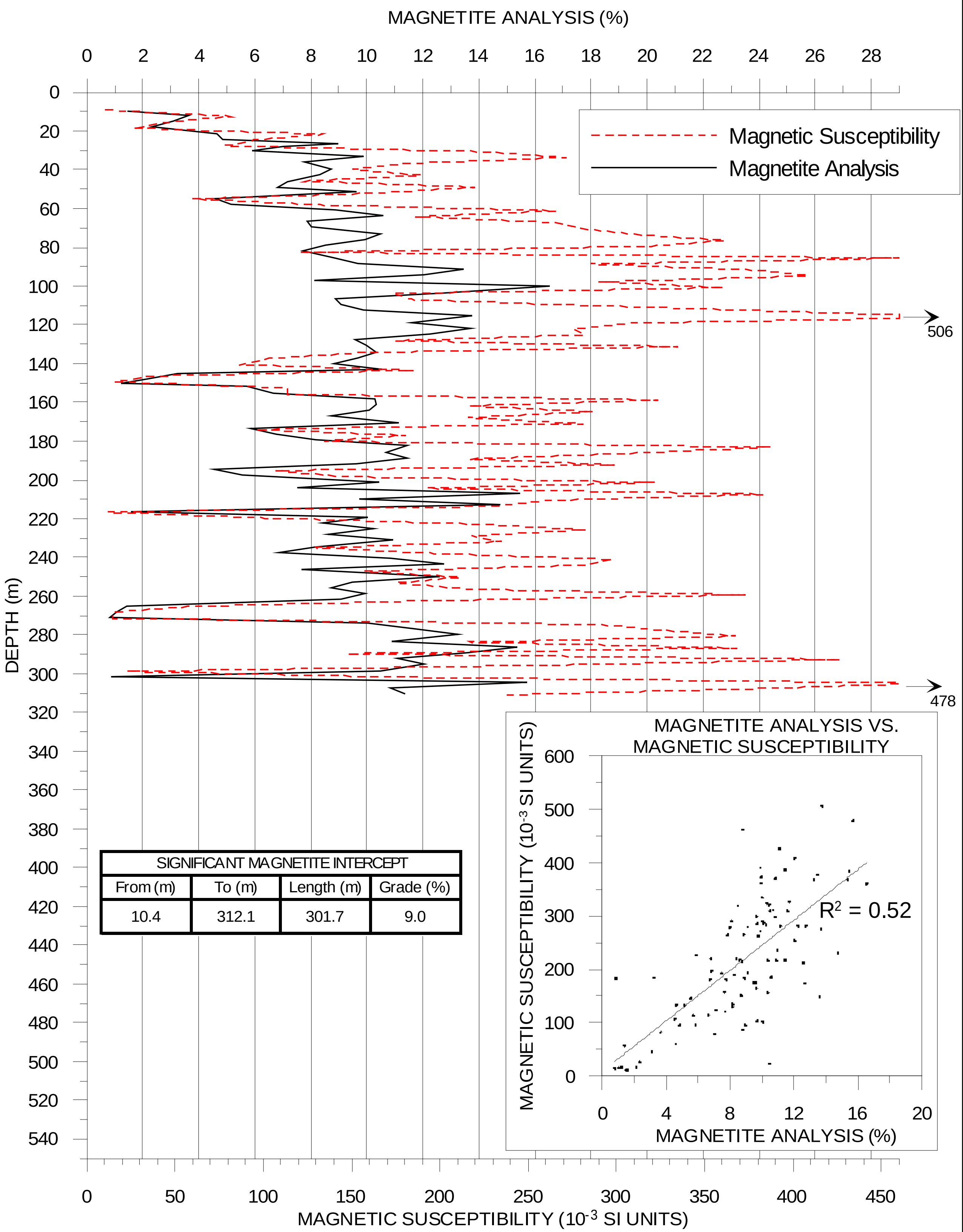


SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
146.6	277.6	131.1	3.6

SKYLINE GOLD CORP.

MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS

HOLE 1220	OCT 09	AB

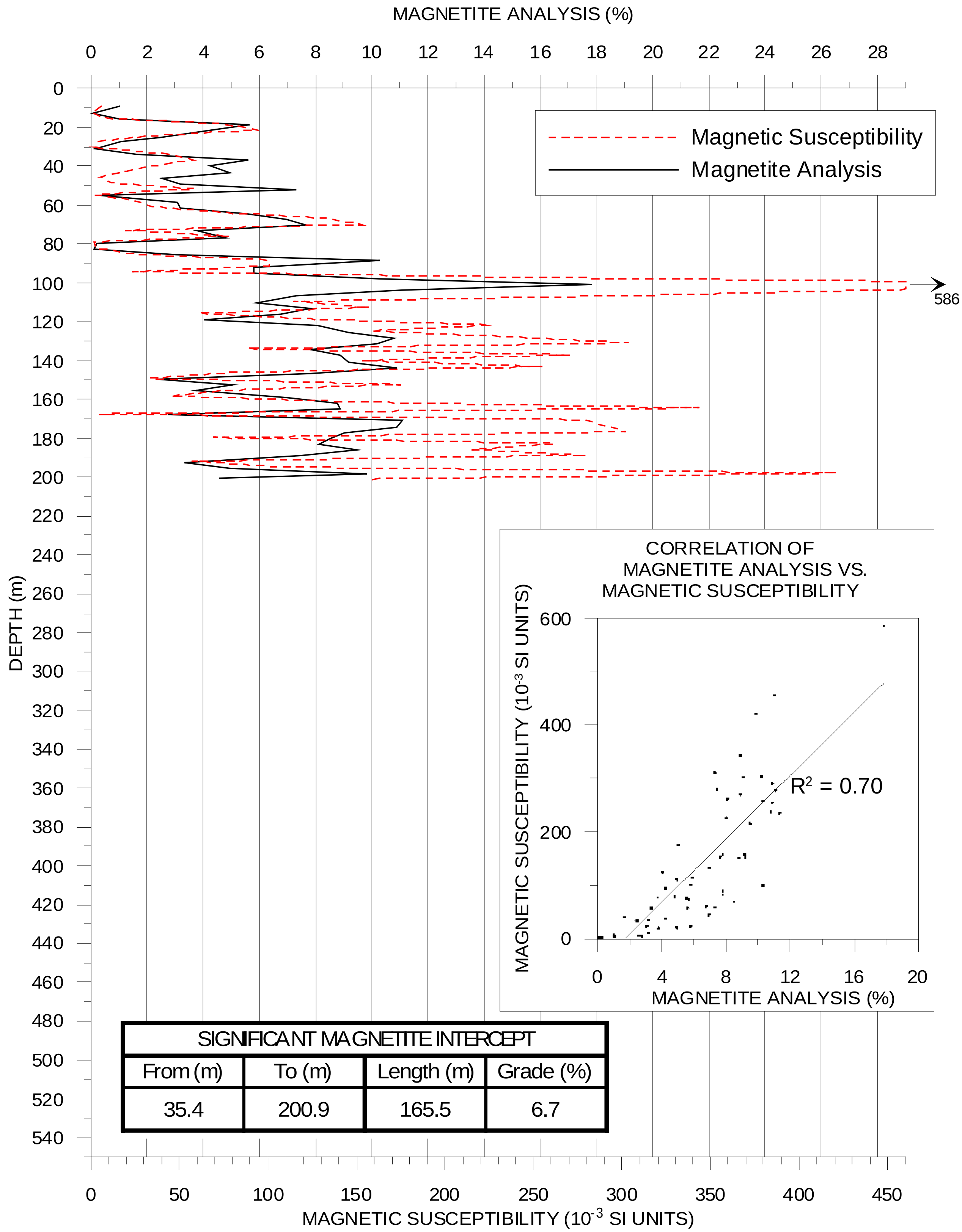


SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
10.4	312.1	301.7	9.0

SKYLINE GOLD CORP.

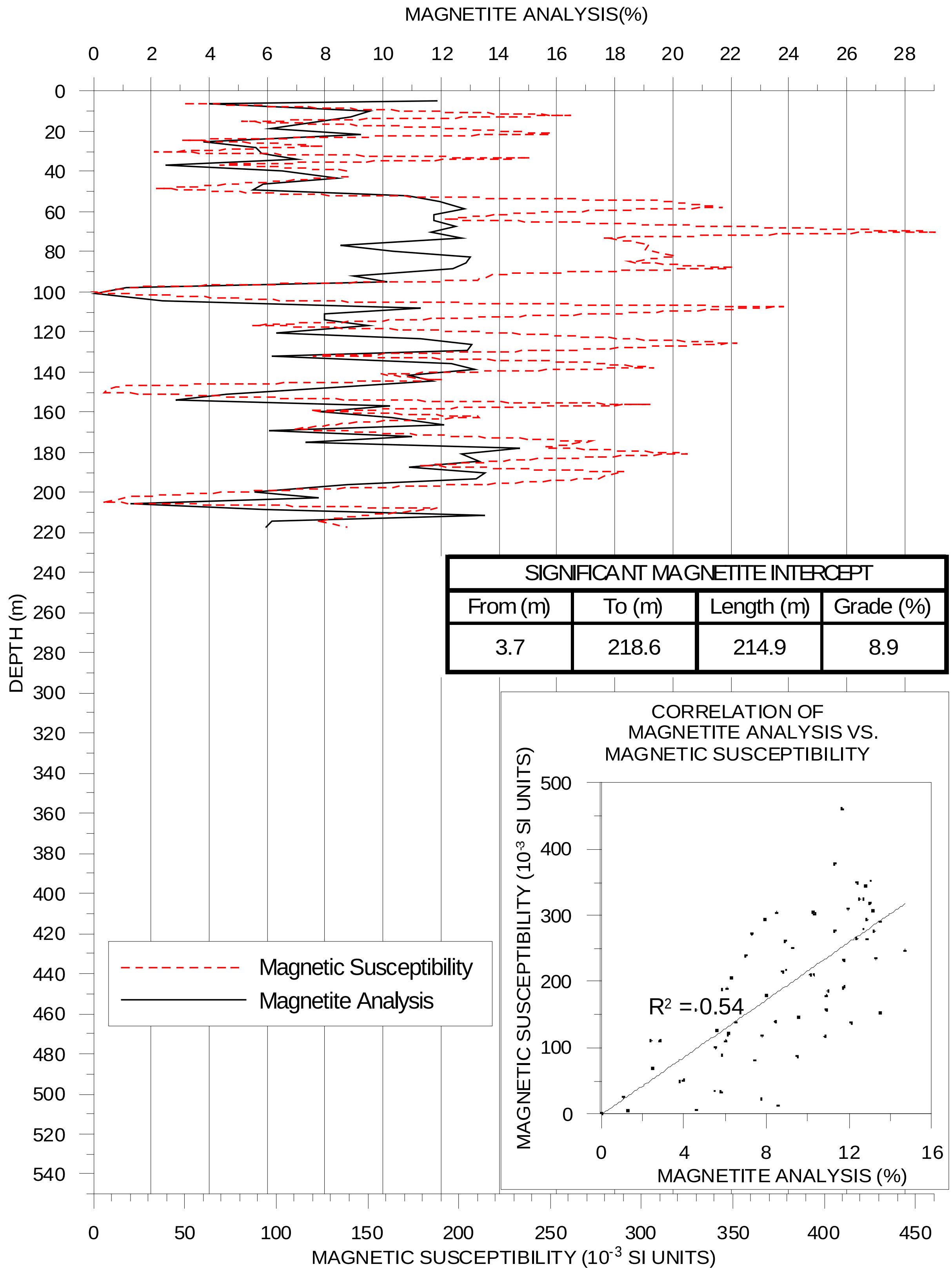
MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS

HOLE 1221	OCT 09	AB



SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
35.4	200.9	165.5	6.7

SKYLINE GOLD CORP.		
MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS		
HOLE 1223	OCT 09	AB

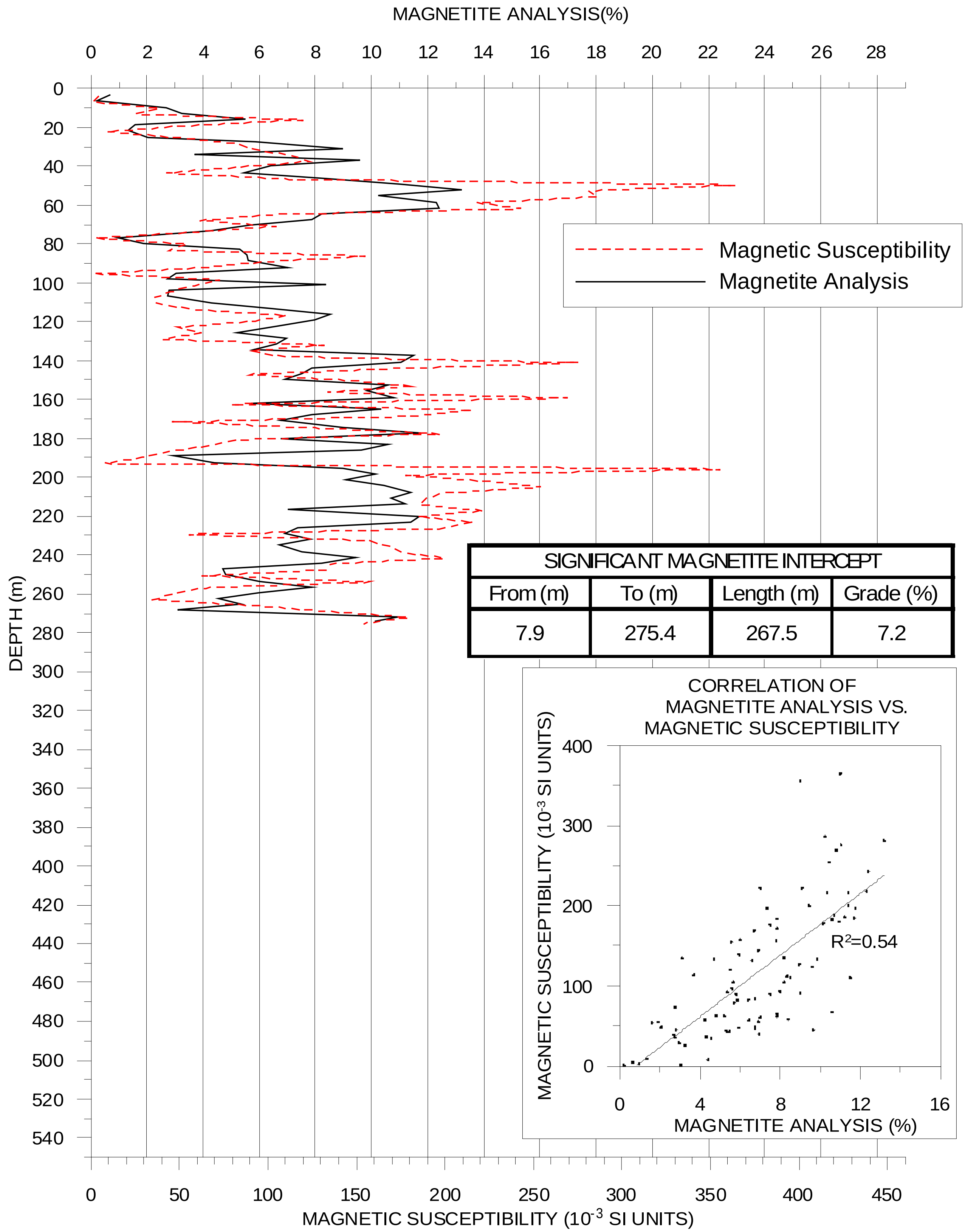


SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
3.7	218.6	214.9	8.9

SKYLINE GOLD CORP.

MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS

HOLE 1225	OCT 09	AB

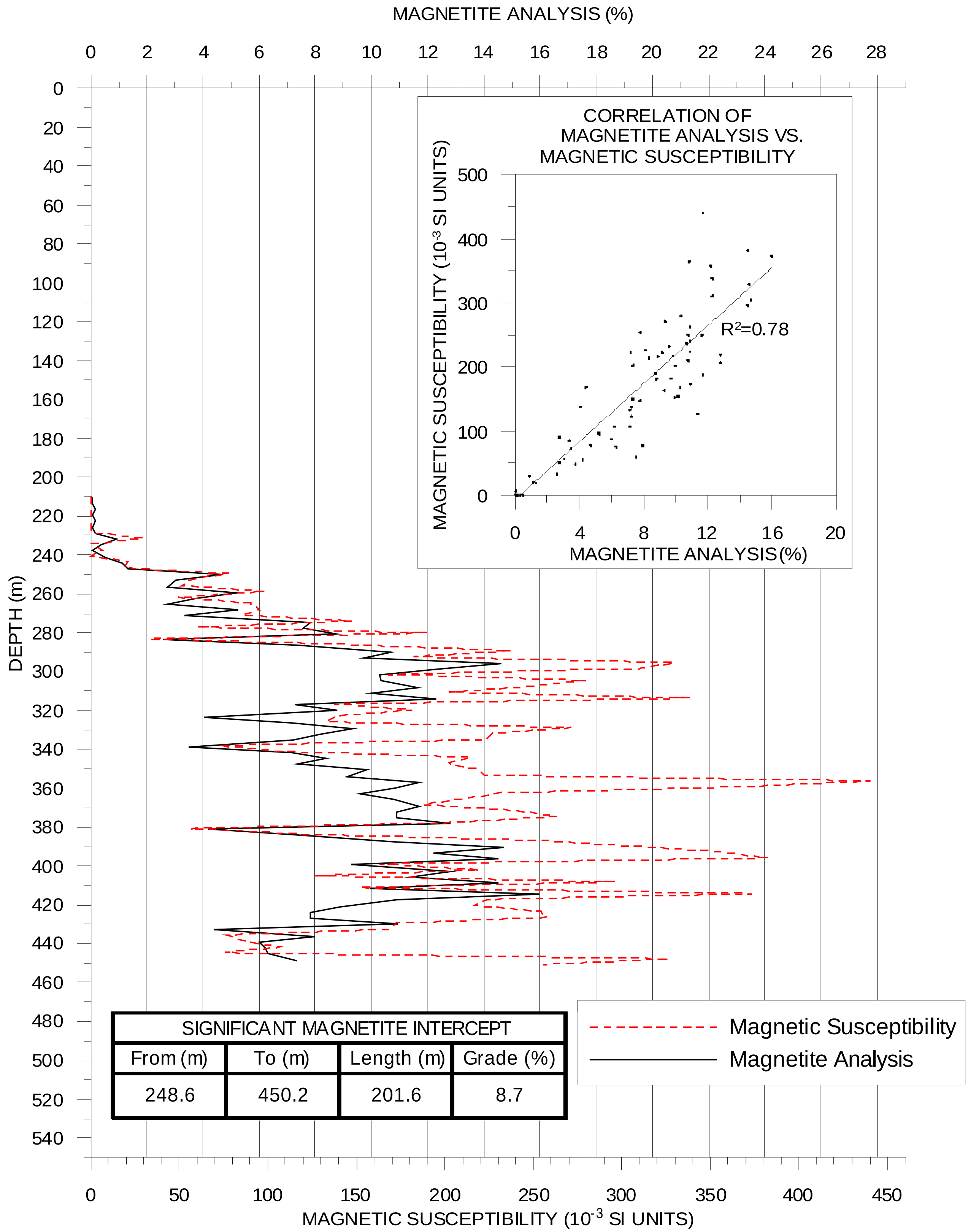


SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
7.9	275.4	267.5	7.2

SKYLINE GOLD CORP.

MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS

HOLE 1226	OCT 09	AB

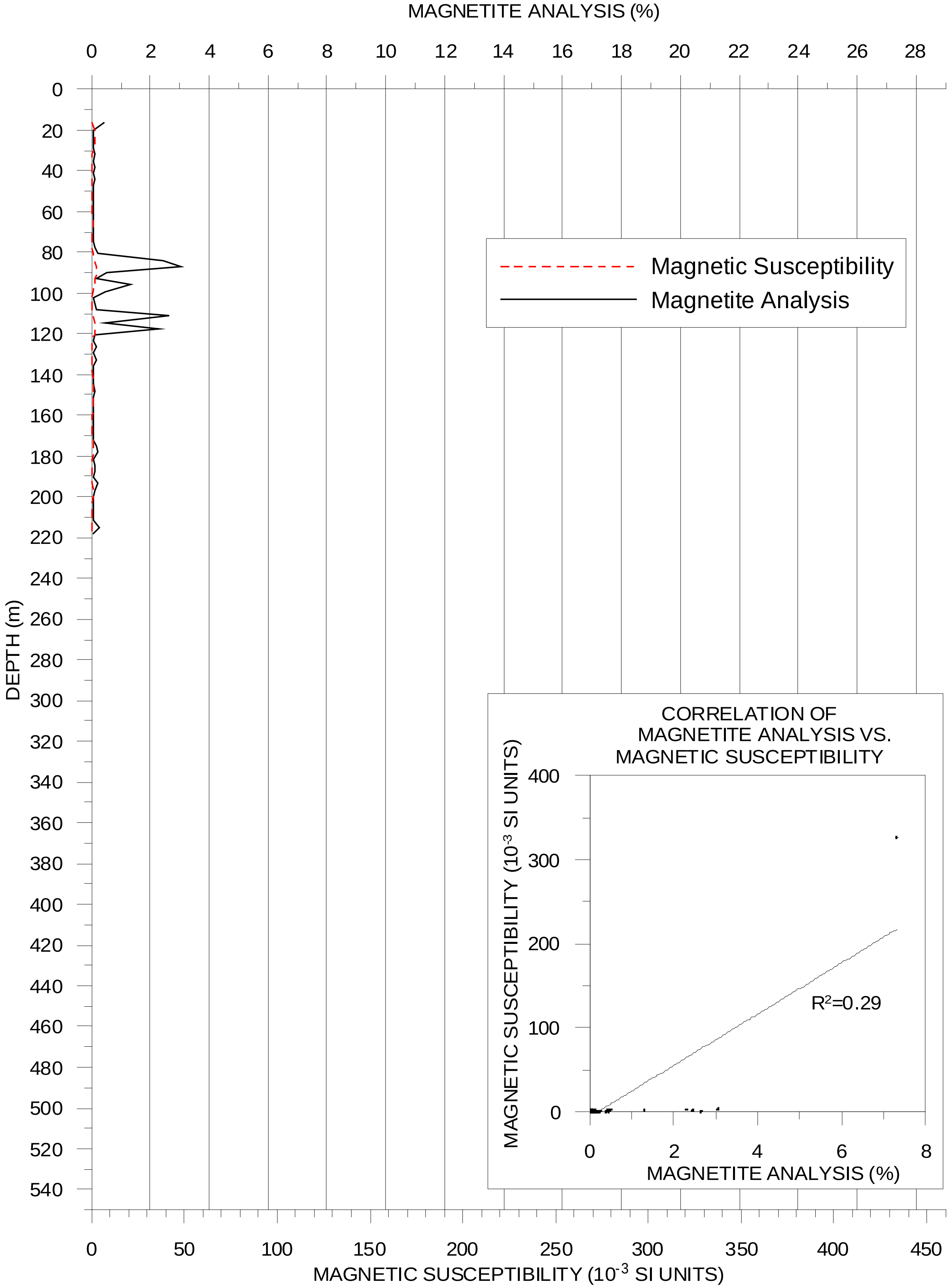


SIGNIFICANT MAGNETITE INTERCEPT			
From (m)	To (m)	Length (m)	Grade (%)
248.6	450.2	201.6	8.7

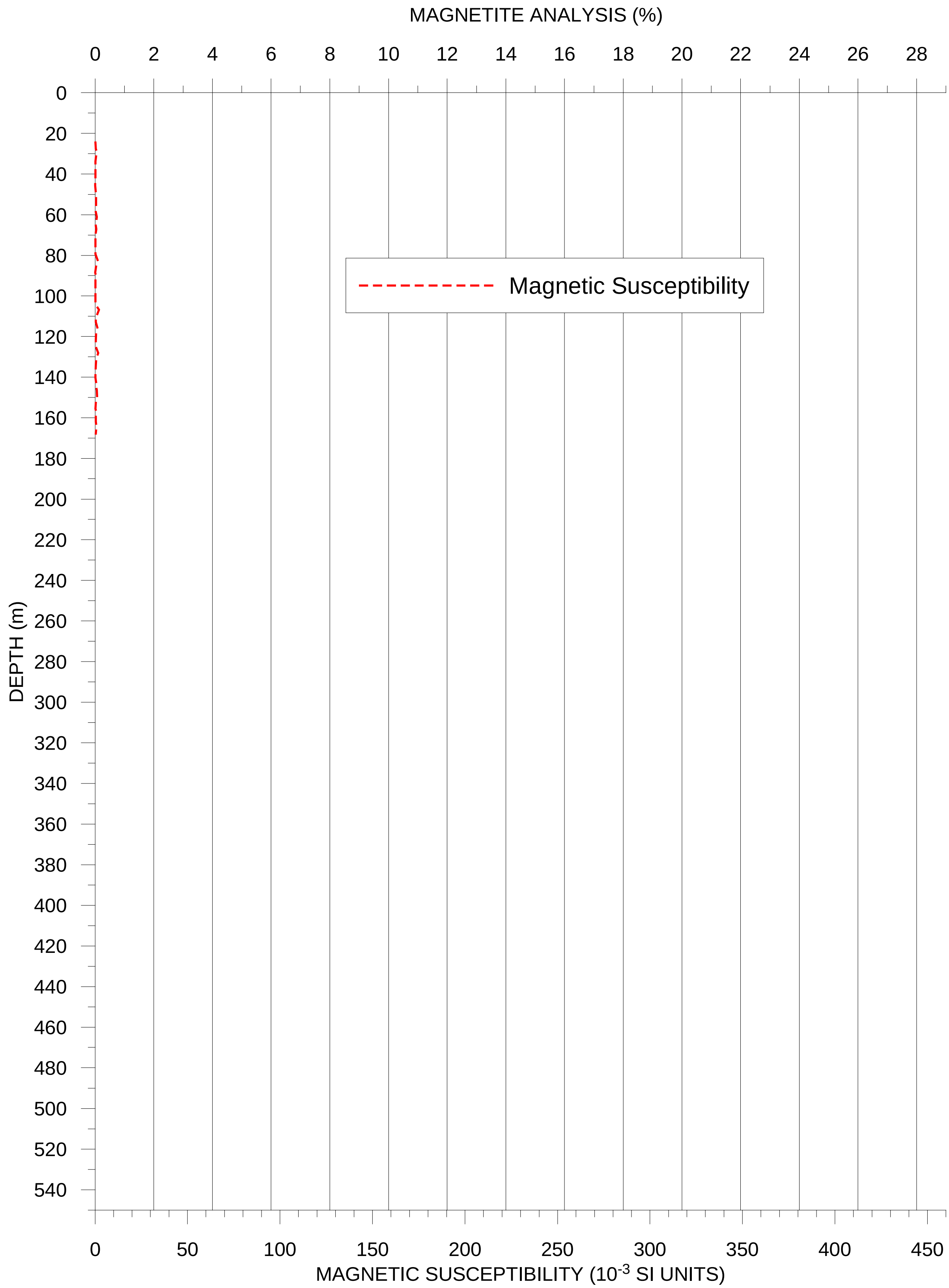
SKYLINE GOLD CORP.

MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS

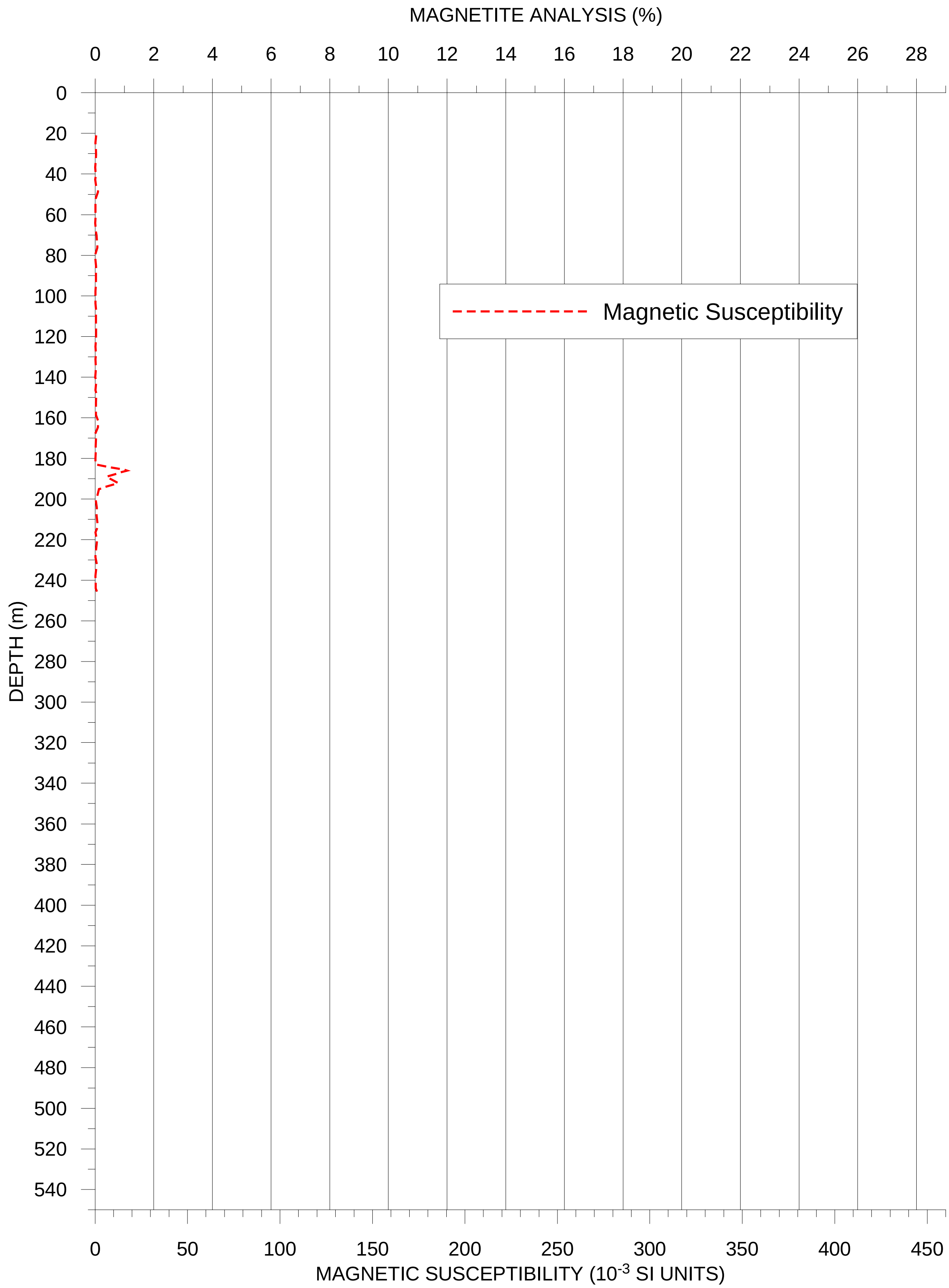
HOLE 1229	OCT 09	AB



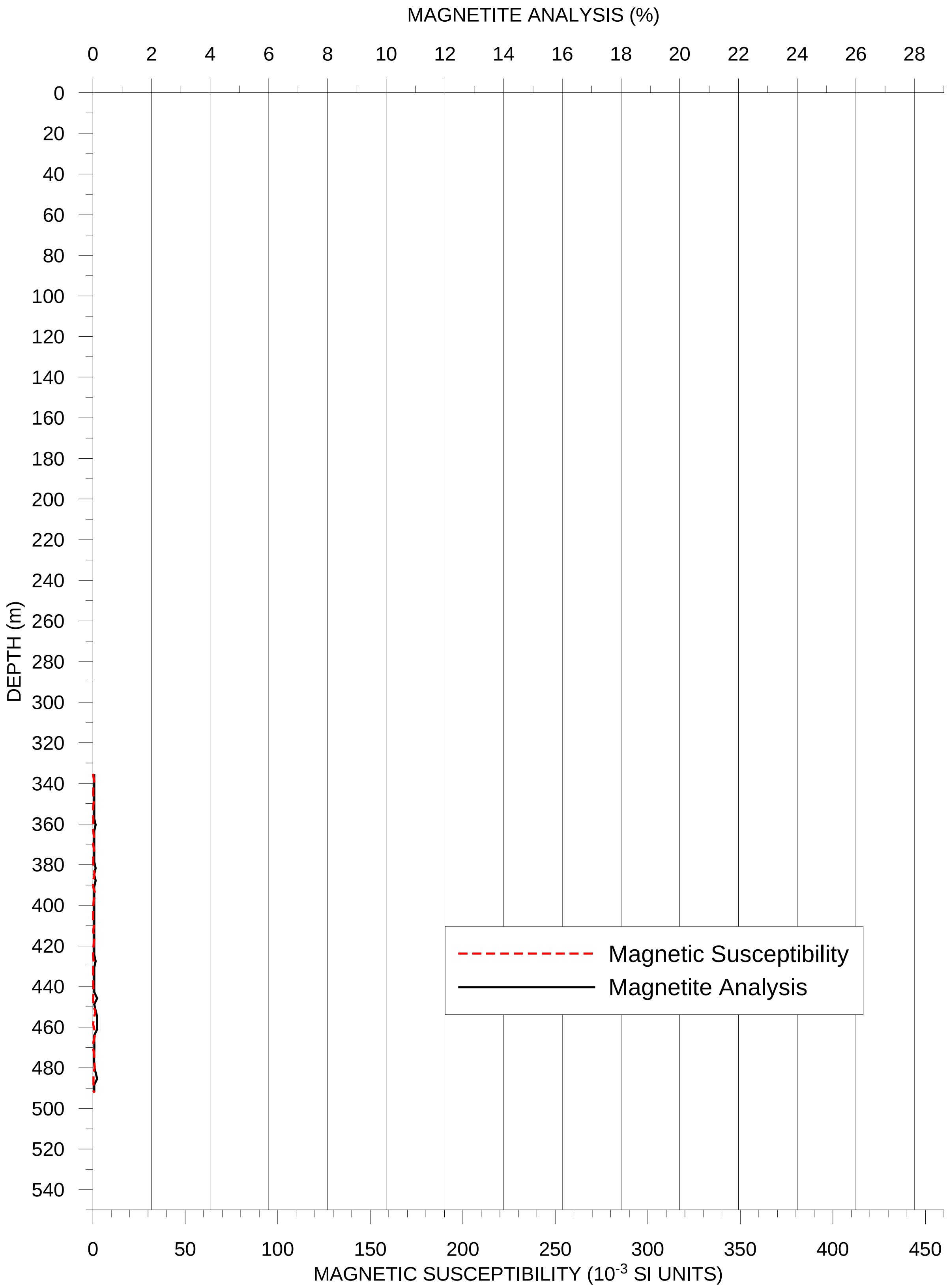
SKYLINE GOLD CORP.		
MAGNETIC SUSCEPTIBILITY AND MAGNETITE ANALYSIS		
HOLE 1232	OCT 09	AB



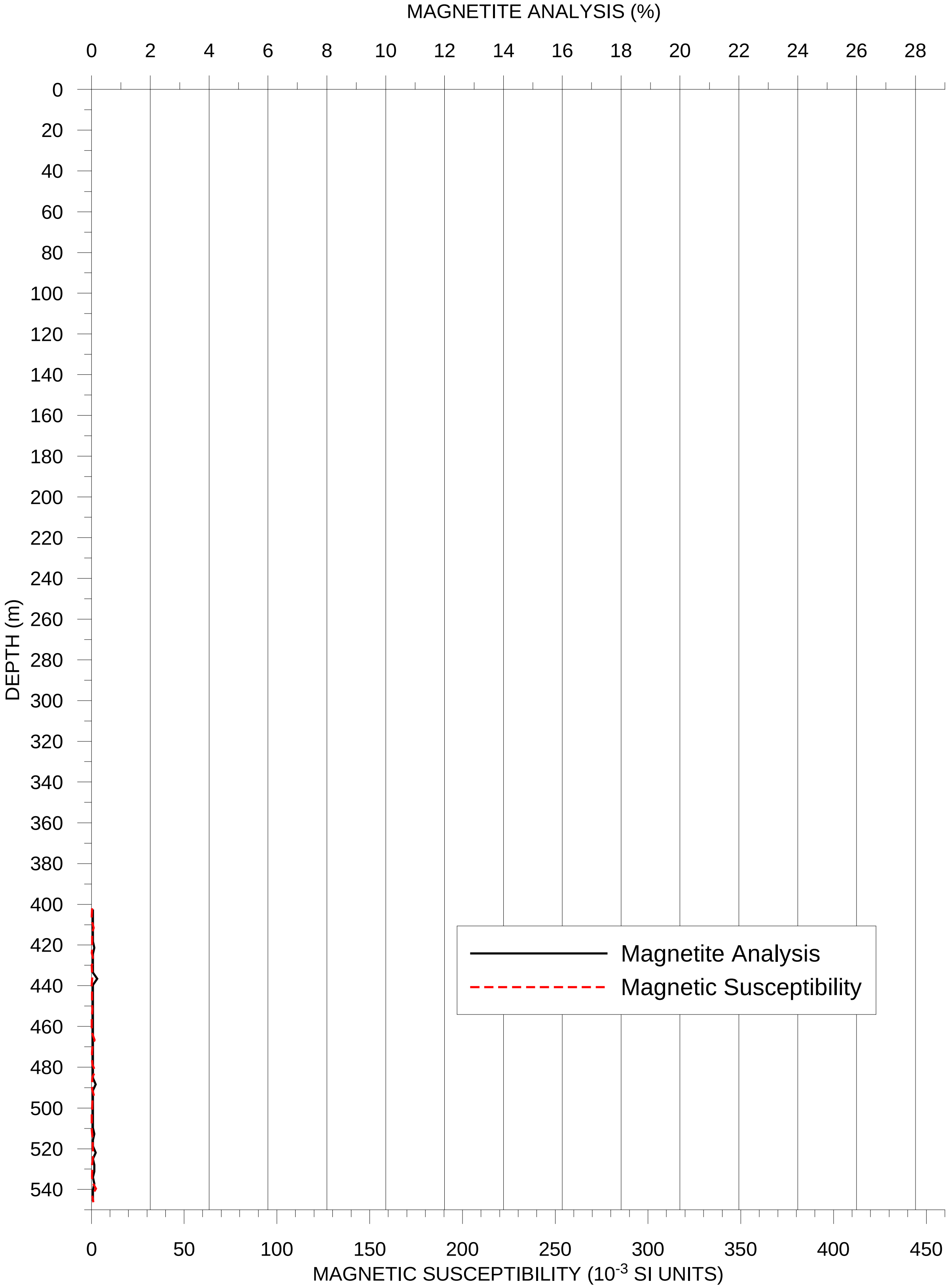
SKYLINE GOLD CORP.		
MAGNETIC SUSCEPTIBILITY GRAPHIC LOG		
HOLE 1243	OCT 09	AB



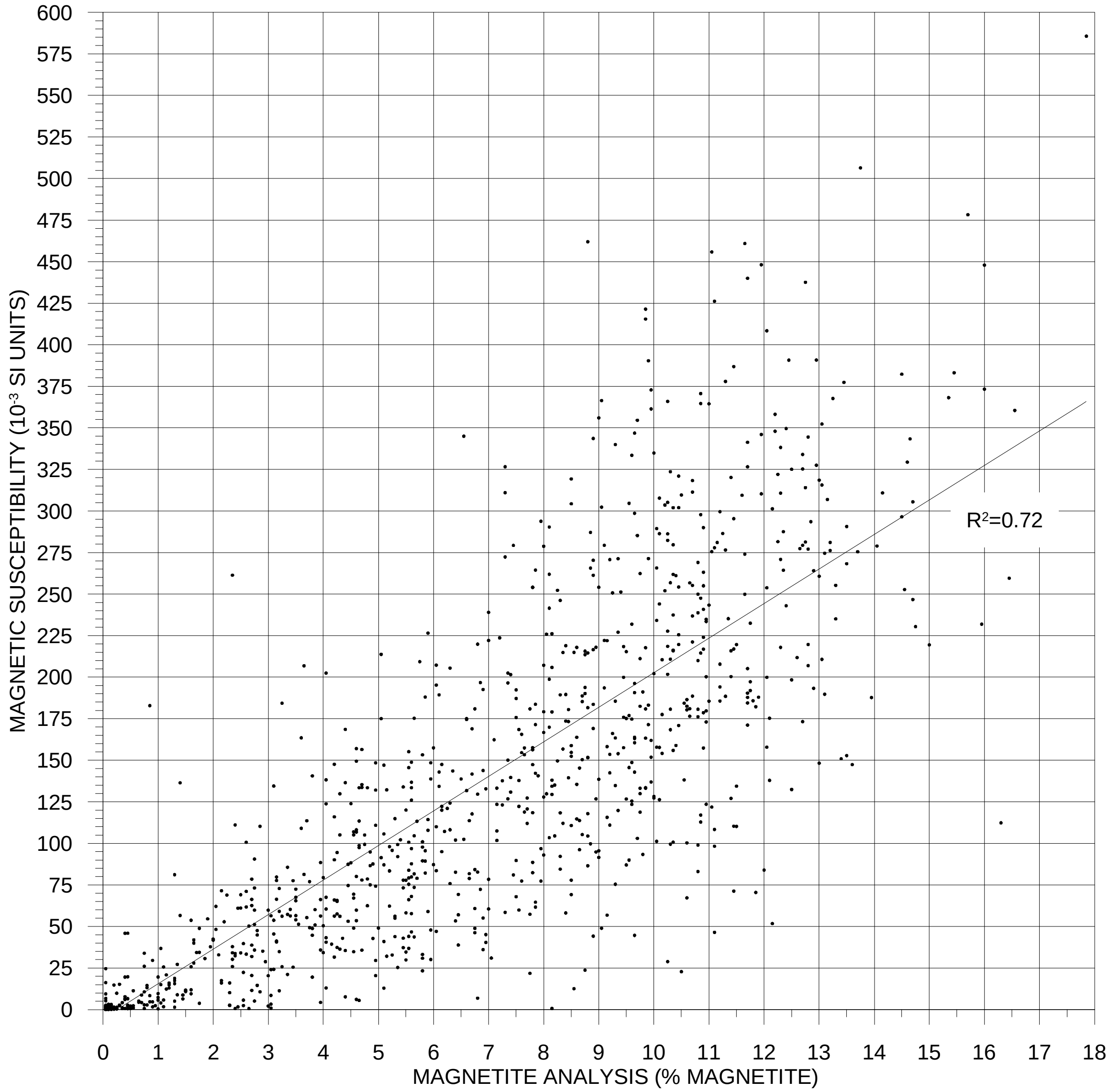
SKYLINE GOLD CORP.		
MAGNETIC SUSCEPTIBILITY GRAPHIC LOG		
HOLE 1244	OCT 09	AB



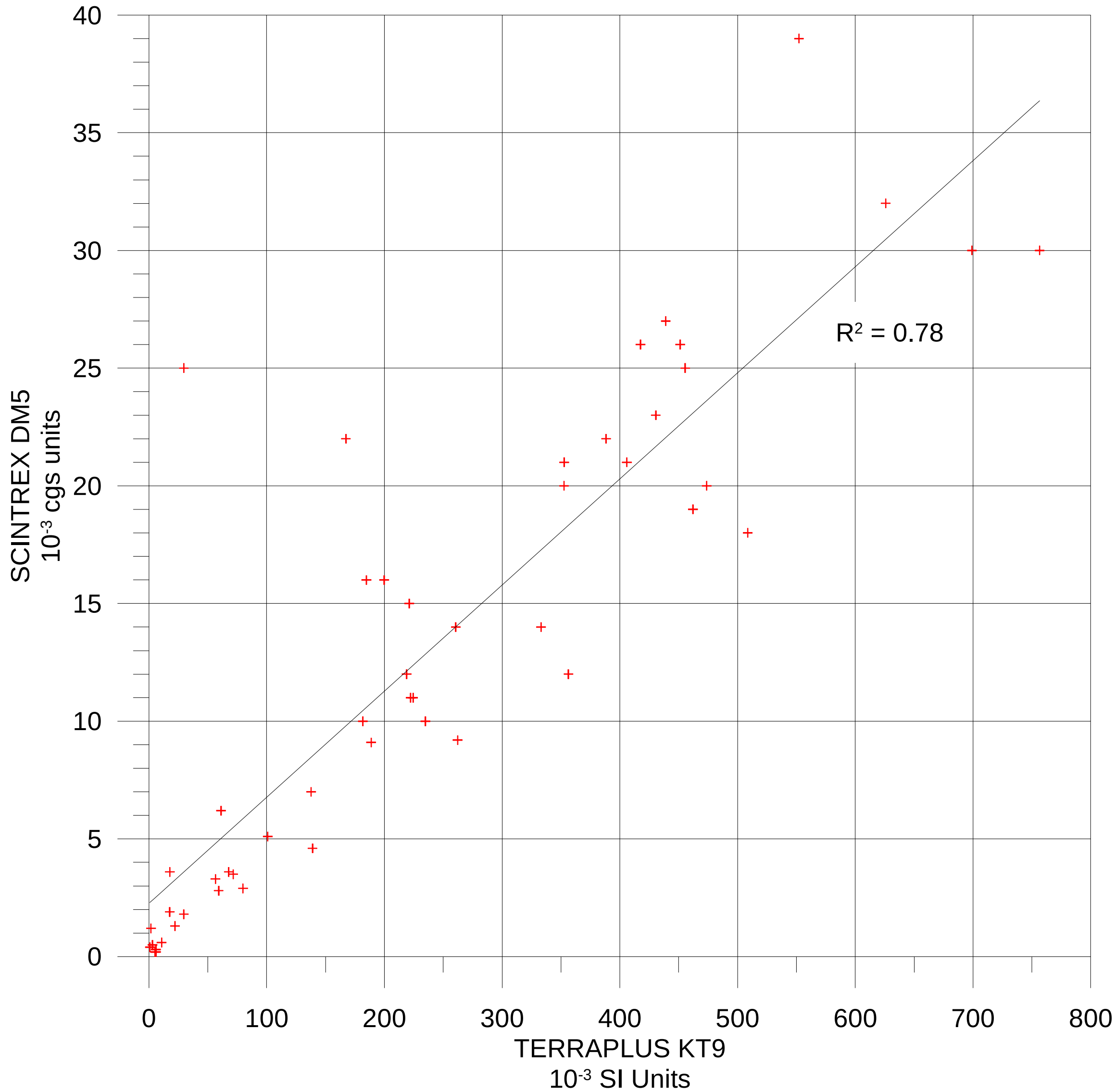
SKYLINE GOLD CORP.		
MAGNETIC SUSCEPTIBILITY GRAPHIC LOG		
HOLE 1245	OCT 09	AB



SKYLINE GOLD CORP.		
MAGNETIC SUSCEPTIBILITY GRAPHIC LOG		
HOLE 1246	OCT 09	AB



MAGNETIC SUSCEPTIBILITY (10-3 SI UNITS)
MAGNETITE ANALYSIS (% MAGNETITE)
R2=0.72
0
25
50
75
100
125
150
175
200
225
250
275
300
325
350
375
400
425
450
475
500
525
550
575
600
0
1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18


40
35
30
25
20
15
10
5
0
SCINTREX DM5
10-3 cgs units
R2 = 0.78
0
100
200
300
400
500
600
700
800
TERRAPLUS KT9
10-3 SI Units

APPENDIX D

MAGNETITE STUDY – BC MINING RESEARCH LTD

BC MINING RESEARCH LTD
Metallurgical and Geo-metallurgical Engineering Services
122–1857 West 4th Avenue, Vancouver, BC, V6J 1M4 *Fax:*604 738 9050

September 18, 2008

Skyline Gold Corporation
212-19451 Shellbridge Way
Richmond, B.C.
V6X 2W8

Dear Jeff Smulders,

Re: Magnetite Study – Progress Report

The following summarizes the results of a magnetite study for the Bronson Slope Project. Included was a market study to estimate the amount of magnetite used for the BC and Alberta Coal industries for dense media separation as well as a metallurgical study to assess the properties of the Bronson Slope magnetite for use in dense media.

Magnetite Market Study

The results of the market study are summarized in the attached table titled "Survey of Magnetite Usage by BC and Alberta Coal Producers. Of the 18 operating coal operations in BC and Alberta, 10 use dense media separation to upgrade their coal. Dense media separation is a process in which finely ground magnetite is mixed with water to create a medium that has the properties of a dense liquid. Specifically when coal and rock particles are added to the medium, the low density coal particles will float while the high density rock particles will sink thereby facilitating separation of coal from waste rock. The dense media is used in two types of separators referred to static separators such as the dense media drum or dynamic separators such as the dense media cyclone. The specifications for magnetite used in dense media applications is as follows:

Particle size: 90% passing 325 mesh (45 μm)
Density: >4.7 g/cm^3
Magnetics content: >93% magnetics

The magnetite usage was estimated from reported magnetite consumption levels. A number of operations were contacted and consumption levels were either reported as kg of magnetite per tonne of raw coal or kg per tonne of clean coal. On a raw coal basis, one mine reported a consumption of 1 kg magnetite per tonne of raw coal. It was more common for operations to provide information on a clean coal basis for which

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consumptions ranged from 1 to 2.5 kg magnetite per tonne of clean coal. To estimate the total magnetite usage, an average value of 1.75 kg magnetite per tonne of clean coal was used. Total magnetite usage was then determined by multiplying the consumption by the tonnes of clean coal produced by each mine. Mine production levels were obtained through government reports and company websites for 2007. Based on the study, the estimate usage of magnetite by BC and Alberta Coal Mines for 2007 was 52,743 tonnes.

Few Operations were willing to provide price information for magnetite although one operation purchasing from the present supplier, Craigmont, indicated a price of $211/tonne delivered. The price of magnetite was estimated as the difference between the delivered cost and the cost of transport. The cost of transport was estimated for each mine based on the distance to the main center, for example Elkford, at a rate of $0.10/km/t. Using this calculation, the cost of magnetite was estimated to be $127.70/tonne. It is worth noting that recent magnetite prices for iron ore of up to $200 per tonne have been reported. While high magnetite pries are bound to fluctuate, such prices should provide pressure to increase the price of magnetite for dense media. Processing costs for dense media grade magnetite are significantly higher than for iron ore and therefore magnetite dense prices should be higher than iron ore.

The total value of magnetite sold to coal operations is estimated to be $6,735,311 per year. Transport costs added an additional $4,123,183 to this price such that the estimated total cost delivered is $10,860,494 per year. For dense media, transport costs from Bronson Slope are estimated to be $64 trucking (800 km x $0.08) plus $30 (1,000 km X $0.03) plus $5 loading charge totalling $99/tonne. For iron ore, the transport cost to Stewart is estimated to be $48 truck (600 km * $0.08) plus $10 loading fee totalling $58/t.

Metallurgical Studies

Metallurgical testing was performed on samples from the Quartz Magnetite zone of the Bronson Slope Deposit. The testing confirmed the metallurgical process, determine grinding work index for regrinding and characterize the magnetite product with respect to the specifications. The testing involved grinding and flotation to recover copper sulphides. The floatation tailings were then used for magnetic separation testing. The results of the metallurgical tests are presented in the attached tables. The quartz magnetite sample used for the testing graded 8.94% Fe, 0.27% Cu and 0.91 g/t Au. From flotation, the copper concentrate contained 79.1% of the copper and the combined flotation-gravity concentration gold recovery was 81.7%.

The flotation tailings were subjected to three stages of magnetite separation. The final product had a density of 4.97 g/cm^3 and a magnetite content of 99.9%. These specifications exceed those required for dense media confirming that a high grade magnetite product can be produced that is suitable for dense media separation. The product accounted for 3.68% of the feed mass and contained 28% of the iron. Based on

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rougher mass yields and recoveries, it is expected that these values could be increased to close to 10% and 55%, respectively.

This is a progress report aimed at providing a summary of information collected for the magnetite study. A final report is in preparation. If you have any questions, please feel free to contact me.

Sincerely yours,

Bern Klein

Bern Klein, PhD

SURVEY OF MAGNETITE USAGE BY BC AND ALBERTA COAL PRODUCERS

Date: 18-Sep-08

	Run of Mine	Clean Coal		Magnetite Consumption(kg/t)		Magnetite Usage**		Value of Magnetite	Transport Costs		Delivered
Operation	t/y	t/y	DMS	per t raw coal	per t clean coal*	kg	t	$***	$/t	$	Cost $
Coal Mountain	3,500,000	2,145,000	Yes		1.75	3753750	3754	479354	83	312687	792041
Elk View	7,000,000	5,047,000	Yes		1.75	8832250	8832	1127878	83	735726	1863605
Fording River	10,416,000	7,867,000	Yes		1.75	13767250	13767	1758078	83	1146812	2904890
Greenhills	5,300,000	4,143,000	Yes		1.75	7250250	7250	925857	83	603946	1529803
Line Creek	3,600,000	2,394,000	Yes		1.75	4189500	4190	534999	83	348985	883985
Quinsam	1,560,000	698,000	Yes		1.75	1221500	1222	155986	50	61075	217061
Western Canadian Coal	3,000,000	1,379,132	Yes		1.75	2413481	2413	308202	95	230246	538448
Cheviot Creek	2,559,334	1,793,929	Yes	1.00	1.75	3139376	3139	400898	61	190246	591144
Coal Valley	7,162,640	3,438,302	Yes	1.00	1.75	6017029	6017	768375	61	364632	1133006
Highvale	12,680,185		No			0	0				
Whitewood	1,265,691		No			0	0				
Genesee	5,137,572		No			0	0				
Paintearth	1,685,194		No			0	0				
Sheerness	3,959,504		No			0	0				
Vesta	1,236,663		No			0	0				
Dodds	101,845		No			0	0				
Burtonsville	15,684		No			0	0				
Grande Cache Corp.	1,245,045	1,233,630	Yes	1.00	1.75	2158853	2159	275685	61	130826	406512
					Total	52743238	52743	6735311		4125183	10860494

* 1 to 2.5 kg Magnetite used per ton clean coal was reported, therefore average of 1.75 kg/t was used for magnetite usage
** Magnetite usage based on consumption and tonnes of clean coal
*** Cost $211/t including transport/delivered was reported by one operation. The cost of magnetite was calculated based on the difference between the total deliverd cost and the transport cost which was estimated based on a rate of 0.10 $/t/km = $211.00-$83.30 = $127.70/t.
The value of magnetite is the product of the cost per ton and the tonnes of magnetite usage.

Distance (Merrit to Hinton) = 606 km
Distance (Merrit to Elkford) = 833 km
Distance (Merrit to Tumbler Ridge) = 954 km
Distance (Merrit to Campbell River) = 500 km

Western Canadian Coal Operations include Dillon, Wolverine, Willow Creek, Brule.

MET-SOLVE LABORATORIES INC.

METALLURGICAL BALANCE TEST REPORT

Client: Skyline Gold
Test: KE101
Sample: Composite as per given instructions

Date: 27-Aug-08
Project: MS1090

Product	Total Sample		Au		Cu		S		Fe		SG	Davis Tube Analysis		Magnetite Mass Yield	
	(g)	(%)	(g/t)	Dist'n (%)	(%)	Dist'n (%)	(%)	Dist'n (%)	(%)	Dist'n (%)		% Mag	% Non-Mag	(g)	(%)
Cleaner Concentrate	385.3	3.68	0.18	0.72	0.05	0.72	0.03	0.07	67.9	28.0	4.97	* 99.9	0.11	384.9	3.68
Cleaner Tailings #3	133.4	1.27	1.60	2.23	0.07	0.31	0.11	0.09	56.9	8.11	3.89	70.6	29.4	94.1	0.90
Cleaner Conc. #2	**518.7**	**4.95**	**0.55**	**2.95**	**0.06**	**1.04**	**0.05**	**0.15**	**65.1**	**36.1**	**4.69**	**92.3**	**7.66**	**479.0**	**4.57**
Cleaner Tailings #2	121.6	1.16	3.02	3.83	0.09	0.41	0.21	0.15	30.8	4.00	3.10	28.6	71.4	34.7	0.33
Cleaner Conc. #1	**640.2**	**6.11**	**1.02**	**6.79**	**0.06**	**1.45**	**0.08**	**0.31**	**58.6**	**40.1**	**4.39**	**80.2**	**19.8**	**513.7**	**4.91**
Cleaner Tailings #1	492.9	4.71	1.17	6.02	0.08	1.44	0.16	0.46	33.2	17.5	3.30	41.8	58.2	205.8	1.97
Rougher Mag. Conc.	**1133.1**	**10.8**	**1.08**	**12.8**	**0.07**	**2.89**	**0.12**	**0.77**	**47.5**	**57.5**	**3.91**	**63.5**	**36.5**	**719.5**	**6.87**
Rougher Non-Mag Tails	8815.5	84.2	0.06	5.52	0.05	16.0	0.20	10.4	2.30	21.7	2.63	0.33	99.7	29.3	0.28
Flotation Tailings	**9948.6**	**95.0**	**0.18**	**18.3**	**0.05**	**18.9**	**0.19**	**11.2**	**7.45**	**79.2**	**2.64**	**7.53**	**87.9**	**748.8**	**7.15**
Flot. Scavenger Conc.	101.6	0.97	3.62	3.84	3.05	11.1	23.0	13.8	29.2	3.17	-	-	-	-	-
Flot. Rougher Conc.	296.3	2.83	11.1	34.2	6.39	68.0	40.5	70.8	42.9	13.6	-	-	-	-	-
Total Flotation Conc.	**397.9**	**3.80**	**9.17**	**38.1**	**5.54**	**79.1**	**36.0**	**84.5**	**39.4**	**16.8**	-	-	-	-	-
Gravity L40 Tails	**10346.5**	**98.8**	**0.52**	**56.4**	**0.26**	**98.1**	**1.57**	**95.7**	**8.68**	**96.0**	-	-	-	-	-
Pan Tailings	103.5	0.99	9.14	9.88	0.47	1.75	4.51	2.75	26.6	2.94	-	-	-	-	-
Pan Conc.	20.0	0.19	161.4	33.7	0.28	0.20	13.1	1.54	51.4	1.10	-	-	-	-	-
Calculated Head	**10470.0**	**100.0**	**0.91**	**100.0**	**0.27**	**100.0**	**1.62**	**100.0**	**8.94**	**100.0**	-	-	-	-	-
Assayed Head			0.50		0.27		1.77		9.83						

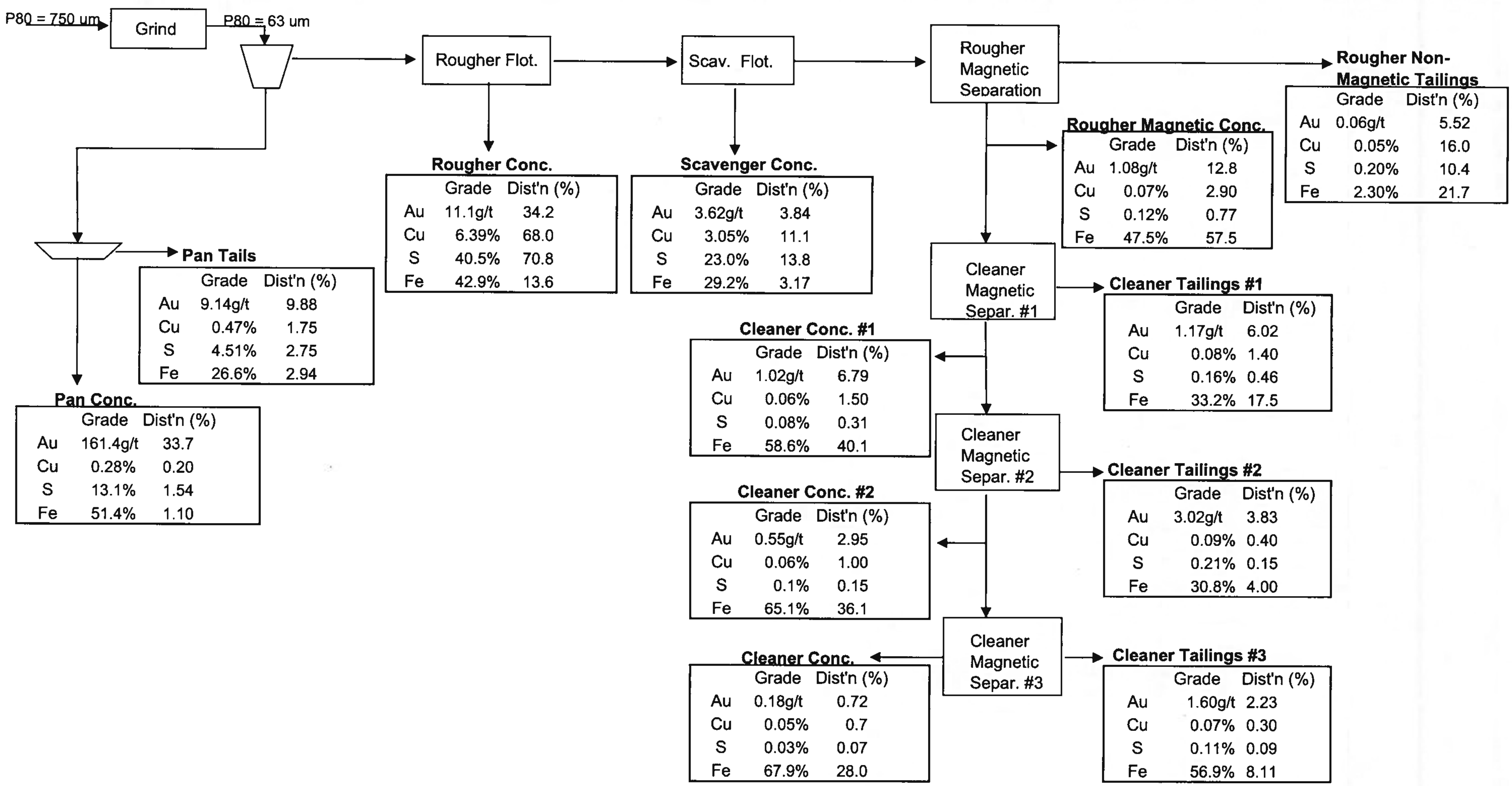
* Magnetic content of cleaner concentrate contains 68.5% Fe

MET-SOLVE LABORATORIES INC.

METALLURGICAL BALANCE FLOWSHEET

Client: Skyline Gold
Test: KE101
Sample: Composite as per given instructions

Date: 27-Aug-08
Project: MS1090



MET-SOLVE LABORATORIES INC.

FLOTATION TEST REPORT

Client: Skyline Gold
Test: KE101
Sample: Composite as per given instructions

Date: 18-Jun-08
Project: MS1090

Feed: Skyline Gold

Grind: 30 minute grind w/10 kg feed

Target pH:
Float Cell Volume: 10.0 liters
Pulp Density: 32.0% by weight

Conditions:

Stage					Time, minutes			pH	Elapsed Time (min)
		PAX	AF208	MIBC	Grind	Cond.	Float		
Initial									
Grind					30				
Gravity Separation									
Conditoner		4	2			5			5
Rougher				6			3		8
Conditoner		4	2			5			13
Scavenger							3		16
Total		8	4	6	30	10	6		16
Comments:	1 drop of MIBC = 30 g/t MIBC Float in each step until barren.								

Metallurgical Balance

Product	**Weight** g	**Weight** %	**Sample**
Rougher Conc.	296.3	2.86	**75359**
Scavenger Conc.	101.6	0.98	**75360**
Tails	9948.6	96.15	**75366**
Head (calc.)	10346.5	100.0	

Agitator Speed	1200	rpm
Float Cell Volume	9.0	Liters (with impeller in)
Solids SG	2.0	(based on wet sample)
Liquid SG	1.0	
Target % Solids	32.0%	
% Solids by Volume	19.0%	
Mass of Solids Req.	3,429	grams
Pulp SG	1.19	

MET-SOLVE LABORATORIES INC.

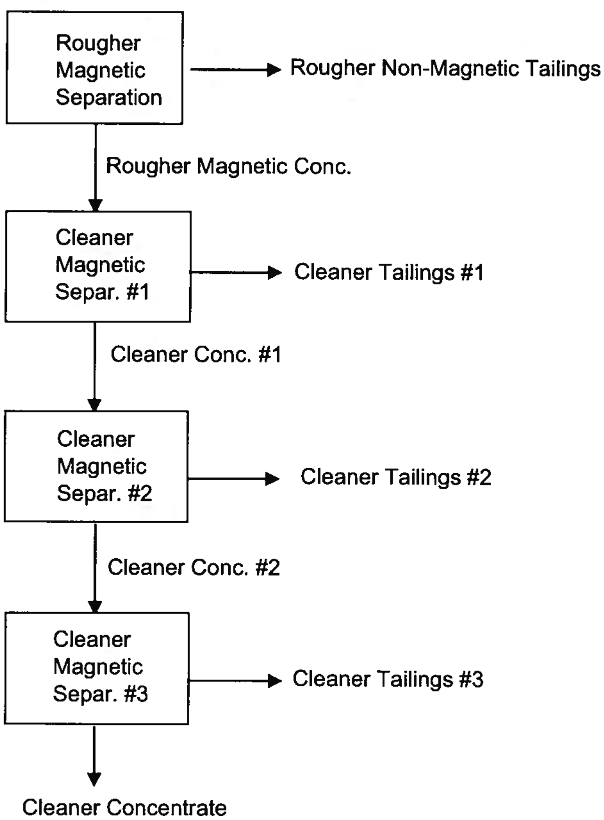
S.G.& DAVIS TUBE TEST REPORT

Client: Skyline Gold
Test: KE101

Date: 16-Jul-08
Project: MS1090

*Density of Water = 1.0000 g/mL
*Total Volume = 200 mL

Product	Flask	Total Sample		Sample used	Water	SG	Davis Tube Analysis	
	(g)	(g)	(%)	(g)	(g)		% Mag	% Non-Mag
Cleaner Concentrate	78.68	385.3	3.87	49.86	189.96	4.97	99.89	0.11
Cleaner Tailings #3	74.74	133.4	1.34	49.49	187.29	3.89	70.55	29.45
Cleaner Conc. #2	-	**518.7**	**5.21**	-	-	**4.69**	**92.34**	**7.66**
Cleaner Tailings #2	76.41	121.6	1.22	47.46	184.70	3.10	28.58	71.42
Cleaner Conc. #1	-	**640.2**	**6.44**	-	-	**4.39**	**80.24**	**19.76**
Cleaner Tailings #1	73.56	492.9	4.95	56.35	182.90	3.30	41.76	58.24
Rougher Mag. Conc.	-	**1133.1**	**11.4**	-	-	**3.91**	**63.50**	**36.50**
Rougher Non-Mag Tails	75.28	8815.5	88.6	51.46	180.45	2.63	0.33	99.67
Calculated Head	-	**9948.6**	**100.0**	-		**2.78**	**7.53**	**92.47**



MET-SOLVE LABORATORIES INC.

PARTICLE SIZE ANALYSIS

Client: Skyline Gold
Test: KE101
Sample: Head Sample

Date: Jun.20/08
Project: MS1090

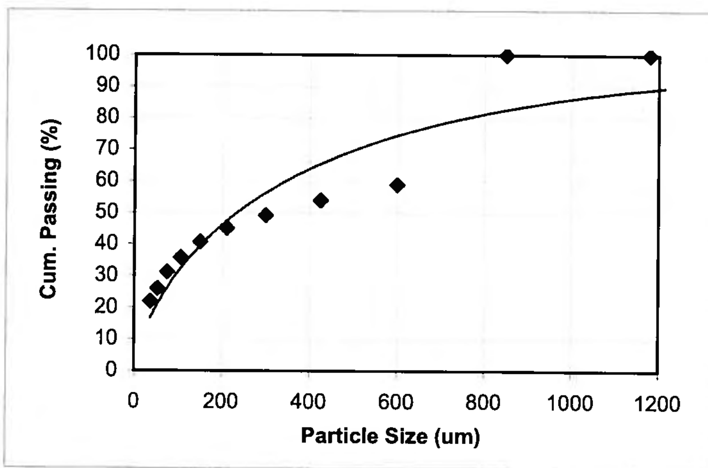
Sieve Size		Weight		Cummulative (%)	
Tyler Mesh	Microns	(g)	(%)	Retained	Passing
8	2360	0.0			
12	1700	0.0			
16	1180	0.0			
20	850	0.0			
30	600	85.9	41.16	41.16	58.84
40	425	10.4	4.98	46.14	53.86
50	300	9.9	4.74	50.89	49.11
70	212	8.5	4.07	54.96	45.04
100	150	9.1	4.36	59.32	40.68
140	106	10.2	4.89	64.21	35.79
200	75	9.5	4.55	68.76	31.24
270	53	11.0	5.27	74.03	25.97
400	37	8.5	4.07	78.10	21.90
Undersize	-37	45.7	21.90	100.00	
	TOTAL:	208.7	100.0		

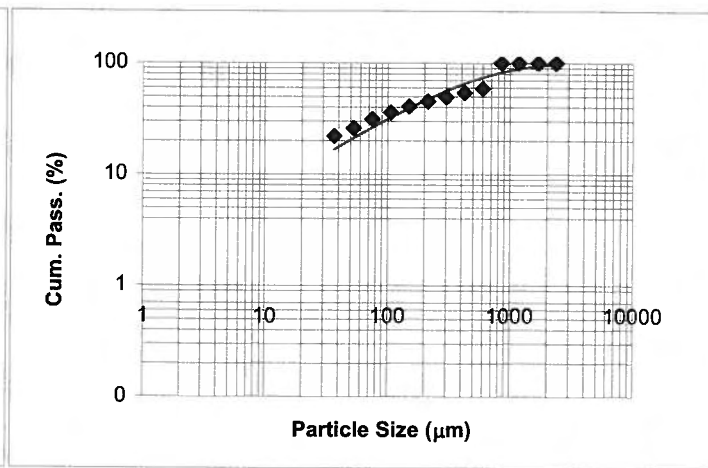
Rosin-Rammler Model

Size (um)	Passing P (%)
754	80
235	50

Linear Interpolation

Size (um)	Passing P (%)
729	80
323	50





MET-SOLVE LABORATORIES INC.

PARTICLE SIZE ANALYSIS

Client: Skyline Gold
Test: KE101
Sample: Feed sample, 30 minute grind

Date: Jun.20/08
Project: MS1090

Sieve Size		Weight		Cummulative (%)	
Tyler Mesh	Microns	(g)	(%)	Retained	Passing
8	2360	0.0			
12	1700	0.0			
16	1180	0.0			
20	850	0.0			
30	600	0.0			
40	425	0.0			
50	300	0.0			
70	212	0.0			
100	150	0.0			
140	106	1.6	1.82	1.82	98.18
200	75	7.7	8.74	10.56	89.44
270	53	15.0	17.03	27.58	72.42
400	37	14.4	16.35	43.93	56.07
Undersize	-37	49.4	56.07	100.00	
	TOTAL:	88.1	100.0		

Rosin-Rammler Model

Size (um)	Passing P (%)
60	80
33	50

Linear Interpolation

Size (um)	Passing P (%)
63	80
29	50